Bryan W. Shaw, Ph.D., *Chairman* Buddy Garcia, *Commissioner* Carlos Rubinstein, *Commissioner* Mark R. Vickery, P.G., *Executive Director* 



## **TEXAS COMMISSION ON ENVIRONMENTAL QUALITY**

Protecting Texas by Reducing and Preventing Pollution

September 2, 2010

Mr. Charles Salsman Christ Our King Anglican Church 111 W. San Antonio Street, Suite 250 New Braunfels, Texas 78130-5158 RECEIVED SEP 1 7 2010 COUNTY ENGINEER

Re: Edwards Aquifer, Comal County

NAME OF PROJECT: Christ Our King Anglican Church, located on FM 1863, 0.75 miles southwest of State Highway 46, New Braunfels, Texas

TYPE OF PLAN: Request for Approval of a Water Pollution Abatement Plan (WPAP). 30 Texas Administrative Code (TAC) Chapter 213 Edwards Aquifer

Edwards Aquifer Protection Program San Antonio File No. 2935.00, Investigation No. 828713

Regulated Entity No. RN105933493

Dear Mr. Salsman:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the WPAP Application for the above-referenced project submitted to the San Antonio Regional Office by HMT Engineering & Surveying on behalf of Christ Our King Anglican Church on June 8, 2010. Final review of the WPAP was completed after additional material was received on August 10, and August 27, 2010. As presented to the TCEO, the Temporary and Permanent Best Management Practices (BMPs) and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213. These planning materials were sealed, signed and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved. subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

#### BACKGROUND

The site is presently ranch land. Two houses, a barn, garage, and a shed (0.42 acre of impervious cover) are located within the boundary of the proposed site. Three water wells are presently in use.

Réply To: Region 13 • 14250 Judson Rd. • San Antonio, Texas 78233-4480 • 210-490-3096 • Fax 210-545-4329

Mr. Charles Salsman Page 2 September 2, 2010

#### PROJECT DESCRIPTION

The proposed commercial project will be constructed in six phases and will have an area of approximately 22.11 acres. The existing 0.42 acre of impervious cover will be removed. The impervious cover to be constructed will be 9.61 acres (43 percent). The project will include a youth building, parking, drives, sidewalks, church, chapel, columbarium, fellowship hall, pavilion, administration building, school buildings, dormitory, and a community center. Three existing wells will provide water for the first few phases of development. The project will include a wastewater treatment facility. The first five phases of development will result in wastewater flows totaling less than 5,000 gallons per day. According to a letter dated June 10, 2010, signed by Robert Boyd, P.E., with Comal County, the site is acceptable for the use of on-site sewage facilities. The projected population for the completed project is about 4,000 people. Wastewater generated is projected to exceed 23,000 gallons per day. Before the wastewater flow exceeds 5,000 gallons per day, the facility will be connected to a public sewer.

#### PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, engineered vegetated filter strips and Vortechs hydrodynamic separators, designed using the TCEQ technical guidance document, *Complying with the Edwards Aquifer Rules: Technical Guidance on Best Management Practices* (2005), will be constructed to treat stormwater runoff. The required total suspended solids (TSS) treatment for this project is 8,249 pounds of TSS generated from the 9.61 acres of impervious cover. 9.48 acres of impervious cover is to be captured for treatment. About 0.13 acre will not be captured for treatment. The approved measures meet the required 80 percent removal of the increased load in TSS caused by the project.

The individual treatment measures will consist of two engineered vegetated filter strips and five Vortechs hydrodynamic separators. A total of about 8,684 pounds of suspended solids will be removed each year from stormwater runoff. Adequate overtreatment will therefore be provided to compensate for the lack of treatment of stormwater generated from the 0.13 acre of impervious cover that will not be captured.

Two engineered vegetative filter strips are to remove about 440 pounds of suspended solids annually.

Vegetated filter strip slopes will not exceed 20%;

The minimum dimension of the filter strips (in the direction of flow) will not be less than 15 feet; The maximum width (in the flow direction) of the contributing impervious areas will not exceed 72 feet;

The minimum vegetated cover will be 80%;

The contributing areas to the filter strips will be relatively flat so that runoff will be distributed evenly to the vegetated area without the use of a level spreader;

The vegetated filter strips will be free of gullies or rills that can concentrate overland flow.

The five Vortechs units, two models Vx1421, one model Vx9000, and one model Vx16000, are to remove a total of about 8,244 pounds of suspended solids per year.

Mr. Charles Salsman Page 3 September 2, 2010

I.

#### **GEOLOGY**

According to the geologic assessment included with the application, the site is on the Edwards Aquifer recharge zone. The geologic map provided shows Cretaceous Buda and Del Rio formations at the higher elevations and over most of the site. The Cretaceous Georgetown formation is mapped at the extreme southern and western parts of the site, and the Cretaceous Person formation is mapped at the extreme south corner of the site. An inferred fault (down to the east) is mapped in the southeast part of the site. No evidence of the fault was related found during the field investigation. Six features were noted. None were characterized as "sensitive". The features included the fault and three water wells. The San Antonio Regional Office did not conduct a site assessment.

#### SPECIAL CONDITIONS

- For each phase of the development, permanent pollution abatement measures shall be operational prior to occupancy.
- II. As the sewage collection system for the facility will eventually be connected to an off-site treatment plant, a sewage collection system plan application must be submitted in accordance with 30 TAC 213. The plan must be approved by the TCEQ prior to any construction of a collection system at the site.
- III. All sediment and/or media removed from permanent pollution abatement measures during maintenance activities shall be properly disposed of according to 30 TAC 330 or 30 TAC 335, as applicable.
- IV. Be advised that if any of the existing water wells on site are utilized for human consumption, compliance with the applicable 30 TAC 290 regulations relating to public water system permitting and operation may be required

#### STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

#### Prior to Commencement of Construction:

4. Within 60 days of receiving written approval of an Edwards Aquifer Protection Plan, the applicant must submit to the San Antonio Regional Office, proof of recordation of notice in the county deed records, with the volume and page number(s) of the county deed

records of the county in which the property is located. A description of the property boundaries shall be included in the deed recordation in the county deed records. A suggested form (Deed Recordation Affidavit, TCEQ-0625) that you may use to deed record the approved WPAP is enclosed.

- 5. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved WPAP and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 6. Modification to the activities described in the referenced WPAP application following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.
- 7. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the San Antonio Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the date on which the regulated activity will commence, the name of the approved plan and program ID number for the regulated activity, and the name of the prime contractor with the name and telephone number of the contact person. The executive director will use the notification to determine if the approved plan is eligible for an extension.
- 8. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved WPAP, must be installed prior to construction and maintained during construction. Temporary E&S controls may be removed when vegetation is established and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.
- 9. All borings with depths greater than or equal to 20 feet must be plugged with non-shrink grout from the bottom of the hole to within three (3) feet of the surface. The remainder of the hole must be backfilled with cuttings from the boring. All borings less than 20 feet must be backfilled with cuttings from the boring. All borings must be backfilled or plugged within four (4) days of completion of the drilling operation. Voids may be filled with gravel.

#### During Construction:

- 10. During the course of regulated activities related to this project, the applicant or agent shall comply with all applicable provisions of 30 TAC Chapter 213, Edwards Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.
- 11. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be

Mr. Charles Salsman Page 5 September 2, 2010

submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 6, above.

12. If any sensitive feature (caves, solution cavities, sink holes, etc.) is discovered during construction, all regulated activities near the feature must be suspended immediately. The applicant or his agent must immediately notify the San Antonio Regional Office of the discovery of the feature. Regulated activities near the feature may not proceed until the executive director has reviewed and approved the methods proposed to protect the feature and the aquifer from potentially adverse impacts to water quality. The plan must be sealed, signed, and dated by a Texas Licensed Professional Engineer.

13. Three wells exist on site. All water wells, including injection, dewatering, and monitoring wells must be in compliance with the requirements of the Texas Department of Licensing and Regulation under Title 16 TAC Chapter 76 (relating to Water Well Drillers and Pump Installers) and all other locally applicable rules, as appropriate.

14. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50 percent. Litter, construction debris, and construction chemicals shall be prevented from becoming stormwater discharge pollutants.

15. Intentional discharges of sediment laden storm water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices. These may include vegetated filter strips, sediment traps, rock berms, silt fence rings, etc.

16. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.

17. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.

#### After Completion of Construction:

18. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the San Antonio Regional Office within 30 days of site completion.

19. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. The regulated entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred. A copy of the transfer of responsibility must be filed with the executive director through the San Antonio Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.

- 20. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 21. An Edwards Aquifer protection plan approval or extension will expire and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new Edwards Aquifer protection plan must be submitted to the San Antonio Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.
- 22. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.

If you have any questions or require additional information, please contact Alan G. Jones of the Edwards Aquifer Protection Program of the San Antonio Regional Office at (210) 403-4074.

Sincerely,

Mark R. Vickery, P.G. Executive Director Texas Commission on Environmental Quality

MRV/AGJ/eg

Enclosures: Deed Recordation Affidavit, Form TCEQ-0625 Change in Responsibility for Maintenance of Permanent BMPs, Form TCEQ-10263

cc:

Mr. Jeffrey D. Moeller, P.E., HMT Engineering & Surveying Mr. James C. Klein, P.E., City Engineer, City of New Braunfels Mr. Tom Hornseth, P.E., Comal County Mr. Karl J. Dreher, Edwards Aquifer Authority TCEQ Central Records, Building F, MC 212 Bryan W. Shaw, Ph.D., *Chairman* Buddy Garcia, *Commissioner* Carlos Rubinstein, *Commissioner* Mark R. Vickery, P.G., *Executive Director* 



# TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

September 2, 2010

Mr. Charles Salsman Christ Our King Anglican Church 111 W. San Antonio Street, Suite 250 New Braunfels, Texas 78130-5158 RECEIVED SEP 1 7 2010 COUNTY ENGINEER

 Re: <u>Edwards Aquifer</u>, Comal County NAME OF PROJECT: Christ Our King Anglican Church, located on FM 1863, 0.75 miles southwest of State Highway 46, New Braunfels, Texas TYPE OF PLAN: Request for Approval of a Water Pollution Abatement Plan (WPAP); 30 Texas Administrative Code (TAC) Chapter 213 Edwards Aquifer Edwards Aquifer Protection Program San Antonio File No. 2935.00, Investigation No. 828713 Regulated Entity No. RN105933493

Dear Mr. Salsman:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the WPAP Application for the above-referenced project submitted to the San Antonio Regional Office by HMT Engineering & Surveying on behalf of Christ Our King Anglican Church on June 8, 2010. Final review of the WPAP was completed after additional material was received on August 10, and August 27, 2010. As presented to the TCEO, the Temporary and Permanent Best Management Practices (BMPs) and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213. These planning materials were sealed, signed and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

## BACKGROUND

The site is presently ranch land. Two houses, a barn, garage, and a shed (0.42 acre of impervious cover) are located within the boundary of the proposed site. Three water wells are presently in use.

REPLY TO: REGION 13 • 14250 JUDSON RD. • SAN ANTONIO, TEXAS 78233-4480 • 210-490-3096 • FAX 210-545-4329

Mr. Charles Salsman Page 2 September 2, 2010

#### PROJECT DESCRIPTION

The proposed commercial project will be constructed in six phases and will have an area of approximately 22.11 acres. The existing 0.42 acre of impervious cover will be removed. The impervious cover to be constructed will be 9.61 acres (43 percent). The project will include a youth building, parking, drives, sidewalks, church, chapel, columbarium, fellowship hall, pavilion, administration building, school buildings, dormitory, and a community center. Three existing wells will provide water for the first few phases of development. The project will include a wastewater treatment facility. The first five phases of development will result in wastewater flows totaling less than 5,000 gallons per day. According to a letter dated June 10, 2010, signed by Robert Boyd, P.E., with Comal County, the site is acceptable for the use of on-site sewage facilities. The projected population for the completed project is about 4,000 people. Wastewater generated is projected to exceed 23,000 gallons per day. Before the wastewater flow exceeds 5,000 gallons per day, the facility will be connected to a public sewer.

#### PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, engineered vegetated filter strips and Vortechs hydrodynamic separators, designed using the TCEQ technical guidance document, *Complying with the Edwards Aquifer Rules: Technical Guidance on Best Management Practices* (2005), will be constructed to treat stormwater runoff. The required total suspended solids (TSS) treatment for this project is 8,249 pounds of TSS generated from the 9.61 acres of impervious cover. 9.48 acres of impervious cover is to be captured for treatment. About 0.13 acre will not be captured for treatment. The approved measures meet the required 80 percent removal of the increased load in TSS caused by the project.

The individual treatment measures will consist of two engineered vegetated filter strips and five Vortechs hydrodynamic separators. A total of about 8,684 pounds of suspended solids will be removed each year from stormwater runoff. Adequate overtreatment will therefore be provided to compensate for the lack of treatment of stormwater generated from the 0.13 acre of impervious cover that will not be captured.

Two engineered vegetative filter strips are to remove about 440 pounds of suspended solids annually.

Vegetated filter strip slopes will not exceed 20%;

The minimum dimension of the filter strips (in the direction of flow) will not be less than 15 feet; The maximum width (in the flow direction) of the contributing impervious areas will not exceed 72 feet;

The minimum vegetated cover will be 80%;

The contributing areas to the filter strips will be relatively flat so that runoff will be distributed evenly to the vegetated area without the use of a level spreader;

The vegetated filter strips will be free of gullies or rills that can concentrate overland flow.

The five Vortechs units, two models Vx1421, one model Vx9000, and one model Vx16000, are to remove a total of about 8,244 pounds of suspended solids per year.

Mr. Charles Salsman Page 3 September 2, 2010

#### <u>GEOLOGY</u>

According to the geologic assessment included with the application, the site is on the Edwards Aquifer recharge zone. The geologic map provided shows Cretaceous Buda and Del Rio formations at the higher elevations and over most of the site. The Cretaceous Georgetown formation is mapped at the extreme southern and western parts of the site, and the Cretaceous Person formation is mapped at the extreme south corner of the site. An inferred fault (down to the east) is mapped in the southeast part of the site. No evidence of the fault was related found during the field investigation. Six features were noted. None were characterized as "sensitive". The features included the fault and three water wells. The San Antonio Regional Office did not conduct a site assessment.

## SPECIAL CONDITIONS

- I. For each phase of the development, permanent pollution abatement measures shall be operational prior to occupancy.
- II. As the sewage collection system for the facility will eventually be connected to an off-site treatment plant, a sewage collection system plan application must be submitted in accordance with 30 TAC 213. The plan must be approved by the TCEQ prior to any construction of a collection system at the site.
- III. All sediment and/or media removed from permanent pollution abatement measures during maintenance activities shall be properly disposed of according to 30 TAC 330 or 30 TAC 335, as applicable.
- IV. Be advised that if any of the existing water wells on site are utilized for human consumption, compliance with the applicable 30 TAC 290 regulations relating to public water system permitting and operation may be required

#### STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

#### Prior to Commencement of Construction:

4. Within 60 days of receiving written approval of an Edwards Aquifer Protection Plan, the applicant must submit to the San Antonio Regional Office, proof of recordation of notice in the county deed records, with the volume and page number(s) of the county deed

records of the county in which the property is located. A description of the property boundaries shall be included in the deed recordation in the county deed records. A suggested form (Deed Recordation Affidavit, TCEQ-0625) that you may use to deed record the approved WPAP is enclosed.

- 5. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved WPAP and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 6. Modification to the activities described in the referenced WPAP application following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.
- 7. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the San Antonio Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the date on which the regulated activity will commence, the name of the approved plan and program ID number for the regulated activity, and the name of the prime contractor with the name and telephone number of the contact person. The executive director will use the notification to determine if the approved plan is eligible for an extension.
- 8. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved WPAP, must be installed prior to construction and maintained during construction. Temporary E&S controls may be removed when vegetation is established and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.
- 9. All borings with depths greater than or equal to 20 feet must be plugged with non-shrink grout from the bottom of the hole to within three (3) feet of the surface. The remainder of the hole must be backfilled with cuttings from the boring. All borings less than 20 feet must be backfilled with cuttings from the boring. All borings must be backfilled or plugged within four (4) days of completion of the drilling operation. Voids may be filled with gravel.

## **During Construction**:

- 10. During the course of regulated activities related to this project, the applicant or agent shall comply with all applicable provisions of 30 TAC Chapter 213, Edwards Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.
- 11. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be

Mr. Charles Salsman Page 5 September 2, 2010

submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 6, above.

- 12. If any sensitive feature (caves, solution cavities, sink holes, etc.) is discovered during construction, all regulated activities near the feature must be suspended immediately. The applicant or his agent must immediately notify the San Antonio Regional Office of the discovery of the feature. Regulated activities near the feature may not proceed until the executive director has reviewed and approved the methods proposed to protect the feature and the aquifer from potentially adverse impacts to water quality. The plan must be sealed, signed, and dated by a Texas Licensed Professional Engineer.
- 13. Three wells exist on site. All water wells, including injection, dewatering, and monitoring wells must be in compliance with the requirements of the Texas Department of Licensing and Regulation under Title 16 TAC Chapter 76 (relating to Water Well Drillers and Pump Installers) and all other locally applicable rules, as appropriate.
- 14. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50 percent. Litter, construction debris, and construction chemicals shall be prevented from becoming stormwater discharge pollutants.
- 15. Intentional discharges of sediment laden storm water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices. These may include vegetated filter strips, sediment traps, rock berms, silt fence rings, etc.
- 16. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 17. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.

## After Completion of Construction:

- 18. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the San Antonio Regional Office within 30 days of site completion.
- 19. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or

municipality) or the ownership of the property is transferred to the entity. The regulated entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred. A copy of the transfer of responsibility must be filed with the executive director through the San Antonio Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.

- 20. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 21. An Edwards Aquifer protection plan approval or extension will expire and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new Edwards Aquifer protection plan must be submitted to the San Antonio Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.
- 22. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.

If you have any questions or require additional information, please contact Alan G. Jones of the Edwards Aquifer Protection Program of the San Antonio Regional Office at (210) 403-4074.

Sincerely,

Mark R. Vickery, P.G. Executive Director Texas Commission on Environmental Quality

MRV/AGJ/eg

Enclosures: Deed Recordation Affidavit, Form TCEQ-0625 Change in Responsibility for Maintenance of Permanent BMPs, Form TCEQ-10263

cc: Mr. Jeffrey D. Moeller, P.E., HMT Engineering & Surveying Mr. James C. Klein, P.E., City Engineer, City of New Braunfels Mr. Tom Hornseth, P.E., Comal County Mr. Karl J. Dreher, Edwards Aquifer Authority TCEQ Central Records, Building F, MC 212 Bryan W. Shaw, Ph.D., *Chairman* Buddy Garcia, *Commissioner* Carlos Rubinstein, *Commissioner* Mark R. Vickery, P.G., *Executive Director* 



# TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

September 2, 2010

Mr. Charles Salsman Christ Our King Anglican Church 111 W. San Antonio Street, Suite 250 New Braunfels, Texas 78130-5158 SEP 1 7 2010 COUNTY ENGINEER

 Re: <u>Edwards Aquifer</u>, Comal County NAME OF PROJECT: Christ Our King Anglican Church, located on FM 1863, 0.75 miles southwest of State Highway 46, New Braunfels, Texas TYPE OF PLAN: Request for Approval of a Water Pollution Abatement Plan (WPAP); 30 Texas Administrative Code (TAC) Chapter 213 Edwards Aquifer Edwards Aquifer Protection Program San Antonio File No. 2935.00, Investigation No. 828713 Regulated Entity No. RN105933493

Dear Mr. Salsman:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the WPAP Application for the above-referenced project submitted to the San Antonio Regional Office by HMT Engineering & Surveying on behalf of Christ Our King Anglican Church on June 8, 2010. Final review of the WPAP was completed after additional material was received on August 10, and August 27, 2010. As presented to the TCEQ, the Temporary and Permanent Best Management Practices (BMPs) and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213. These planning materials were sealed, signed and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

#### BACKGROUND

The site is presently ranch land. Two houses, a barn, garage, and a shed (0.42 acre of impervious cover) are located within the boundary of the proposed site. Three water wells are presently in use.

Reply To: Region 13 • 14250 Judson Rd. • San Antonio, Texas 78233-4480 • 210-490-3096 • Fax 210-545-4329

Mr. Charles Salsman Page 2 September 2, 2010

#### **PROJECT DESCRIPTION**

The proposed commercial project will be constructed in six phases and will have an area of approximately 22.11 acres. The existing 0.42 acre of impervious cover will be removed. The impervious cover to be constructed will be 9.61 acres (43 percent). The project will include a youth building, parking, drives, sidewalks, church, chapel, columbarium, fellowship hall, pavilion, administration building, school buildings, dormitory, and a community center. Three existing wells will provide water for the first few phases of development. The project will include a wastewater treatment facility. The first five phases of development will result in wastewater flows totaling less than 5,000 gallons per day. According to a letter dated June 10, 2010, signed by Robert Boyd, P.E., with Comal County, the site is acceptable for the use of on-site sewage facilities. The projected population for the completed project is about 4,000 people. Wastewater generated is projected to exceed 23,000 gallons per day. Before the wastewater flow exceeds 5,000 gallons per day, the facility will be connected to a public sewer.

#### PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, engineered vegetated filter strips and Vortechs hydrodynamic separators, designed using the TCEQ technical guidance document, *Complying with the Edwards Aquifer Rules: Technical Guidance on Best Management Practices* (2005), will be constructed to treat stormwater runoff. The required total suspended solids (TSS) treatment for this project is 8,249 pounds of TSS generated from the 9.61 acres of impervious cover. 9.48 acres of impervious cover is to be captured for treatment. About 0.13 acre will not be captured for treatment. The approved measures meet the required 80 percent removal of the increased load in TSS caused by the project.

The individual treatment measures will consist of two engineered vegetated filter strips and five Vortechs hydrodynamic separators. A total of about 8,684 pounds of suspended solids will be removed each year from stormwater runoff. Adequate overtreatment will therefore be provided to compensate for the lack of treatment of stormwater generated from the 0.13 acre of impervious cover that will not be captured.

Two engineered vegetative filter strips are to remove about 440 pounds of suspended solids annually.

Vegetated filter strip slopes will not exceed 20%;

The minimum dimension of the filter strips (in the direction of flow) will not be less than 15 feet; The maximum width (in the flow direction) of the contributing impervious areas will not exceed 72 feet;

The minimum vegetated cover will be 80%;

The contributing areas to the filter strips will be relatively flat so that runoff will be distributed evenly to the vegetated area without the use of a level spreader;

The vegetated filter strips will be free of gullies or rills that can concentrate overland flow.

The five Vortechs units, two models Vx1421, one model Vx9000, and one model Vx16000, are to remove a total of about 8,244 pounds of suspended solids per year.

Mr. Charles Salsman Page 3 September 2, 2010

1

#### <u>GEOLOGY</u>

According to the geologic assessment included with the application, the site is on the Edwards Aquifer recharge zone. The geologic map provided shows Cretaceous Buda and Del Rio formations at the higher elevations and over most of the site. The Cretaceous Georgetown formation is mapped at the extreme southern and western parts of the site, and the Cretaceous Person formation is mapped at the extreme south corner of the site. An inferred fault (down to the east) is mapped in the southeast part of the site. No evidence of the fault was related found during the field investigation. Six features were noted. None were characterized as "sensitive". The features included the fault and three water wells. The San Antonio Regional Office did not conduct a site assessment.

## SPECIAL CONDITIONS

- I. For each phase of the development, permanent pollution abatement measures shall be operational prior to occupancy.
- II. As the sewage collection system for the facility will eventually be connected to an off-site treatment plant, a sewage collection system plan application must be submitted in accordance with 30 TAC 213. The plan must be approved by the TCEQ prior to any construction of a collection system at the site.
- III. All sediment and/or media removed from permanent pollution abatement measures during maintenance activities shall be properly disposed of according to 30 TAC 330 or 30 TAC 335, as applicable.
- IV. Be advised that if any of the existing water wells on site are utilized for human consumption, compliance with the applicable 30 TAC 290 regulations relating to public water system permitting and operation may be required

## STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

## Prior to Commencement of Construction:

4. Within 60 days of receiving written approval of an Edwards Aquifer Protection Plan, the applicant must submit to the San Antonio Regional Office, proof of recordation of notice in the county deed records, with the volume and page number(s) of the county deed

records of the county in which the property is located. A description of the property boundaries shall be included in the deed recordation in the county deed records. A suggested form (Deed Recordation Affidavit, TCEQ-0625) that you may use to deed record the approved WPAP is enclosed.

- 5. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved WPAP and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 6. Modification to the activities described in the referenced WPAP application following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.
- 7. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the San Antonio Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the date on which the regulated activity will commence, the name of the approved plan and program ID number for the regulated activity, and the name of the prime contractor with the name and telephone number of the contact person. The executive director will use the notification to determine if the approved plan is eligible for an extension.
- 8. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved WPAP, must be installed prior to construction and maintained during construction. Temporary E&S controls may be removed when vegetation is established and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.
- 9. All borings with depths greater than or equal to 20 feet must be plugged with non-shrink grout from the bottom of the hole to within three (3) feet of the surface. The remainder of the hole must be backfilled with cuttings from the boring. All borings less than 20 feet must be backfilled with cuttings from the boring. All borings must be backfilled or plugged within four (4) days of completion of the drilling operation. Voids may be filled with gravel.

## During Construction:

- 10. During the course of regulated activities related to this project, the applicant or agent shall comply with all applicable provisions of 30 TAC Chapter 213, Edwards Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.
- 11. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be

Mr. Charles Salsman Page 5 September 2, 2010

submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 6, above.

- 12. If any sensitive feature (caves, solution cavities, sink holes, etc.) is discovered during construction, all regulated activities near the feature must be suspended immediately. The applicant or his agent must immediately notify the San Antonio Regional Office of the discovery of the feature. Regulated activities near the feature may not proceed until the executive director has reviewed and approved the methods proposed to protect the feature and the aquifer from potentially adverse impacts to water quality. The plan must be sealed, signed, and dated by a Texas Licensed Professional Engineer.
- 13. Three wells exist on site. All water wells, including injection, dewatering, and monitoring wells must be in compliance with the requirements of the Texas Department of Licensing and Regulation under Title 16 TAC Chapter 76 (relating to Water Well Drillers and Pump Installers) and all other locally applicable rules, as appropriate.
- 14. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50 percent. Litter, construction debris, and construction chemicals shall be prevented from becoming stormwater discharge pollutants.
- 15. Intentional discharges of sediment laden storm water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices. These may include vegetated filter strips, sediment traps, rock berms, silt fence rings, etc.
- 16. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 17. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.

## After Completion of Construction:

- 18. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the San Antonio Regional Office within 30 days of site completion.
- 19. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or

municipality) or the ownership of the property is transferred to the entity. The regulated entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred. A copy of the transfer of responsibility must be filed with the executive director through the San Antonio Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.

- 20. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 21. An Edwards Aquifer protection plan approval or extension will expire and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new Edwards Aquifer protection plan must be submitted to the San Antonio Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.
- 22. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.

If you have any questions or require additional information, please contact Alan G. Jones of the Edwards Aquifer Protection Program of the San Antonio Regional Office at (210) 403-4074.

Sincerely,

Mark R. Vickery, P.G. Executive Director Texas Commission on Environmental Quality

MRV/AGJ/eg

- Enclosures: Deed Recordation Affidavit, Form TCEQ-0625 Change in Responsibility for Maintenance of Permanent BMPs, Form TCEQ-10263
- cc: Mr. Jeffrey D. Moeller, P.E., HMT Engineering & Surveying Mr. James C. Klein, P.E., City Engineer, City of New Braunfels Mr. Tom Hornseth, P.E., Comal County Mr. Karl J. Dreher, Edwards Aquifer Authority TCEQ Central Records, Building F, MC 212



2010 1122

PM 4: 30



RECEIVED

OCT 1 1 2010

COUNTY ENGINEER

August 27, 2010

Mr. Alan Jones Field Operations Division, Region 13 (San Antonio) Texas Commission on Environmental Quality 14250 Judson Road San Antonio, TX 78233-4480

RE: Christ Our King Anglican Church Water Pollution Abatement Plan Application

This letter is in response to the fax received 08/13/2010 TCEQ as it pertains to the Christ Our King Anglican Church Water Pollution Abatement Plan Application. The comments received are in italics and our responses are in bold.

- 1. Descriptions of Permanent BMPs Treatment methods and areas treated.
  - a. TCEQ-0587, Item No. 7, Attachment C, Project Description, and TCEQ-0600, Item No. 7 Attachment c, BMPs for On-Site Stormwater. In both attachments, please relate the area of existing impervious cover (square feet/acres) to be removed, the impervious cover to be treated by both types of BMPs, the impervious cover not captured (including areas of driveways on the highway right-of-way) and how the uncaptured impervious cover will be compensated for. Also relate annuals pounds to be removed be each kind of permanent MP and specify how treatment will exceed the required treatment.

## See attached Project Description and BMPs for On-Site Stormwater.

b. The table on Sheet 1, Drainage Area Map, gives a total of 9.36 acres of impervious cover in the 24 drainage areas. (Vegetated filter strips are shown treating 0.86 acres and Vortechs systems are shown treating 8.5 acres) The total impervious area shown above the table (and in the impervious cover table in the WPAP Application, Item No. 4) is 9.11 acres. The total of the impervious cover shown treated by the five Vortechs systems (the calculations) is 9.33 acres. Please explain the different numbers. Do the larger figures include off-site impervious cover?



# The total impervious cover for the project is 9.61 ac. The Drainage Area Map, WPAP Application, and TCEQ Calculations have been revised to accurately show the impervious areas.

c. In the table on sheet 1, Drainage Area Map, the impervious area is shown larger than the total area in Drainage Area 4. Drainage Area 9 looks to contain a significant amount of roof, but is shown with no impervious area. Also, the total impervious area shown treated by the Vortechs system is 0.62 acres, whereas the calculations show 1.42 acres of impervious area treated. Please explain or revise as needed.

The table has been corrected to accurately show the areas for Drainage Area 4. The table has been revised to accurately show the impervious cover for Drainage Area 9. The calculations have been updated to show a captured area of 1.9 acres (0.77 impervious, and 0.08 uncaptured).

d. Sheet 1, Drainage Area Map and Sheet 2, Phase 2 Map. At the northeast corner of the site most of the Drainage Area 4 looks to be down gradient of the (uncaptured by) Vortechs Systen #3. Also part of the parking lot which is shown in the Drainage Area 3 looks to drain to Drainage Area 4 (see Attachment). Also, much of the north end of the drainage area 1 does not look to drain to the vegetated filter strip. Please explain or revise as necessary. Please show any areas where runoff is not captured on the Drainage Area Map.

The location of the Vortechs System #3 has been relocated to the northeast corner of the site, where a larger portion of the drainage area can be captured. Drainage Areas 1 and 4 have been revised to show the area uncaptured. The new drainage areas are 1A, 1B, 4A, and, where 1B and 4B are the uncaptured areas. The drainage boundary between areas 3 and 4A have been revised to more accurately represent the drainage patterns. Drainage Area 3 remained 0.23 ac due to rounding of the acreage. Also, a landscaping inlet has been added for Drainage 8 to convey the runoff into the open area in Drainage Area 9 and ultimately be captured in Vortechs System #3.



Please accept these comments and revisions to the WPAP for the referenced project. If you need additional information or have any questions, please do not hesitate to contact myself or James Ingalls.

Sincerely,

James Ingalls on behalf of Jeff Moeller, P.E. Attachments

Water Pollution Abatement Plan Application

for Regulated Activities

on the Edwards Aquifer Recharge Zone and Relating to 30 TAC §213.5(b), Effective June 1, 1999

## REGULATED ENTITY NAME: Christ Our King Anglican Church

#### **REGULATED ENTITY INFORMATION**

The ty  	ype of project is: Residential: # of Lots: Residential: # of Living Unit Equivalents: Commercial Industrial Other:	
	Other:	
Total	site acreage (size of property):	22.11

3. Projected population:

1.

2.

4. The amount and type of impervious cover expected after construction are shown below:

4000

Impervious Cover of Proposed Project	Sq. Ft.	Sq. Ft./Acre	Acres
Structures/Rooftops	123,606	÷ 43,560 =	2.84
Parking (Driveway)	252,381	÷ 43,560 =	5.79
Other paved surfaces (Sidewalk)	42,625	÷ 43,560 =	0.98
Total Impervious Cover	305,420	÷ 43,560 =	9.61
Total Impervious Cover ÷ Total Acr	43%		

- 5. X ATTACHMENT A Factors Affecting Water Quality. A description of any factors that could affect surface water and groundwater quality is provided at the end of this form.
- 6. X Only inert materials as defined by 30 TAC §330.2 will be used as fill material.

## FOR ROAD PROJECTS ONLY Complete questions 7-12 if this application is exclusively for a road project.

- 7. Type of project:
  - \_\_\_\_\_ TXDOT road project.
  - County road or roads built to county specifications.
  - City thoroughfare or roads to be dedicated to a municipality.
  - Street or road providing access to private driveways.
- 8. Type of pavement or road surface to be used:
  - \_\_\_\_ Concrete
  - Asphaltic concrete pavement
  - \_\_\_\_Other: \_\_\_\_\_

2010

AUG



Christ Our King Anglican Church Water Pollution Abatement Plan

## ATTACHMENT "C" Project Description

Christ Our King Anglican Church is located on the south side of FM 1863 approximately 0.75 miles southwest of the intersection with State Highway 46. (See Location Map) There are 2 existing houses on-site along with some storage buildings. The site is divided into two watersheds, one drains north to Blieders Creek, the second drains south and west to the Dry Comal Creek. According to the Flood Insurance Rate Map No. 48091C0430F there is no existing floodplain located within the property.

The project is proposed to be constructed in 6 Phases (See Phasing Exhibit), each phase will have its own temporary and permanent BMP's installed per TCEQ requirements.

The church campus infrastructure will include a water system, electricity, telephone, cable television, and an On-Site Sewerage Facility is proposed to treat the sanitary sewer from the development. There are three on-site wells that will provide water service for the first few phases of development.

The impervious cover for the ultimate development of the 22.11 acre site will be approximately 43%. The site will utilize a combination of vegetative filter strips and Vortechs® Stormwater treatment systems to treat stormwater runoff generated by the proposed improvements.

Due to the construction phasing of the project, there will not be more than 10 acres of disturbed soil in one common drainage area that will occur at one time. The site is divided into two drainage areas. (See Drainage Area Map)

The site current has 0.42 acres of impervious cover that will be removed upon construction of the proposed improvements. The total proposed impervious cover to be on site is 9.61 acres, of this total, 9.48 acres will be captured and treated using Vegetative Filter Strips and 5 Vortechs systems. A total of 0.13 acres will be uncaptured. According to TCEQ Rules, 8249 lbs of TSS are required to be removed each year using BMPs. The proposed Vegetative Filter Strips will remove 440 lbs and the Vortechs systems will remove 8244 lbs of TSS per year. The proposed BMPs are treating in excess of 435 lbs of TSS per year.

## ATTACHMENT "A" 20% of Less Impervious Cover Waiver

The proposed development is a church campus and the 20% Impervious Cover Waiver does not apply. Permanent BMP's will be designed in accordance with TCEQ requirements for the removal of TSS generated by the proposed development.

## <u>ATTACHMENT "B"</u> BMP's for Upgradient Stormwater

The proposed site is at the top of the drainage area, thus no upgradient stormwater is accepted by the site.

## ATTACHMENT "C" BMP's for On-Site Stormwater

The permanent BMP's used to treat on-site stormwater runoff will be a combination of the Vortechs® system and vegetative filter strips. Please refer to the Drainage Area Map in the Temporary Stormwater Section for areas of treatment and BMP structures used.

The site current has 0.42 acres of impervious cover that will be removed upon construction of the proposed improvements. The total proposed impervious cover to be on site is 9.61 acres, of this total, 9.48 acres will be captured and treated using Vegetative Filter Strips and 5 Vortechs systems. A total of 0.13 acres will be uncaptured. According to TCEQ Rules, 8249 lbs of TSS are required to be removed each year using BMPs. The proposed Vegetative Filter Strips will remove 440 lbs and the Vortechs systems will remove 8244 lbs of TSS per year. The proposed BMPs are treating in excess of 435 lbs of TSS per year.

## ATTACHMENT "D" BMP's for Surface Streams

The vegetative filter strips and Vortechs® Storm water treatment system will be installed to prevent pollutants from entering surface streams and ultimately the aquifer. There were no sensitive features identified by the Geologic Assessment.

The natural vegetation located down gradient of proposed improvements will provide additional filtration to help prevent pollutant from entering streams, sensitive features, and the aquifer.

Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

Project Name: Christ Our King Anglican Church Date Prepared: 6/6/2010

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell.

Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348.

#### Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations f	rom RG-348	Pages 3-27 to 3-30			
Page 3-29 Equation 3.3: L <sub>M</sub> = 27.2(A <sub>N</sub> x P)						
where: $L_{M \text{ TOTAL PROJECT}} = R$ $A_N = R$	Required TSS Net increase i	removal resulting from the propos in impervious area for the project	ed development = 80% of increased load			
Site Data: Determine Required Load Removal Based on the Entire Project County = Total project area included in plan * = Predevelopment impervious area within the limits of the plan * = Total post-development impervious cover fraction * = Total post-development impervious cover fraction * = P =	Comal 22.11 0.42 9.61 0.43 33 8249	acres acres acres inches lbs.				
<ul> <li>* The values entered in these fields should be for the total project area.</li> <li>Number of drainage basins / outfalls areas leaving the plan area =</li> </ul>	5					
2. Drainage Basin Parameters (This information should be provided for each Drainage Basin/Outfall Area No. =	<u>n basin):</u> 1					
Total drainage basin/outfall area = Predevelopment impervious area within drainage basin/outfall area = Post-development impervious area within drainage basin/outfall area = Post-development impervious fraction within drainage basin/outfall area = L <sub>M THIS BASIN</sub> =	2.66 0.00 1.84 0.69 1652	acres acres acres Ibs.				

3. Indicate the proposed BMP Code for this basin.

#### Proposed BMP = Vortechs Removal efficiency = 0 percent

Aqualogic Cartridge Filter Bioretention Contech StormFilter Constructed Wetland Extended Detention Grassy Swale Retention / Irrigation Sand Filter Stormceptor Vegetated Filter Strips Vortechs Wet Basin Wet Vault

#### 4. Calculate Maximum TSS Load Removed (L<sub>B</sub>) for this Drainage Basin by the selected BMP Type.

RG-348 Page 3-33 Equation 3.7:  $L_B = (BMP \text{ efficiency}) \times P \times (A_1 \times 34.6 + A_P \times 0.54)$ 

where:

Ac = Total On-Site	drainage	area	in the	BMP	catchment	area
•						

 $A_i =$  Impervious area proposed in the BMP catchment area

 $A_P$  = Pervious area remaining in the BMP catchment area

L<sub>R</sub> = TSS Load removed from this catchment area by the proposed BMP

A <sub>C</sub> =	4.14	acres
A₁ =	2.88	acres
A <sub>P</sub> =	1.26	acres
L <sub>R</sub> =	0	lbs

#### 5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall area

Desired L<sub>M THIS BASIN</sub> = 3482 lbs.

F = #DIV/0!

6. Calculate Capture Volume required by the BMP Type for this drainage basin / outfall area.

Calculations from RG-348

Pages 3-34 to 3-36

 Rainfall Depth = #DIV/0! inches

 Post Development Runoff Coefficient = 0.50

 On-site Water Quality Volume = #DIV/0!
 cubic feet

Calculations from RG-348 Pages 3-36 to 3-37





Off-site area draining to BMP = Off-site Impervious cover draining to BMP = Impervious fraction of off-site area =	0.00	acres acres	
Off-site Runoff Coefficient = Off-site Water Quality Volume =	0.00 #DIV/0!	cubic feet	
Storage for Sediment =	#DIV/01		
Total Capture Volume (required water quality volume(s) x 1.20) = The following sections are used to calculate the required water quality volu- The values for BMP Types not selected in cell C45 will show NA.	#DIV/0! ume(s) for the	cubic feet selected BMP.	
7. Retention/Irrigation System	Designed as I	Required in RG-348	Pages 3-42 to 3-46
Required Water Quality Volume for retention basin =	NA	cubic feet	
Irrigation Area Calculations:			
Soil infiltration/permeability rate = Irrigation area =	0.1 NA NA	in/hr Ente square feet acres	r determined permeability rate or assumed value of 0.1
8. Extended Detention Basin System	Designed as I	Required in RG-348	Pages 3-46 to 3-51
Required Water Quality Volume for extended detention basin =	: NA	cubic feet	
9. Filter area for Sand Filters	Designed as I	Required in RG-348	Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration System			
Water Quality Volume for sedimentation basin =	- NA	cubic feet	
Minimum filter basin area =	= NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	= NA = NA	square feet For square feet For	minimum water depth of 2 feet maximum water depth of 8 feet
9B. Partial Sedimentation and Filtration System			
Water Quality Volume for combined basins =	NA .	cubic feet	
Minimum filter basin area =	= NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	= NA = NA	square feet For square feet For	minimum water depth of 2 feet maximum water depth of 8 feet

10. Bioretention System	Designed	as Required in R	G-348	Pages 3-63 to 3-65
Required Water Quality Volume for Bioretention Basin	= <b>NA</b>	cubic feet		
11. Wet Basins	Designed	as Required in R	G-348	Pages 3-66 to 3-71
Required capacity of Permanent Pool Required capacity at WQV Elevation	= NA = NA	cubic feet cubic feet	Permanent I Total Capac plus a seco	Pool Capacity is 1.20 times the WQV ity should be the Permanent Pool Capacity nd WQV.
12. Constructed Wetlands	Designed	as Required in R	G-348	Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands	= NA	cubic feet		
13. AquaLogic <sup>™</sup> Cartridge System	Designed	as Required in R	G-348	Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the require	d 20% incr	ease with mainte	nance contra	ct with AquaLogic <sup>™</sup> .
Required Sedimentation chamber capacity Filter canisters (FCs) to treat WQV Filter basin area ( $RIA_F$ )	= NA = NA = NA	cubic feet cartridges square feel	t	
14. Stormwater Management StormFilter® by CONTECH				
Required Water Quality Volume for Contech StormFilter System	= NA	cubic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPs / LOAD REMO	VALS ARE	BASED UPON F	LOW RATES	- NOT CALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designed	l as Required in R	G-348	Pages 3-51 to 3-54
Design parameters for the swale:				
Drainage Area to be Treated by the Swale = A Impervious Cover in Drainage Area Rainfall intensity = i Swale Slope Side Slope (z) Design Water Depth = y Weighted Runoff Coefficient = C		8.00 acres 4.00 acres 1.1 in/hr 0.01 ft/ft 3 0.33 ft 0.54		
A <sub>CS</sub> = cross-sectional area of flow in Swale	=	13.17 sf		

~

P <sub>w</sub> = Wetted Perimeter =	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

#### 15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = \underline{1.49} A_{CS} R_{H}^{23} S^{0.5}$$
  
n  
 $b = \underline{0.134 \times Q}_{y^{1.67}} - zy = 38.51$   
 $Q = CiA = 4.71$   
To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) = Q/A<sub>CS</sub> = 0.36 ft/sec

#### To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

feet

cfs

15B.	Alternative Method using Excel Solver				To solve for bottom v Excel can simultanec The required "Swale
	Design Q = CiA =	4.71 cfs			
					First, highlight Cell F.
	Manning's Equation Q =	0.76 cfs	Error 1 =	3.95	Then click on "Tools"
	Swale Width=	6.00 ft			The value in the "Set
					The value in the "By "
					Click on solve.
	Instructions are provided to the right (green comments).				
					The resulting "Swale
					If the resulting "Swal
	Flow Velocity	0.36 ft/s			
	Minimum Length =	107.24 ft			If there is not the opti
					Click on "Tools" and
	instructions are provided to the right (blue comments).				Then proceed as inst
	Design Width -	6.#			If you would like to in
	Design Vildin =		Error 0	2.05	Freel can simultanee
	Design Discharge =	0.22 #		3.95	Excer can simulated
	Design Depth =	0.33 π			The required "Design

Flow Velocity =	0.3	2 cfs			
Minimum Length =	97.4	-8 ft			First set the desired I Highlight Cell F232.
If any of the resulting values do not meet the design requirement set forth in	1 RG-348, the	e design para	meters may be modifie	d and the solver rerun.	OI' 1
If any of the resulting values still do not meet the design requirement set for	th in RG-348	3, widening th	e swale bottom value r	nay not be possible.	The value in the "Set
16. Vegetated Filter Strips	Designed as	Required in R	G-348 F	Pages 3-55 to 3-57	The value in the "By Click on solve.
There are no calculations required for determining the load or size of vegeta The 80% removal is provided when the contributing drainage area does not of the sheet flow leaving the impervious cover is directed across 15 feet of eng across 50 feet of natural vegetation with a maximum slope of 10%. There can the sheet fill area is a standard to be a standard to b	s or ds 20%.	The resulting "Design If the resulting "Desig First set the desired I Highlight Cell F232. Click on "Toole" and			
If vegetative filter strips are proposed for an interim permanent BMP, they m	hay be sized	as described	on Page 3-56 of HG-34	18.	The value in the "Set
					The value in the "By u
17. Wet Vaults	Designed as	Required in Re	G-348 I	Pages 3-30 to 3-32 & 3-79	Click on solve.
Required Load Removal Based upon Equation 3.3 =	NA	lbs			The resulting "Design If the resulting "Design
First calculate the load removal at 1.1 in/hour					<b>.</b>
RG-348 Page 3-30 Equation 3.4: Q = CiA					
C = runoff coefficient for the drainage area = i = design rainfall intensity = A = drainage area in acres =	0.5 1	52 .1 in/hour 1 acres	C = Runoff Coefficien	$t = 0.546 (IC)^2 + 0.328 (IC) + 0.03$	
Q = flow rate in cubic feet per second =	0.5	57 cubic feet/s	ec		
RG-348 Page 3-31 Equation 3.5: V <sub>OR</sub> = Q/A					
Q = Runoff rate calculated above = A = Water surface area in the wet vault =	0.5 1!	57 cubic feet/s 50 square feet	ec		
_					
V <sub>OR</sub> = Overflow Rate =	0.0	00 feet/sec			
Percent TSS Removal from Figure 3-1 (RG-348 Page 3-31) =	5	53 percent			
Load removed by Wet Vault =	#VALUE!	lbs			
If a bypass occurs at a rainfall intensity of less than 1.1 in/hours Calculate the efficiency reduction for the actual rainfall intensity rate					
Actual Rainfall Intensity at which Wet Vault bypass Occurs =	0	0.5 in/hour			
Fraction of rainfall treated from Figure 3-2 RG-348 Page 3-32 = Efficiency Reduction for Actual Rainfall Intensity =	0.7 0.7	75 percent 83 percent			

Resultant TSS Load removed by Wet Vault =	#VALUEI	lbs		
18. Permeable Concrete	Designed as I	Required in RC	3-348	Pages 3-79 to 3-83
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING Z	ONE			
19. BMPs Installed in a Series	Designed as I	Required in RO	3-348	Pages 3-32
Michael E. Barrett, Ph.D., P.E. recommended that the coeffi	cient for E <sub>2</sub> be	changed fro	m 0.5 to 0.65 on Ma	ay 3, 2006
$E_{TOT} = \{1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))\} \times 100 =$	86.3	8 percent	NET EFFICIENCY	OF THE BMPs IN THE SERIES
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1$ =	75.0	0 percent		
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	- 70.0	0 percent		
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3 =$	= 0.0	0 percent		
THEREFORE, THE NET LOAD REMOVAL WOULD BE: $(A_1 AND A_2 VALUES ARE FROM SECTION 3 ABOVE)$				
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>i</sub> X 34.6 X A <sub>P</sub> X0.54) =	- 2859.7	4 lbs		
20. Stormceptor				
Required TSS Removal in BMP Drainage Area	NA NA	lbs		
Impervious Cover Overtreatment=	= 0.0000	ac		
BMP Sizing	- 0.00	ius.		
Effective Area =	= NA	EA		
<ul> <li>Calculated Model Size(s) = Actual Model Size (if multiple values provided in Calculater</li> </ul>	= #N/A 1			
Model Size or if you are choosing a larger model size) =	= 0	Model Size		
Surface Area =	= #N/A	ft <sup>2</sup>		
Overflow Rate =	= #VALUEI	Vor		
Rounded Overflow Rate =	= #VALUE!	Vor		
BMP Efficiency % =	= #VALUE!	%		
L <sub>R</sub> Value -	= #VALUE!	lbs		
TSS Load Credit -	= #VALUE!	lbs		
Is Sufficient Treatment Available? (TSS Credit $\geq$ TSS Uncapt.	) #VALUEI			
TSS Treatment by BMP (LM + TSS Uncapt.) :	= #VALUEI			

#### 21. Vortech

Required TSS Removal in BMP Drainage Area= Impervious Cover Overtreatment= TSS Removal for Uncaptured Area = BMP Sizing	1651.58 0.0000 0.00	lbs ac lbs
Effective Area = Calculated Model Size(s) =	1.68 Vx1319	EA
Actual Model Size (if choosing larger model size) =	Vx1421	Pick Model Size
Surface Area =	153.90	ħ²
Overflow Rate =	0.012012	V <sub>or</sub>
Rounded Overflow Rate =	0.012500	Vor
BMP Efficiency % =	84.00	%
L <sub>R</sub> Value =	1777.04	lbs
TSS Load Credit =	125.46	lbs
Is Sufficient Treatment Available? (TSS Credit ≥ TSS Uncapt.	) Yes	
TSS Treatment by BMP (LM + TSS Uncapt.) =	1651.58	

Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

Project Name: Christ Our King Anglican Church Date Prepared: 6/6/2010

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell.

Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348.

Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations	from RG-348	Pages 3-27 to 3-30				
Page 3-29 Equation 3.3: L <sub>M</sub> = 27.2(A <sub>N</sub> x P)							
where: $L_{M \text{ TOTAL PROJECT}} = F$ $A_N = N$	$L_{M \text{ TOTAL PROJECT}}$ = Required TSS removal resulting from the proposed development = 80% of increased load $A_N$ = Net increase in impervious area for the project						
P = Average annual precipitation, inches							
Site Data: Determine Required Load Removal Based on the Entire Project County =	Comal						
Total project area included in plan * =	22.11	acres					
Predevelopment impervious area within the limits of the plan * =	0.42	acres					
lotal post-development impervious area within the limits of the plan" =	9.61	acres					
I otal post-development impervious cover fraction " =	0.43	linahaa					
		Inches					
LM TOTAL PROJECT =	8249	lbs.					
* The values entered in these fields should be for the total project area.							
Number of drainage basins / outfalls areas leaving the plan area =	5						
2. Drainage Basin Parameters (This information should be provided for each basin):							
Drainage Basin/Outfall Area No. =	2						
Total drainage basin/outfall area =	3.90	acres					
Predevelopment impervious area within drainage basin/outfall area =	0.00	acres					
Post-development impervious area within drainage basin/outfall area =	2.76	acres					
Post-development impervious fraction within drainage basin/outfall area =	0.71						
L <sub>M THIS</sub> BASIN =	2477	lbs.					
3. Indicate the proposed BMP Code for this basin.							

Proposed BMP = V	/ortechs						
Aemovat efficiency = 4. Calculate Maximum TSS Load Removed (La) for this Drainage Basin by the	0 e selected Bi	AP Type.	Aqualog Bioreten Construc Extende Grassy S Retentio Sand Fil Stormce Vegetate Vortechs Wet Bas Wet Vau	ic Cartridge Filter tion StormFilter Sted Wetland d Detention Swale n / Irrigation ter ptor ed Filter Strips s in			
RG-348 Page 3-33 Equation 3.7: $L_R = (BMP \text{ efficiency}) \times P \times (A_f \times 34.6 + A_P \times 0.54)$							
where: $A_{C} = T$ $A_{I} = h$ $A_{P} = F$ $L_{R} = T$ $A_{C} = A_{I} = A_{P} = L_{R} = L$	Total On-Site of mpervious area Pervious area TSS Load rem <b>3.90</b> <b>2.76</b> <b>1.14</b> <b>0</b>	n-Site drainage area in the BMP catchment area ous area proposed in the BMP catchment area is area remaining in the BMP catchment area ad removed from this catchment area by the proposed BMP 90 acres 76 acres 14 acres 0 lbs					
5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall area							
Desired L <sub>M THIS BASIN</sub> =	3482	lbs.					
F =	#DIV/0!						
6. Calculate Capture Volume required by the BMP Type for this drainage basin / outfall area. Calculations from RG-348 Pages 3-34 to 3-36							
Rainfall Depth = Post Development Runoff Coefficient = On-site Water Quality Volume ≃	#DIV/0! 0.51 #DIV/0!	inches cubic feet					

Calculations from RG-348 Pages 3-36 to 3-37
Off-site area draining to BMP = Off-site Impervious cover draining to BMP = Impervious fraction of off-site area = Off-site Runoff Coefficient = Off-site Water Quality Volume =	0.00 0.00 0 0.00 #DIV/0!	acres acres cubic feet	
Storage for Sediment =	#DIV/0!		
Total Capture Volume (required water quality volume(s) $x = 1.20$ ) = The following sections are used to calculate the required water quality volu The values for BMP Types not selected in cell C45 will show NA.	#DIV/0! ume(s) for the	cubic feet selected BMP.	
7. Retention/Irrigation System	Designed as F	Required in RG-348	Pages 3-42 to 3-46
Required Water Quality Volume for retention basin =	NA	cubic feet	
Irrigation Area Calculations:			
Soil infiltration/permeability rate = irrigation area =	0.1 NA NA	in/hr Enter determined p square feet acres	permeability rate or assumed value of 0.1
8. Extended Detention Basin System	Designed as I	Required in RG-348	Pages 3-46 to 3-51
Required Water Quality Volume for extended detention basin =	NA	cubic feet	
9. Filter area for Sand Filters	Designed as I	Required in RG-348	Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration System			
Water Quality Volume for sedimentation basin =	NA	cubic feet	
Minimum filter basin area =	NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	NA NA	square feet For minimum wate square feet For maximum wate	r depth of 2 feet er depth of 8 feet
9B. Partial Sedimentation and Filtration System			
Water Quality Volume for combined basins =	NA	cubic feet	
Minimum filter basin area =	- NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	NA NA	square feet For minimum wate square feet For maximum wate	er depth of 2 feet er depth of 8 feet

-

10. Bioretention System	Designe	d as Required in F	RG-348	Pages 3-63 to 3-65
Required Water Quality Volume for Bioretention Basir	1= <b>N</b> /	cubic feet		
11. Wet Basins	Designe	d as Required in F	RG-348	Pages 3-66 to 3-71
Required capacity of Permanent Pool Required capacity at WQV Elevation	= N/ = N/	Cubic feet	Permanent Total Capa plus a seco	Pool Capacity is 1.20 times the WQV city should be the Permanent Pool Capacity ond WQV.
12. Constructed Wetlands	Designe	d as Required in I	RG-348	Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands	s = <b>N</b> /	A cubic feet		
13. AquaLogic <sup>TM</sup> Cartridge System	Designe	d as Required in I	RG-348	Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the requir	ed 20% inc	rease with maint	enance contra	act with AquaLogic <sup>™</sup> .
Required Sedimentation chamber capacity Filter canisters (FCs) to treat WO Filter basin area (RIA <sub>F</sub>	y = N/ √ = N/ ) = N/	Acubic feetAcartridgesAsquare feet	et	
14. Stormwater Management StormFilter® by CONTECH				
Required Water Quality Volume for Contech StormFilter System	n = Ni,	cubic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPs / LOAD REM	OVALS AR	E BASED UPON	FLOW RATES	- NOT CALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designe	d as Required in	RG-348	Pages 3-51 to 3-54
Design parameters for the swale:				
Drainage Area to be Treated by the Swale = A Impervious Cover in Drainage Area Rainfall intensity = Swale Slop Side Slope (z Design Water Depth = Weighted Runoff Coefficient = 0	A = a = i = e = y = y = C =	8.00 acres 4.00 acres 1.1 in/hr 0.01 ft/ft 3 0.33 ft 0.54		
A <sub>CS</sub> = cross-sectional area of flow in Swal	e =	13.17 sf		

P <sub>w</sub> = Wetted Perimeter =	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

#### 15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = \underline{1.49} A_{CS} R_{H}^{2/3} S^{0.5}$$
  
n  
 $b = \underline{0.134 \times Q}_{y^{1.67}} S^{0.5}$  -  $zy = 38.51$  feet  
 $Q = CiA = 4.71$  cfs  
To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) =  $Q/A_{CS}$  = 0.36 ft/sec

### To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

cfs

15B.	Alternative	Method	using	Excel	Solver

<ul> <li>A service of laboration</li> <li>County from the instruction</li> </ul>				Excel can simultaneo The required "Swale
Design Q = CiA =	4.71 cfs			
	0.70	E	0.05	First, highlight Cell F
Manning's Equation Q =	0.76 CIS	Error 1 =	3.95	Then click on Tools
	0.00 11			The value in the "By
				Click on solve.
Instructions are provided to the right (green comments).				
				The resulting "Swale
	0.26 #/c			If the resulting "Swal
Minimum Length =	107 24 ft			If there is not the opti
	107.24 1			Click on "Tools" and
Instructions are provided to the right (blue comments).				Then proceed as inst
Desian Width =	6 ft			If you would like to in
Design Discharge =	0.76 cfs	Error 2 =	3.95	Excel can simultaneo
Design Depth =	0.33 ft			The required "Design

To solve for bottom v

	0.32 cfs					
= !	97.48 ft			First set the desired i Highlight Cell F232.		
in RG-348	, the design par	ameters may	be modified and the solver rerun.	Olisk as "Tools" and		
iorth in RG	-348, widening t	he swale both	om value may not be possible.	The value in the "Set		
er Strips Designed as Required in RG-348 Pages 3-55 to 3-57				The value in the "By v Click on solve.		
There are no calculations required for determining the load or size of vegetative filter strips. The 80% removal is provided when the contributing drainage area does not exceed 72 feet (direction of flow) and the sheet flow leaving the impervious cover is directed across 15 feet of engineered filter strips with maximum slope of 20% or across 50 feet of natural vegetation with a maximum slope of 10%. There can be a break in grade as long as no slope exceeds 20%.						
may be si	zed as describe	d on Page 3-5	6 of RG-348.	Click on "Tools" and The value in the "Se		
Designeo	as Required in F	RG-348	Pages 3-30 to 3-32 & 3-79	The value in the "By Click on solve.		
= NA	lbs			The resulting "Design If the resulting "Design		
A						
4	0.54 1.1 in/hour 1 acres	C = Runoff	Coefficient = $0.546 (IC)^2 + 0.328 (IC) + 0.03$			
	0.59 cubic feet/	sec				
A						
=	0.59 cubic feet/ 150 square fee	sec				
~	0.00 feet/sec					
<b>22</b>	53 percent					
= #VALU	UEI Ibs					
=	0.5 in/hour					
	= in RG-348 forth in RG Designed etative filte ot exceed 7 engineered can be a b r may be si Designed = NA A = = A = = A = = = = = = = = = = = = =	<ul> <li>= 0.32 cfs</li> <li>= 97.48 ft</li> <li>a in RG-348, the design paraforth in RG-348, widening to Designed as Required in Fetative filter strips.</li> <li>a texceed 72 feet (direction engineered filter strips with can be a break in grade as reacted as described Designed as Required in Fee NA lbs</li> <li>A lbs<!--</td--><td><ul> <li>= 0.32 cfs</li> <li>= 97.48 ft</li> <li>a in RG-348, the design parameters may forth in RG-348, widening the swale both</li> <li>Designed as Required in RG-348</li> <li>etative filter strips.</li> <li>ot exceed 72 feet (direction of flow) and engineered filter strips with maximum sl can be a break in grade as long as no s</li> <li><i>r</i> may be sized as described on Page 3-5</li> <li>Designed as Required in RG-348</li> <li>= NA Ibs</li> <li>A = 0.54 C = Runoff</li> <li>= 1.1 in/hour</li> <li>= 1 acres</li> <li>= 0.59 cubic feet/sec</li> <li>A = 0.59 cubic feet/sec</li> <li>= 150 square feet</li> <li>= 0.00 feet/sec</li> <li>= 53 percent</li> <li>= #VALUE1 Ibs</li> </ul></td><td><ul> <li>0.32 cfs</li> <li>97.48 ft</li> <li>an RG-348, the design parameters may be modified and the solver rerun. forth in RG-348, widening the swale bottom value may not be possible.</li> <li>Designed as Required in RG-348 Pages 3-55 to 3-57</li> <li>etative filter strips.</li> <li>of exceed 72 feet (direction of flow) and engineered filter strips with maximum slope of 20% or can be a break in grade as long as no slope exceeds 20%.</li> <li>or may be sized as described on Page 3-56 of RG-348.</li> <li>Designed as Required in RG-348 Pages 3-30 to 3-32 &amp; 3-79</li> <li>NA lbs</li> <li>A</li> <li>0.54 C = Runoff Coefficient = 0.546 (IC)<sup>2</sup> + 0.328 (IC) + 0.03</li> <li>1.1 in/hour</li> <li>1 acres</li> <li>0.59 cubic feet/sec</li> <li>35 percent</li> <li>9.00 feet/sec</li> <li>53 percent</li> <li>#VALUE! lbs</li> </ul></td></li></ul>	<ul> <li>= 0.32 cfs</li> <li>= 97.48 ft</li> <li>a in RG-348, the design parameters may forth in RG-348, widening the swale both</li> <li>Designed as Required in RG-348</li> <li>etative filter strips.</li> <li>ot exceed 72 feet (direction of flow) and engineered filter strips with maximum sl can be a break in grade as long as no s</li> <li><i>r</i> may be sized as described on Page 3-5</li> <li>Designed as Required in RG-348</li> <li>= NA Ibs</li> <li>A = 0.54 C = Runoff</li> <li>= 1.1 in/hour</li> <li>= 1 acres</li> <li>= 0.59 cubic feet/sec</li> <li>A = 0.59 cubic feet/sec</li> <li>= 150 square feet</li> <li>= 0.00 feet/sec</li> <li>= 53 percent</li> <li>= #VALUE1 Ibs</li> </ul>	<ul> <li>0.32 cfs</li> <li>97.48 ft</li> <li>an RG-348, the design parameters may be modified and the solver rerun. forth in RG-348, widening the swale bottom value may not be possible.</li> <li>Designed as Required in RG-348 Pages 3-55 to 3-57</li> <li>etative filter strips.</li> <li>of exceed 72 feet (direction of flow) and engineered filter strips with maximum slope of 20% or can be a break in grade as long as no slope exceeds 20%.</li> <li>or may be sized as described on Page 3-56 of RG-348.</li> <li>Designed as Required in RG-348 Pages 3-30 to 3-32 &amp; 3-79</li> <li>NA lbs</li> <li>A</li> <li>0.54 C = Runoff Coefficient = 0.546 (IC)<sup>2</sup> + 0.328 (IC) + 0.03</li> <li>1.1 in/hour</li> <li>1 acres</li> <li>0.59 cubic feet/sec</li> <li>35 percent</li> <li>9.00 feet/sec</li> <li>53 percent</li> <li>#VALUE! lbs</li> </ul>		

Resultant TSS Load removed by Wet Vault = #VALUE! Ibs

18. Permeable Concrete	Designed as F	Required in RG-	-348 Pages 3-79 to 3-83				
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING ZONE							
19. BMPs Installed in a Series	Designed as F	Required in RG	-348 Pages 3-32				
Michael E. Barrett, Ph.D., P.E. recommended that the coeffic	cient for E <sub>2</sub> be	changed from	1 0.5 to 0.65 on May 3, 2006				
$E_{TOT} = [1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))] \times 100 =$	86.38	3 percent	NET EFFICIENCY OF THE BMPS IN THE SERIES				
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1$ =	75.00	) percent					
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	70.00	) percent					
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3 =$	0.00	) percent					
THEREFORE, THE NET LOAD REMOVAL WOULD BE: $(A_i \text{ AND } A_P \text{ VALUES ARE FROM SECTION 3 ABOVE})$							
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>I</sub> X 34.6 X A <sub>P</sub> X0.54) =	2739.54	4 lbs					
20. Stormceptor							
Required TSS Removal in BMP Drainage Area=	NA	lbs					
Impervious Cover Overtreatment=	0.0000	ac					
BMP Sizing	0.00	IDS					
Effective Area =	NA	EA					
Calculated Model Size(s) =	#N/A						
Actual Model Size (if multiple values provided in Calculated							
Model Size or if you are choosing a larger model size) =	. 0	Model Size					
Surface Area =	#N/A	ft <sup>2</sup>					
Overflow Rate =	#VALUE!	Vor					
Rounded Overflow Rate =	#VALUE!	Vor					
BMP Efficiency % =	#VALUE!	%					
L <sub>R</sub> Value =	#VALUE!	lbs					
TSS Load Credit =	#VALUE!	lbs					
Is Sufficient Treatment Available? (TSS Credit $\geq$ TSS Uncapt.)	#VALUE!						
TSS Treatment by BMP (LM + TSS Uncapt.) =	#VALUE!	•1					

## 21. Vortech

BMP Sizing	Required TSS Removal in BMP Drainage Area= Impervious Cover Overtreatment= TSS Removal for Uncaptured Area =	2477.38 0.0000 0.00	lbs ac ibs
	Effective Area = Calculated Model Size(s) = A	2.52 rea Too Larc	EA
		-	
Ad	ctual Model Size (if choosing larger model size) =	Vx1421	Pick Model Size
	Surface Area =	153.90	ft <sup>2</sup>
	Overflow Rate =	0.017999	Vor
	Rounded Overflow Rate =	0.018300	V <sub>or</sub>
	BMP Efficiency % =	76.00	%
	L <sub>R</sub> Value =	2410.48	lbs
	TSS Load Credit =	-66.90	lbs
Is Sufficient T	reatment Available? (TSS Credit   TSS Uncapt.)	No	
	TSS Treatment by BMP (LM + TSS Uncapt.) =	NA	

Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

Project Name: Christ Our King Anglican Church Date Prepared: 6/6/2010

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell.

Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348.

Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project: Ca		Calculations f	rom RG-348	Pages 3-27 to 3-30		
	Page 3-29 Equation 3.3: $L_M = 2$	27.2(A <sub>N</sub> x P)				
where: $L_{M TOTAL PROJECT} = Required TSS removal resulting from the proposed development = 80% of increased load A_N = Net increase in impervious area for the projectP = Average annual precipitation, inches$						
Site Data: Determine Re Predevelopme Total post-developm Total	equired Load Removal Based on the Entire Project County = Total project area included in plan * = ent impervious area within the limits of the plan* = tal post-development impervious cover fraction * = P =	Comal 22.11 0.42 9.61 0.43 33	acres acres acres inches			
* The values entered in the	L <sub>M TOTAL PROJECT</sub> = se fields should be for the total project area.	8249	lbs.			
Number of drain	age basins / outfalls areas leaving the plan area =	5				
2. Drainage Basin Paramete	rs (This information should be provided for each	<u>n basin):</u>				
	Drainage Basin/Outfall Area No. =	3				
Predevelopment ir Post-development ir Post-development impe	Total drainage basin/outfall area = npervious area within drainage basin/outfall area = npervious area within drainage basin/outfall area = ervious fraction within drainage basin/outfall area = L <sub>M THIS BASIN</sub> =	1.98 0.12 0.85 0.43 655	acres acres acres Ibs.			

3. Indicate the proposed BMP Code for this basin.

#### Proposed BMP = Vortechs Removal efficiency = 0 percent

Aqualogic Cartridge Filter Bioretention Contech StormFilter Constructed Wetland Extended Detention Grassy Swale Retention / Irrigation Sand Filter Stormceptor Vegetated Filter Strips Vortechs Wet Basin Wet Vault

#### 4. Calculate Maximum TSS Load Removed (L<sub>B</sub>) for this Drainage Basin by the selected BMP Type.

RG-348 Page 3-33 Equation 3.7: L<sub>B</sub> = (BMP efficiency) x P x (A<sub>1</sub> x 34.6 + A<sub>P</sub> x 0.54)

where:

A <sub>c</sub> = Total On-Site drainage area in the BMP ca						
A <sub>1</sub> = Impervious area proposed in the BMP catchment area						
$A_P = Pe$	ervious are	a remaining in the BMP catchment area				
$L_{R} = TS$	SS Load re	moved from this catchment area by the proposed BMP				
A <sub>C</sub> =	4.14	acres				
$A_i =$	2.88	acres				
A <sub>P</sub> =	1.26	acres				
L <sub>R</sub> =	0	lbs				

#### 5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall area

- Desired L<sub>M THIS BASIN</sub> = 3482 lbs.
  - F = #DIV/0!

6. Calculate Capture Volume required by the BMP Type for this drainage basin / outfall area.

Calculations from RG-348

Pages 3-34 to 3-36

Rainfall Depth =#DIV/0!inchesPost Development Runoff Coefficient =0.50On-site Water Quality Volume =#DIV/0!cubic feet

Calculations from RG-348 Pages 3-36 to 3-37

Off-site area draining to B Off-site Impervious cover draining to B Impervious fraction of off-site a Off-site Runoff Coeffic Off-site Water Quality Volu	BMP = BMP = area = ient = ume =	0.00 0.00 0 0.00 #DIV/0!	acres acres cubic feet	
Storage for Sedim	nent =	#DIV/0!		
Total Capture Volume (required water quality volume(s) x 1	.20) =	#DIV/0!	cubic feet	
The following sections are used to calculate the required water quality	y volu	me(s) for the	selected BMI	Ρ.
7. Retention/Irrigation System		Designed as F	Required in B(	3-348 Pages 3-42 to 3-46
		Designed us i		
Required Water Quality Volume for retention be	asin =	NA	cubic feet	
Irrigation Area Calculations:				
Soil infiltration/permeability Irrigation a	rate = area =	0.1 NA NA	in/hr square feet acres	Enter determined permeability rate or assumed value of 0.1
8. Extended Detention Basin System		Designed as F	Required in R	G-348 Pages 3-46 to 3-51
Required Water Quality Volume for extended detention b	asin =	NA	cubic feet	
9. Filter area for Sand Filters		Designed as F	Required in R	G-348 Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration System				
Water Quality Volume for sedimentation b	asin =	NA	cubic feet	
Minimum filter basin a	area =	NA	square feet	
Maximum sedimentation basin a Minimum sedimentation basin a	area = area =	NA NA	square feet square feet	For minimum water depth of 2 feet For maximum water depth of 8 feet
9B. Partial Sedimentation and Filtration System				
Water Quality Volume for combined ba	sins =	NA	cubic feet	
Minimum filter basin a	area =	NA	square feet	
Maximum sedimentation basin a Minimum sedimentation basin a	area = area =	NA NA	square feet square feet	For minimum water depth of 2 feet For maximum water depth of 8 feet

10. Bioretention System	Designed	I as Required in R	IG-348	Pages 3-63 to 3-65
Required Water Quality Volume for Bioretention Basin	= NA	cubic feet		
11. Wet Basins	Designed	l as Required in R	G-348	Pages 3-66 to 3-71
Required capacity of Permanent Pool = Required capacity at WQV Elevation =	- NA - NA	cubic feet cubic feet	Permanent F Total Capaci plus a secor	Pool Capacity is 1.20 times the WQV ity should be the Permanent Pool Capacity ad WQV.
12. Constructed Wetlands	Designed	I as Required in R	IG-348	Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands	= NA	cubic feet		
13. AguaLogic <sup>TM</sup> Cartridge System	Designed	as Required in F	IG-348	Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the required	d 20% incr	ease with mainte	enance contrac	et with AquaLogic <sup>™</sup> .
Required Sedimentation chamber capacity Filter canisters (FCs) to treat WQV Filter basin area (RIA <sub>F</sub> )	= NA = NA = NA	cubic feet cartridges square fee	t	
14. Stormwater Management StormFilter® by CONTECH				
Required Water Quality Volume for Contech StormFilter System	= NA	cubic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPs / LOAD REMO	VALS ARE	BASED UPON F	LOW RATES	NOT CALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designe	d as Required in F	1G-348	Pages 3-51 to 3-54
Design parameters for the swale:				
Drainage Area to be Treated by the Swale = A Impervious Cover in Drainage Area Rainfail intensity = i Swate Slope Side Slope (z) Design Water Depth = y Weighted Runoff Coefficient = C		8.00 acres 4.00 acres 1.1 in/hr 0.01 ft/ft 3 0.33 ft 0.54		
A <sub>CS</sub> = cross-sectional area of flow in Swale	=	13.17 sf		

P <sub>w</sub> = Wetted Perimeter =	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

#### 15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = 1.49 A_{CS} R_{H}^{2/3} S^{0.5}$$
  
n  
 $b = \frac{0.134 \times Q}{y^{1.67} S^{0.5}} - zy = 38.51$  feet  
 $Q = CiA = 4.71$  cfs

To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) =  $Q/A_{CS}$  = 0.36 ft/sec

#### To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

15B.	Alternative Method using Excel Solver			To solve for bottom v Excel can simultaneo The required "Swale
	Design Q = CiA =	4.71 cfs		
				First, highlight Cell F.
	Manning's Equation Q =	0.76 cfs	Error 1 = 3	.95 Then click on "Tools"
	Swale Width=	6.00 ft		The value in the "Set
				The value in the "By the Click on solve
	Instructions are provided to the right (green comments)			Click off solve.
				The resulting "Swale
				If the resulting "Swal
	Flow Velocity	0.36 ft/s		
	Minimum Length =	107.24 ft		If there is not the opti
				Click on "Tools" and
	Instructions are provided to the right (blue comments).			Then proceed as inst
	Design Width =	6 ft		If you would like to in
	Design Discharge =	0.76 cfs	Error 2 = 3	.95 Excel can simultaneo
	Design Depth =	0.33 ft		The required "Design

	Flow Velocity =	0.32 cfs			
	Minimum Length =	97.48 ft			First set the desired I Highlight Cell E232
If any of the resulting values do not meet the design rea	quirement set forth in R	G-348, the design	parameters may be	modified and the solver rerun.	
If any of the resulting values still do not meet the desig	n requirement set forth	in RG-348, widen	ing the swale botton	n value may not be possible.	Click on "Tools" and The value in the "Set
16. Vegetated Filter Strips	Des	signed as Required	d in RG-348	Pages 3-55 to 3-57	The value in the "By Click on solve.
There are no calculations required for determining the The 80% removal is provided when the contributing dra the sheet flow leaving the impervious cover is directed across 50 feet of natural vegetation with a maximum sh	e of 20% or be exceeds 20%.	The resulting "Design If the resulting "Desig First set the desired I Highlight Cell F232.			
If vegetative filter strips are proposed for an interim pe	rmanent BMP, they may	be sized as desc	ribed on Page 3-56	of RG-348.	Click on "Tools" and The value in the "Set
17. Wet Vaults	Des	signed as Require	d in RG-348	Pages 3-30 to 3-32 & 3-79	The value in the "By Click on solve.
Required Load Removal Based	upon Equation 3.3 =	NA Ibs			The resulting "Design If the resulting "Desig
First calculate the load removal at 1.1 in/hour					naak maasaan to ahaanaa kaabad kad ma
RG-348 Page 3-30 E	quation 3.4: Q = CiA				
C = runoff coefficient fo i = des A = dra	r the drainage area = ign rainfall intensity = inage area in acres =	0.27 1.1 in/hou 1 acres	C = Runoff Co ar	oefficient = 0.546 (IC) <sup>2</sup> + 0.328 (IC) + 0.03	
Q = flow rate in cu	bic feet per second =	0.30 cubic	feet/sec		
RG-348 Page 3-31 Equ	ation 3.5: V <sub>OR</sub> = Q/A				
Q = Runoff ra A = Water surface a	te calculated above = rea in the wet vault =	0.30 cubic 150 squai	feet/sec e feet		
v	<sub>on</sub> = Overflow Rate =	0.00 feet/s	ec		
Percent TSS Removal from Figure 3-1 (	RG-348 Page 3-31) =	53 perce	nt		
Load ren	noved by Wet Vault =	#VALUE! Ibs			
If a bypass occurs at a rainfall intensity of less than 1.1 Calculate the efficiency reduction for the actual rainfall	in/hours intensity rate				
Actual Rainfall Intensity at which Wet V	ault bypass Occurs =	0.5 in/ho	Jr		
Fraction of rainfall treated from Figure 3-2 Efficiency Reduction for Actu	RG-348 Page 3-32 = al Rainfall Intensity =	0.75 perce 0.83 perce	ent ent		

			0.49	Decce 2 70 to 2 82		
18. Permeable Concrete	Designed as He	equirea in Ro	a-348	Pages 3-79 10 3-03		
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING ZONE						
19. BMPs Installed in a Series	Designed as Re	equired in RC	à-348	Pages 3-32		
Michael E. Barrett, Ph.D., P.E. recommended that the coeffic	ient for E <sub>2</sub> be c	changed fro	m 0.5 to 0.65 on May	/ 3, 2006		
$E_{TOT} = [1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))] \times 100 =$	86.3 <b>8</b>	percent	NET EFFICIENCY (	OF THE BMPs IN THE SERIES		
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1 =$	75.00	percent				
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	70.00	percent				
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3 =$	0.00	percent				
THEREFORE, THE NET LOAD REMOVAL WOULD BE: $(A_1 \text{ AND } A_P \text{ VALUES ARE FROM SECTION 3 ABOVE})$						
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>I</sub> X 34.6 X A <sub>P</sub> X0.54) =	2859.74	lbs				
20. Stormceptor						
Required TSS Removal in BMP Drainage Area=	NA	lbs				
Impervious Cover Overtreatment=	0.0000	ac				
BMP Sizing	0.00	IDS				
Effective Area =	NA	EA				
Calculated Model Size(s) =	#N/A					
Actual Model Size (if multiple values provided in Calculated						
Model Size or if you are choosing a larger model size) =	0	Model Size				
Surface Area =	#N/A	ft <sup>2</sup>				
Overflow Rate =	#VALUE!	Vor				
Rounded Overflow Rate =	#VALUE!	Vor				
BMP Efficiency % =	#VALUE!	%				
L <sub>R</sub> Value =	#VALUE!	lbs				
TSS Load Credit =	#VALUE!	lbs				
Is Sufficient Treatment Available? (TSS Credit > TSS Uncapt.)	#VALUE!					
TSS Treatment by BMP (LM + TSS Uncapt.) =	#VALUE!					

Resultant TSS Load removed by Wet Vault = #VALUE! Ibs

AOUGCII				
		Required TSS Removal in BMP Drainage Area= Impervious Cover Overtreatment= TSS Removal for Uncaptured Area =	<b>655.25</b> 0.0800 71.81	lbs ac Ibs
	BMP Sizing	Effective Area = Calculated Model Size(s) =	0.80 Vx9000	EA
	A	ctual Model Size (if choosing larger model size) =	Vx16000	Pick Model Size
		Surface Area =	113.10	ft <sup>2</sup>
		Overflow Rate =	0.007770	V <sub>or</sub>
		Rounded Overflow Rate =	0.007800	Vor
		BMP Efficiency % =	90.00	%
		L <sub>R</sub> Value =	891.60	lbs
		TSS Load Credit =	236.35	lbs
	Is Sufficient	Treatment Available? (TSS Credit > TSS Uncapt.)	Yes	
		TSS Treatment by BMP (LM + TSS Uncapt.) =	727.06	

.

# 21. Vortech



Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

Project Name: Christ Our King Anglican Church Date Prepared: 6/6/2010

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell.

Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348.

## Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations fi	rom RG-348	Pages 3-27 to 3-30
Page 3-29 Equation 3.3: $L_M = 2$	27.2(A <sub>N</sub> x P)		
where:	Required TSS	removal resulting from the p	proposed development = 80% of increased load
P =	Average annu	al precipitation, inches	
	inologo anna		
Site Data: Determine Required Load Removal Based on the Entire Project			
County =	Comal		
Total project area included in plan * =	22.10	acres	
Predevelopment impervious area within the limits of the plan * =	0.42	acres	
Total post-development impervious area within the limits of the plan* =	9.61	acres	
Total post-development impervious cover fraction * =	0.43		
P =[	33	inches	
LM TOTAL PROJECT =	8249	lbs.	
* The values entered in these fields should be for the total project area.			
Number of drainage basins / outfalls areas leaving the plan area =	5		
2. Drainage Basin Parameters (This information should be provided for each	n basin):		
Drainage Basin/Outfall Area No. =	4		
Total drainage basin/outfall area =	1.98	acres	
Predevelopment impervious area within drainage basin/outfall area =	0.00	acres	
Post-development impervious area within drainage basin/outfall area =	1.40	acres	
Post-development impervious fraction within drainage basin/outfall area =	0.71		
L <sub>M THIS BASIN</sub> =	1257	lbs.	
3. Indicate the proposed BMP Code for this basin.			

Proposed BMP	e = Vortechs	porcont		
4. Calculate Maximum TSS Load Removed (L <sub>R</sub> ) for this Drainage Basin by	y = U y the selected BM	<u>MP Type.</u>	Aqualogic Bioretentic Contech S Constructe Extended Grassy Sw Retention Sand Filte Stormcept Vegetated Vortechs Wet Basin Wet Vault	Cartridge Filter in tormFilter id Wetland Detention vale / Irrigation r or Filter Strips
RG-348 Page 3-33 Equation 3.7: L <sub>R</sub>	<sub>R</sub> = (BMP efficienc	y) x P x (A <sub>1</sub> x	34.6 + A <sub>P</sub> x 0.54)	
where: A <sub>c</sub> A A <sub>p</sub> L <sub>p</sub> A <sub>c</sub> A A <sub>p</sub> L <sub>p</sub>	$c_{P} = \text{Total On-Site } c_{P} = \text{Impervious area}$ $c_{P} = \text{Pervious area}$ $c_{R} = \text{TSS Load rem}$ $c_{P} = 1.40$ $c_{P} = 0.58$ $c_{R} = 0$	drainage area a proposed in remaining in oved from thi acres acres acres lbs	in the BMP catchment area h the BMP catchment area he BMP catchment area s catchment area by the proposed	і ВМР
5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfa	all area			
Desired L <sub>M THIS BASIN</sub>	N = 3482 F = #DIV/0!	lbs.		
6. Calculate Capture Volume required by the BMP Type for this drainage	basin / outfall ar	<u>ea.</u>	Calculations from RG-348	Pages 3-34 to 3-36
Rainfall Dept Post Development Runoff Coefficient On-site Water Quality Volume	h = #DIV/0! t = 0.51 e = #DIV/0!	inches cubic feet		

Calculations from RG-348 Pages 3-36 to 3-37

Off-site area draining to BMP = Off-site Impervious cover draining to BMP = Impervious fraction of off-site area =	0.00	acres acres	
Off-site Water Quality Volume =	#DIV/0!	cubic feet	
Storage for Sediment =	#DIV/0!	aubic fact	
The following sections are used to calculate the required water quality volume(s) x 1.20) =	ume(s) for the	selected BMP.	
7. Retention/Irrigation System	Designed as	Required in RG-3	348         Pages 3-42 to 3-46
Required Water Quality Volume for retention basin =	• <b>NA</b>	cubic feet	
Irrigation Area Calculations:			
Soil infiltration/permeability rate = Irrigation area =	= 0.1 = NA NA	in/hr E square feet acres	Enter determined permeability rate or assumed value of 0.1
8. Extended Detention Basin System	Designed as	Required in RG-3	348 Pages 3-46 to 3-51
Required Water Quality Volume for extended detention basin =	= NA	cubic feet	
9. Filter area for Sand Filters	Designed as	Required in RG-3	348 Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration System			
Water Quality Volume for sedimentation basin =	= <b>NA</b>	cubic feet	
Minimum filter basin area =	= NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	= NA = NA	square feet F square feet F	For minimum water depth of 2 feet For maximum water depth of 8 feet
9B. Partial Sedimentation and Filtration System			
Water Quality Volume for combined basins =	= NA	cubic feet	
Minimum filter basin area =	= NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	= NA = NA	square feet F square feet F	For minimum water depth of 2 feet For maximum water depth of 8 feet

10. Eloretention System	Designe	d as Required in R	G-348	Pages 3-63 to 3-65
Required Water Quality Volume for Bioretention Basin	= N/	cubic feet		
11. Wet Basins	Designe	d as Required in Re	G-348	Pages 3-66 to 3-71
Required capacity of Permanent Pool Required capacity at WQV Elevation	= N/ = N/	cubic feet	Permanent Pool Cap Total Capacity shoul plus a second WQV.	acity is 1.20 times the WQV Id be the Permanent Pool Capacity
12. Constructed Wetlands	Designe	d as Required in Re	G-348	Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands	= N/	cubic feet		
13. AquaLogic <sup>™</sup> Cartridge System	Designe	d as Required in R	G-348	Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the require	ed 20% inc	rease with mainte	nance contract with A	quaLogic <sup>™</sup> .
Required Sedimentation chamber capacity Filter canisters (FCs) to treat WQV Filter basin area (RIA <sub>F</sub> )	= N/ = N/ = N/	A cubic feet A cartridges A square feet		
14. Stormwater Management StormFilter® by CONTECH				
Required Water Quality Volume for Contech StormFilter System	= N/	cubic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPS / LOAD REMO	OVALS AR	E BASED UPON F	OW RATES - NOT CA	ALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designe	d as Required in R	G <b>-34</b> 8	Pages 3-51 to 3-54
Design parameters for the swale:				
Drainage Area to be Treated by the Swale = A Impervious Cover in Drainage Area Rainfall intensity = i Swale Slope Side Slope (z) Design Water Depth = y Weighted Runoff Coefficient = C		8.00 acres 4.00 acres 1.1 in/hr 0.01 ft/ft 3 0.33 ft 0.54		
A <sub>CS</sub> = cross-sectional area of flow in Swale	=	13.17 sf		

P <sub>w</sub> = Wetted Perimeter =	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = 1.49 A_{CS} R_{H}^{2/3} S^{0.5}$$
  
n  
 $b = 0.134 x Q_{H}^{2/3} - zy = 38.51$  feet  
 $y^{1.67} S^{0.5}$   
 $Q = CiA = 4.71$  cfs

To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) =  $Q/A_{CS}$  = 0.36 ft/sec

#### To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

15B.	Alternative Method using Excel Solver				To solve for bottom v Excel can simultaneo The required "Swale
	Design Q = CiA =	4.71 cfs			
					First, highlight Cell F.
	Manning's Equation Q =	0.76 cfs	Error 1 =	3.95	Then click on "Tools"
	Swale Width=	6.00 ft			The value in the "Set
					The value in the "By (
					Click on solve.
	Instructions are provided to the right (green comments).				
					The resulting "Swale If the resulting "Swal
	Flow Velocity	0.36 tt/s			
	Minimum Length =	107.24 ft			If there is not the opti
	-				Click on "Tools" and
	Instructions are provided to the right (blue comments).				Then proceed as inst
	Design Width =	6 ft			If you would like to in
	Design Discharge =	0.76 cfs	Error 2 =	3.95	Excel can simultaneo
	Design Depth =	0.33 ft			The required "Design



Flow Velocity = Minimum Length =	0.32 cfs 97.45 ft			First set the desired I Highlight Cell F232.
If any of the resulting values do not meet the design requirement set forth in If any of the resulting values still do not meet the design requirement set for	RG-348, the design pa th in RG-348, widening	rameters may be moo the swale bottom val	lified and the solver rerun. ue may not be possible.	Click on "Tools" and The value in the "Set
16. Vegetated Filter Strips	Designed as Required in	RG-348	Pages 3-55 to 3-57	The value in the "By I Click on solve.
There are no calculations required for determining the load or size of vegeta The 80% removal is provided when the contributing drainage area does not of the sheet flow leaving the impervious cover is directed across 15 feet of eng across 50 feet of natural vegetation with a maximum slope of 10%. There ca If vegetative filter strips are proposed for an interim permanent RMP, they may	The resulting "Design If the resulting "Design First set the desired I Highlight Cell F232. Click on "Tools" and			
n vegetative inter strips are proposed for all interim permanent bmr, they in	ay be sized as describ	Ed off Fage 5-50 of fic		The value in the "Set
17. Wet Vaults	Designed as Required in	RG-348	Pages 3-30 to 3-32 & 3-79	Click on solve.
Required Load Removal Based upon Equation 3.3 =	NA Ibs			The resulting "Design If the resulting "Design
First calculate the load removal at 1.1 in/hour				
RG-348 Page 3-30 Equation 3.4: Q = CiA				
C = runoff coefficient for the drainage area = i = design rainfall intensity = A = drainage area in acres =	0.53 1.1 in/hour 1 acres	C = Runoff Coeffic	cient = 0.546 (IC) <sup>2</sup> + 0.328 (IC) + 0.03	
Q = flow rate in cubic feet per second =	0.59 cubic fee	v/sec		
RG-348 Page 3-31 Equation 3.5: V <sub>OR</sub> = Q/A				
Q = Runoff rate calculated above = A = Water surface area in the wet vault =	0.59 cubic fee 150 square fe	t/sec eet		
V <sub>OR</sub> = Overflow Rate =	0.00 feet/sec			
Percent TSS Removal from Figure 3-1 (RG-348 Page 3-31) =	53 percent			
Load removed by Wet Vault =	#VALUEI Ibs			
If a bypass occurs at a rainfall intensity of less than 1.1 in/hours Calculate the efficiency reduction for the actual rainfall intensity rate				
Actual Rainfall Intensity at which Wet Vault bypass Occurs =	0.5 in/hour			
Fraction of rainfall treated from Figure 3-2 RG-348 Page 3-32 = Efficiency Reduction for Actual Rainfall Intensity =	0.75 percent 0.83 percent			

Resultant TSS Load removed by Wat Vault	= #VALUE!	lbs		
18. Permeable Concrete	Designed as I	Required in RG	A-348 Pages 3-79 to 3-83	
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING 2	ONE			
19. BMPs Installed in a Series	Designed as I	Required in RG	à-348 Pages 3-32	
Michael E. Barrett, Ph.D., P.E. recommended that the coeff	icient for E <sub>2</sub> be	e changed from	m 0.5 to 0.65 on May 3, 2006	
$E_{TOT} = [1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))] \times 100$	= 86.3	8 percent	NET EFFICIENCY OF THE BMPs IN THE SERIES	
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1$	= 75.0	0 percent		
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$	= 70.0	10 percent		
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3$	= 0.0	0 percent		
THEREFORE, THE NET LOAD REMOVAL WOULD BE: $(A_1 \text{ AND } A_P \text{ VALUES ARE FROM SECTION 3 ABOVE})$				
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>i</sub> X 34.6 X A <sub>P</sub> X0.54)	= 1389.6	i5 lbs		
20. Stormceptor		the e		
Impensious Cover Overtreatment	= NA - 0.0000	105		
TSS Removal for Lincantured Area	- 0.000	lbs		
BMP Sizing	- 0.00	100		
Effective Area	= NA	EA		
Calculated Model Size(s)	= #N/A			
Actual Model Size (if multiple values provided in Calculate	d			
Model Size or if you are choosing a larger model size)	= 0	Model Size		
Surface Area	= #N/A	ft <sup>2</sup>		
Overflow Rate	= #VALUE!	Vor		
Rounded Overflow Rate	= #VALUE!	Vor		
BMP Efficiency %	= #VALUE	%		
L <sub>B</sub> Value	= #VALUEI	lbs		
		100		
TSS Load Credit	= #VALUE!	IDS		
Is Sufficient Treatment Available? (TSS Credit > TSS Uncapt	.) #VALUE!			
TSS Treatment by BMP (LM + TSS Uncapt.)	= #VALUE!			

lbs ac Ibs	1256.64 0.0000 0.00	Required TSS Removal in BMP Drainage Area= Impervious Cover Overtreatment= TSS Removal for Uncaptured Area =
EA	1.28 Vx16000	BMP Sizing Effective Area = Calculated Model Size(s) =
Pick Model Size	Vx16000	Actual Model Size (if choosing larger model size) =
ft <sup>2</sup> V <sub>or</sub> % Ibs	113.10 0.012424 0.012500 84.00 1351.44	Surface Area = Overflow Rate = Rounded Overflow Rate = BMP Efficiency % = L <sub>R</sub> Value =
lbs	94.80	TSS Load Credit =
	Yes	Is Sufficient Treatment Available? (TSS Credit   TSS Uncapt.)
	1256.64	TSS Treatment by BMP (LM + TSS Uncapt.) =

# 21. Vortech

# Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

......

			Date Prepared:	6/6/2010
Additional information is provided for cells with a red triangle in t Text shown in blue indicate location of instructions in the Technical Gu Characters shown in red are data entry fields. Characters shown in black (Bold) are calculated fields. Changes	he upper Iidance M to these	right corner. anual - RG-34 fields will rem	Place the curso 3. Hove the equation	r over the cell. ns used in the spreadsheet.
1. The Required Load Reduction for the total project: Ca	dculations fr	om RG-348	P	ages 3-27 to 3-30
Page 3-29 Equation 3.3: $L_M = 27$	.2(A <sub>N</sub> x P)			
where: $L_{M \text{ TOTAL PROJECT}} = Re$ $A_{N} = Ne$ $P = A_{N}$	iquired TSS at increase i verage annu	removal resulting n impervious area al precipitation, ir	) from the proposed o a for the project aches	development = 80% of increased load
Site Data: Determine Required Load Removal Based on the Entire Project County = Total project area included in plan * = Predevelopment impervious area within the limits of the plan * = Total post-development impervious area within the limits of the plan * = Total post-development impervious cover fraction * = P =	Comal 22.10 0.42 9.61 0.43 33	acres acres acres inches		
L <sub>M TOTAL PROJECT</sub> = * The values entered in these fields should be for the total project area.	8249	lbs.		
Number of drainage basins / outfalls areas leaving the plan area =	5			
2. Drainage Basin Parameters (This information should be provided for each t	pasin):			
Drainage Basin/Outfall Area No. =	5			
Total drainage basin/outfall area = Predevelopment impervious area within drainage basin/outfall area = Post-development impervious area within drainage basin/outfall area = Post-development impervious fraction within drainage basin/outfall area =	2.59 0.00 1.88 0.73	acres acres acres		
LIN THIS BASIN	1687	IDS.		

Project Name: Christ Our King Anglican Church

3. Indicate the proposed BMP Code for this basin.

	Proposed BMP = Vo	rtechs			
4. Calculate Maximum TSS Load Removed (La) for this I	Removal efficiency = <u>Drainage Basin by the s</u>	0 selected Bl	percent MP Type.	Ad Bik Co Co Ex Gr Re Sa St Ve Vo W W	ualogic Cartridge Filter oretention ontech StormFilter onstructed Wetland tended Detention assy Swale etention / Irrigation and Filter ormceptor egetated Filter Strips ortechs et Basin et Vault
RG-348 Page 3-3	3 Equation 3.7: L <sub>B</sub> = (Bl	MP efficiend	су) х Р х (А, х	34.6 + A <sub>P</sub> x 0.54)	
where:	$A_{C} = To$ $A_{i} = Im$ $A_{P} = Pe$ $L_{R} = TS$ $A_{C} =$ $A_{i} =$ $A_{P} =$ $L_{R} =$	tal On-Site pervious area S Load ren 1.98 1.40 0.58 0	drainage area ea proposed remaining in noved from th acres acres acres lbs	a in the BMP catchment ar in the BMP catchment area the BMP catchment area is catchment area by the p	ea a xroposed BMP
5. Calculate Fraction of Annual Runoff to Treat the drain	nage basin / outfall are	a			
E	Desired L <sub>M THIS BASIN</sub> =	3482	lbs.		
		#DIV/0!			
6. Calculate Capture Volume required by the BMP Type	for this drainage basin	n / outfall a	rea.	Calculations from RG-34	Pages 3-34 to 3-36
Post Development On-site Wa	Rainfall Depth = Runoff Coefficient = ater Quality Volume =	#DIV/0! 0.51 #DIV/0!	inches cubic feet		

Calculations from RG-348 Pages 3-36 to 3-37



Off-site area draining to BMP = Off-site Impervious cover draining to BMP = Impervious fraction of off-site area = Off-site Runoff Coefficient = Off-site Water Quality Volume =	0.00 0.00 0.00 #DIV/0!	acres acres cubic feet	
Storage for Sediment = Total Capture Volume (required water quality volume(s) x 1.20) = The following sections are used to calculate the required water quality volu The values for BMP Types not selected in cell C45 will show NA. <u>7. Retention/Irrigation System</u>	#DIV/0! #DIV/0! Ime(s) for the Designed as F	cubic feet <b>selected BMF</b> Required in RG	•. 5-348 Pages 3-42 to 3-46
Required Water Quality Volume for retention basin =	NA	cubic feet	
Irrigation Area Calculations:			
Soil infiltration/permeability rate = Irrigation area =	0.1 NA NA	in/hr square feet acres	Enter determined permeability rate or assumed value of 0.1
8. Extended Detention Basin System	Designed as F	Required in RC	3-348 Pages 3-46 to 3-51
Required Water Quality Volume for extended detention basin =	NA	cubic feet	
9. Filter area for Sand Filters	Designed as F	Required in RC	3-348 Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration System			
Water Quality Volume for sedimentation basin =	NA	cubic feet	
Minimum filter basin area =	NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	NA NA	square feet square feet	For minimum water depth of 2 feet For maximum water depth of 8 feet
9B. Partial Sedimentation and Filtration System			
Water Quality Volume for combined basins =	NA	cubic feet	
Minimum filter basin area =	NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	NA NA	square feet square feet	For minimum water depth of 2 feet For maximum water depth of 8 feet

10. Bioretention System	Designed	l as R∈ <sup>-</sup>	d in R	G-348	P <sub>=</sub> ⊖s 3-63 to 3-65
Required Water Quality Volume for Bioretention Basin	= NA	C_	ac feet		
11. Wet Basins	Designed	l as Requ	ared in R	G-348	Pages 3-66 to 3-71
Required capacity of Permanent Pool Required capacity at WQV Elevation	≖ NA = NA	cul	bic feet bic feet	Perma Total ( plus a	nent Pool Capacity is 1.20 times the WQV Capacity should be the Permanent Pool Capacity second WQV.
12. Constructed Wetlands	Designed	l as Requ	ired in R	G-348	Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands	= NA	cu	bic feet		
13. AquaLogic <sup>™</sup> Cartridge System	Designed	l as Requ	ired in R	G-348	Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the require	ed 20% incr	ease with	n mainte	nance o	ontract with AquaLogic <sup>™</sup> .
Required Sedimentation chamber capacity	= NA	Cu	bic feet		
Filter canisters (FCs) to treat WQV	= NA	ca	rtridges		
Filter basin area (HIA <sub>F</sub> )	= NA	sq	uare feet		
14. Stormwater Management StormFilter® by CONTECH					
Required Water Quality Volume for Contech StormFilter System	= NA	u cu	bic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPS / LOAD REMO	OVALS ARE	BASED	UPON F	LOWR	ATES - NOT CALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designed	d as Requ	ired in R	G-348	Pages 3-51 to 3-54
Design parameters for the swale:					
Drainage Area to be Treated by the Swale = $A$	=	8.00 ac	res		
Impervious Cover in Drainage Area	=	4.00 ac	res		
Rainfall intensity = i	=	1.1 in/	'hr H		
Swale Slope Side Slope	=	0.01 10/1	u		
Design Water Depth = v	/=	0.33 ft			
Weighted Runoff Coefficient = C	=	0.54			
A <sub>CS</sub> = cross-sectional area of flow in Swale	) =	13.17 sf			

Surger and the owner of the owner

P <sub>w</sub> = Wetted Perimeter =	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

## 15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = \frac{1.49}{1.49} A_{CS} R_{H}^{-2/3} S^{0.5}$$
  
n  
 $b = \frac{0.134 \times Q}{y^{1.67} S^{0.5}} - zy = 38.51$  feet  
 $Q = CiA = 4.71$  cfs  
To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) =  $Q/A_{CS}$  = 0.36 ft/sec

#### To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

15B.	Alternative Method using Excel Solver				To solve for bottom v Excel can simultaneo The required "Swale
	Design Q = CiA =	4.71 cfs			
					First, highlight Cell F
	Manning's Equation Q =	0.76 cfs	Error 1 =	3.95	Then click on "Tools"
	Swale Width=	6.00 ft			The value in the "Set
					The value in the "By (
					Click on solve.
	instructions are provided to the right (green comments).				The resulting "Swale
					If the resulting "Swale
	Flow Velocity	0.36 ft/s			in the resulting share
	Minimum Lenath =	107.24 ft			If there is not the opti
					Click on "Tools" and
	Instructions are provided to the right (blue comments).				Then proceed as inst
	Design Width -	6 H			If you would like to in
	Design Width =	0.76.cfs	Error 2 m	2.05	Fixed can simultaneo
	Design Discharge =	0.33 ft		5.95	The required "Design
	Design Depin =	0.00 ft			The required Design

Flow Velocity =	0.3	32 cfs			
Minimum Length =	97.4	18 ft			First set the desired I Highlight Cell F232.
If any of the resulting values do not meet the design requirement set forth in	RG-348, the	e design param	eters may be modifi	ed and the solver rerun.	
If any of the resulting values still do not meet the design requirement set for	th in RG-348	B, widening the	swale bottom value	may not be possible.	Click on "Tools" and
16. Vegetated Filter Strips	Designed as	Required in RG-	348	Pages 3-55 to 3-57	The value in the "Set The value in the "By ( Click on solve.
There are no calculations required for determining the load or size of vegeta	ative filter st	rips.			
The 80% removal is provided when the contributing drainage area does not the sheet flow leaving the impervious cover is directed across 15 feet of en- across 50 feet of natural vegetation with a maximum slope of 10%. There can	exceed 72 fe jineered filte in be a breal	eet (direction of er strips with ma k in grade as lo	flow) and aximum slope of 20° ng as no slope exce	% or <del>e</del> ds 20%.	The resulting "Design If the resulting "Design First set the desired I Highlight Cell F232.
If vegetative filter strips are proposed for an interim permanent BMP, they may	nav be sized	as described o	n Page 3-56 of RG-3	48.	Click on "Tools" and
(a) Signal and the r of the transfer of the structure transfer ender 1 and 1 and 1					The value in the "Set
17. Wet Vaults	Designed as	Required in RG-	348	Pages 3-30 to 3-32 & 3-79	The value in the "By the Click on solve.
Required Load Removal Based upon Equation 3.3 =	NA	lbs			The resulting "Desigı If the resulting "Desiແ
First calculate the load removal at 1.1 in/hour					
RG-348 Page 3-30 Equation 3.4: Q = CiA					
C = runoff coefficient for the drainage area = i = design rainfall intensity = A = drainage area in acres =	0.5 1	56 .1 .1 in/hour 1 acres	C = Runoff Coefficie	nt = 0.546 (IC) <sup>2</sup> + 0.328 (IC) + 0.03	
Q = flow rate in cubic feet per second =	0.€	61 cubic feet/sec			
RG-348 Page 3-31 Equation 3.5: V <sub>OR</sub> = Q/A					
Q = Runoff rate calculated above = A = Water surface area in the wet valit =	0.€	61 cubic feet/sec			
V <sub>OR</sub> = Overflow Rate =	0.0	00 feet/sec			
Percent TSS Removal from Figure 3-1 (RG-348 Page 3-31) =	ŧ	53 percent			
Load removed by Wet Vault =	#VALUE!	lbs			
If a bypass occurs at a rainfall intensity of less than 1.1 in/hours Calculate the efficiency reduction for the actual rainfall intensity rate					
Actual Rainfall Intensity at which Wet Vault bypass Occurs =	0	).5 in/hour			
Fraction of rainfall treated from Figure 3-2 RG-348 Page 3-32 = Efficiency Reduction for Actual Bainfall Intensity =	0.7	75 percent 83 percent			
	0.0				

18. Permeable Concrete	Designed as F	Required in R	3-348 Pages 3-79 to 3-83
		ioqui ou in tr	
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING 20	NE		
19. BMPs Installed in a Series	Designed as F	Required in R	G-348 Pages 3-32
Michael E. Barrett, Ph.D., P.E. recommended that the coefficient	ent for E2 be	changed fro	m 0.5 to 0.65 on May 3, 2006
$E_{TOT} = [1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))] \times 100 =$	86.3	8 percent	NET EFFICIENCY OF THE BMPs IN THE SERIES
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1 =$	75.0	0 percent	
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	70.0	0 percent	
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3$ =	0.0	0 percent	
THEREFORE, THE NET LOAD REMOVAL WOULD BE: $(A_1 AND A_2 VALUES ARE FROM SECTION 3 ABOVE)$			
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>1</sub> X 34.6 X A <sub>P</sub> X0.54) =	1389.6	5 lbs	
20. Stormceptor			
Required TSS Removal in BMP Drainage Area=	NA	lbs	
Impervious Cover Overtreatment≃ TSS Removal for Lincentured Area –	0.0000	ac	
BMP Sizing	0.00	103	
Effective Area =	NA	EA	
Calculated Model Size(s) =	#N/A		
Actual Model Size (if multiple values provided in Calculated Model Size or if you are choosing a larger model size) =	0	Model Size	
Surface Area =	#N/A	ft <sup>2</sup>	
Overflow Rate =	#VALUE!	Vor	
Rounded Overflow Rate =	#VALUE!	Vor	
BMP Efficiency % =	#VALUE!	%	
L <sub>R</sub> Value =	#VALUEI	lbs	
TSS Load Credit =	#VALUE!	lbs	
Is Sufficient Treatment Available? (TSS Credit $\geq$ TSS Uncapt.)	#VALUE!		
TSS Treatment by BMP (LM + TSS Uncapt.) =	#VALUE!		

Resultant TSS Load removed by Wet Vault = #VALUE! lbs

 Required TSS Removal in BMP Drainage Area= Impervious Cover Overtreatment=	1687.49 0.0000	lbs ac
BMP Sizing	0.00	IDS
Effective Area =	1.71	EA
Calculated Model Size(s) =	Vx1319	
Actual Model Size (if choosing larger model size) =	Vx1421	Pick Model Size
Surface Area =	153.90	ft <sup>2</sup>
Overflow Rate =	0.012246	V <sub>or</sub>
Rounded Overflow Rate =	0.012500	Var
BMP Efficiency % =	84.00	%
L <sub>R</sub> Value =	1813.76	lbs
TSS Load Credit =	126.27	lbs
Is Sufficient Treatment Available? (TSS Credit $\geq$ TSS Uncapt.)	Yes	
TSS Treatment by BMP (LM + TSS Uncapt.) =	1687.49	

-

## 21. Vortech



SECTION

SCALE:

"C-C"

HORZ: 1"=20'

VERT: 1"=2'

Filtration Rate Puncture Strength ASTM D-751\* Mullen Burst Strength ASTM D-751 Tensile Strength ASTM D-1682 Equiv. Opening Size **US Standard Sieve** \*modified NOTE: ALL CLEANOUTS TO BE SCREW TYPE. BURY A MIN. OF 6" IN GROUND - FILTER FABRIC SEE THIS SHEET FOR DETAILS AND SPECIFICATIONS GABION BASKET DETAIL SCALE: NTS 1. STONE STONE FILL MATERIAL SHALL CONSIST OF HARD, DURABLE, CLEAN STONE OF THE SIZE ANT TO THE ACTION OF AND AND AND AND AND THE ENGINEER AND RESISTANT TO THE ACTION OF AIR AND WATER AND SUITABLE IN ALL RESPECTS FOR THE PURPOSE INTENDED. 2. WIRE CONTAINERS WRE MESH SHALL CONSIST OF PLASTIC COATED (P.V.C.) GALVANIZED WRE 0.120 INCH IN DIAMETER MINIMUM AND SHALL EQUAL OR EXCEED FEDERAL SPECIFICATION QQ-W-461G, CLASS 3 UNLESS OTHERWISE INDICATED. OPENING OF THE MESH SHALL NOT EXCEED APPROXIMATELY 4 INCHES IN THE LONGEST DIMENSION. THE WIRE MESH IS TO BE FABRICATED IN SUCH MANNER AS TO BE NONRAVELING. THE AND CONNECTING WIRE SHALL BE OF THE SAME TYPE AND SIZE AS THE BASKETS AND SHALL BE SUPPLIED IN SUFFICIENT QUANTITY FOR SECURELY FASTENING ALL EDGES OF THE GABION AND DIAPHRAGMS. 3. FILTER FABRIC FILTER FABRIC SHALL BE NON-BIODEGRADABLE ULTRAVIOLET STABILIZED, INERT TO MOST SOIL CHEMICALS, UNAFFECTED BY MOISTURE WHICH ALLOWS WATER TO PASS THROUGH WHILE RETAINING SOIL PARTICLES AND SHALL CONFORM TO ITEM NO. 620, "FILTER FABRIC". #4 bar @ -12"o.c. max Top Of Wall PARKING LOT (SEE CIVIL) STEMWALL 4" Cover Typ. 2"dia. weep hole -#4 bar @ 12" Granular Backfill @ 6'-0" on center (TxDot Item 247 on center type Grade 2 Base) --bottom of weep hole 6" above top of grade Drainage gravel(3/4" washed concrete aggregate) according to geotech report \_ #4 bar @ 12" on center -LILLAIIIIIII ×----\_\_\_\_\_\_ #4 bent bar @ 12" on center - Existing Soil -Existing Soi #4 U bar @ 12" on center 15 3'-6" 2'-4" 3'-6" NOTES: 1. F.G. = finish Grade

> 1- RETAINING AT PARKING LOT SCALE: 1/2" = 1'-0"

Unit	Specification					
cm/sec	1 x 10 -6					
%	Not less than 15					
%	Not less than 30					
%	Not less than 30					
%	95% of Standard Proctor Density					

Table 3-1 Clay Liner Specifications (COA,2004)

CLAY LINER SHALL BE A MINIMUM OF 12" THICK.

Table 3-2 Fabric Specifications (COA,2004)

Test Method

ASTM D-2434

ASTM D-2216

ASTM D-2216

Test Method

ASTM D-422

ASTM D-423 & D-424

Property

Permeability

Plasticity Index of Clay

Liquid Limit of Clay

Clay Particles Passing

**Clay Compaction** 

Property

Unit Weight

	Unit	Specification	
-	oz/yd <sup>2</sup>	8	
	in/sec	0.08	
	lb	125	
	psi	400	
	lb	200	
I	No.	80	













	TANA	TI-14	6
Property	lest Method	Unit	Specification
Permeability	ASTM D-2434	cm/sec	1 x 10 <sup>-6</sup>
Plasticity Index of Clay	ASTM D-423 & D-424	%	Not less than 15
Liquid Limit of Clay	ASTM D-2216	%	Not less than 30
Clay Particles Passing	ASTM D-422	%	Not less than 30
Clay Compaction	ASTM D-2216	%	95% of Standard Proctor Density

CLAY LINER SHALL BE A MINIMUM OF 12" THICK.

Property	Test Method	Unit	Specification
Unit Weight		oz/yd <sup>2</sup>	8
Filtration Rate		in/sec	0.08
uncture Strength	ASTM D-751*	lb	125
Iullen Burst Strength	ASTM D-751	psi	400
ensile Strength	ASTM D-1682	lb	200
Equiv. Opening Size modified	US Standard Sieve	No.	80





1- RETAINING AT PARKING LOT SCALE: 1/2" = 1'-0"



Figure 3-1 Schematic of Sand Bed Profile











NOTE: ALL CLEANOUTS TO BE SCREW TYPE.

-BURY A MIN. OF 6" IN GROUND FILTER FABRIC SEE THIS SHEET FOR DETAILS AND SPECIFICATIONS

SCALE: NTS







APPROVED DATE: 3/03	DWG NO: ST-010	SCALE: N.T.S.	
DRAWN BY: RAS	SHEET: 1 OF 1		CITY OF NEW BRAUNFELS
FILENAME: ST-010 CURB AND	GUTTER		ENGINEERING DEPARTMENT





# OCT 1 1 2010

# LETTER OF TRANSMITTAL

COUNTY ENGINEER

ATTN: Alan Jones	DATE: 8-10-10
To: TCEQ	RE: Christ Our King Anglican Church WPAP

WE ARE SENDING YOU	attached	under separate cove	er the following:
🗆 shop drawings	🗆 prints	standards	specifications
🗆 plans	□ copy of letter	ordinance	□ other:

COPIES	ITEM	DESCRIPTION
1	Original	Christ Our King Anglican Church WPAP Resubmittal
4	Copies	Christ Our King Anglican Church WPAP Resubmittal

# THESE ARE TRANSMITTED AS CHECKED BELOW:

for approval

□ for your use

□ as requested

□ for review and comment

□ approved as noted

 $\Box$  returned for corrections

□ approved as submitted

□ other:

resubmit
submit
return

□ copies for approval□ copies for distribution

 $\Box$  corrected prints

Signed

nea James Ingalis


ENGINEERING & SURVEYING

August 10, 2010

Mr. Alan Jones Field Operations Division, Region 13 (San Antonio) Texas Commission on Environmental Quality 14250 Judson Road San Antonio, TX 78233-4480

2010 AUG 10 PM 4: 4

RE: Christ Our King Anglican Church Water Pollution Abatement Plan Application

This letter is in response to the fax received 08/02/2010 TCEQ as it pertains to the Christ Our King Anglican Church Water Pollution Abatement Plan Application. The comments received are in italics and our responses are in bold.

- 1. Water Wells Information does not agree throughout the application.
  - a. TCEQ-0585, Geologic Assessment- The well identified "S-6" in the Assessment Table is referred to as "S-3" in the Narrative Description. Please correct the typo.

#### The Narrative Description has been corrected, see attached.

b. TCEQ-0584, WPAP Application, Item#20, status of wells, and TCEQ-0585, Geologic Assessment, Item #11, status of wells. The response gives differing information on well statuses. Please make needed corrections. Please also relate whether the requirements noted in the June 21, 2010 letter from the Edwards Aquifer Authority have been addressed.

For the first phase of development (Construction of the Fellowship Hall), wells S-1, S-2, and S-6 will supply water to the new Fellowship Hall. The owner is aware of the TCEQ requirements for a public water system. In their opinion, they will not meet the threshold for a public water supply in the first phase of construction. Once the public water supply threshold is met, they will proceed to either abandon the three wells in accordance with 16 TAC Chapter 76 requirements and connect into NBU's public water system, or ensure that the existing wells meet the requirements of a public water system, according to TCEQ regulations.



2. Wastewater Treatment- TCEQ-0584, WPAP Application, Item #5, any factors that could affect surface and groundwater quality, and Item #15, wastewater disposal. The facility is to generate more than 23,000 gallons of wastewater per day. By definition, on-site sewage facilities do not treat or dispose of more than 5,000 gallons of sewage each day. An individual wastewater permit is required for the anticipated amount of wastewater. Please contact TCEQ's Water Quality Division, Wastewater Permitting Section, about the proposed facility. Please find whether the prohibition noted by 30 TAC 213.6(a)(1) and 213.8(a)(6) apply. Please correct the response and relate the status of any permit application.

The first five phases of development will result in wastewater flows totaling less than 5,000 gallons per day. The assumption of the design was that by the time the final phase will be constructed (approximately 10-20 years) either public sewer would be available from NBU or the church will apply for an individual wastewater permit.

Please accept these comments and revisions to the WPAP for the referenced project. If you need additional information or have any questions, please do not hesitate to contact myself or James Ingalls.

Sincerely,

Jeff Moeller, P.E. Attachments



Re: Edwards Aquifer, Comal County

NAME OF PROJECT: Christ Our King Anglican Church, located on FM 1863, 0.75 miles southwest of State Highway 46, New Braunfels, Texas TYPE OF PLAN: Request for Approval of a Water Pollution Abatement Plan (WPAP); 30 Texas Administrative Code (TAC) Chapter 213 Edwards Aquifer Edwards Aquifer Protection Program San Antonio File ID No. 2935.00 Investigation No. 828713, Regulated Entity No. RN105933493

We are in the process of technically reviewing the WPAP application you submitted for the abovereferenced project. Before we can proceed with our review, the following comments relating to the application must be addressed:

1. Water Wells - Information does not agree throughout the application.

a. TCEQ-0585, Geologic Assessment

The well identified "S-6" in the Assessment Table is referred to as "S-3" in the Narrative Description. Please correct the typo.

b. TCEQ-0584, WPAP application, Item #20, status of wells, and TCEQ-0585, Geologic Assessment, Item #11, status of wells.

The responses give differing information on well statuses. Please make needed corrections. Please also relate whether the requirements noted in the June 21, 2010 letter from the Edwards Aquifer Authority have been addressed.

Mr. Salsman and Mr. Moeller August 2, 2010 Page 2

2. Wastewater Treatment

TCEQ-0584, WPAP application, Item #5, any factors that could affect surface and groundwater quality, and Item #15, wastewater disposal.

The facility is to generate more than 23,000 gallons of wastewater per day. By definition, on-site sewage facilities do not treat or dispose of more than 5,000 gallons of sewage each day. An individual wastewater permit is required for the anticipated amount of wastewater. Please contact TCEQ's Water Quality Division, Wastewater Permitting Section, about the proposed facility. Please find whether the prohibition noted by 30 TAC 213.6(a)(1) and 213.8(a)(6) apply. Please correct the response and relate the status of any permit application.

We ask that you submit one original and three copies of the amended materials to supplement the WPAP application to this office by no later than 14 days from the date of this letter to avoid denial of the plan. If the response to this notice is not received, is incomplete or inadequate, or provides new information that is incomplete or inadequate, a second notice will be sent to you requiring a response within 14 days from the notice date. If the response to the second notice is not received, is incomplete or inadequate, or provides new information that is incomplete or inadequate. If the response to the second notice is not received, is incomplete or inadequate, or provides new information that is incomplete or inadequate, the application will be denied unless you provide written notification that the application is being withdrawn. Please note that the application fee will be forfeited if the plan is not withdrawn. If you have any questions or require additional information, please contact Alan G. Jones the Edwards Aquifer Protection Program of the San Antonio Regional Office at (210) 403-4074.

# FEATURE NARRATIVE

### WPAP GEOLOGIC ASSESSMENT PROPOSED CHRIST OUR KING ANGLICAN CHURCH 467 F.M. 1863 NEW BRAUNFELS, TEXAS

Five features found are described as follows:

Three man-made features in bedrock were observed on Site. Features S-1 and S-2 are existing water wells located on the hilltop and ridge in the north central portion of the Site. Feature S-6 is a water well casing and riser plug, not currently used as a well, with grout surrounding the casing at the ground surface. Features S-1 and S-2 were surrounded by concrete surface completion pads that are in good shape without any open pathways observed between the casing and native ground. Based on the point values in the geologic assessment table and criteria in the Rapid Infiltration Probability Flowchart of TCEQ-0585, the features have a low probability of rapid infiltration and are considered not sensitive.

Two non-karst closed depressions were observed on Site. Feature S-3 is a manmade stock tank on the south portion of the Site in Del Rio Clay. Feature S-4 is a manmade stock tank on the west portion of the Site, near F.M. 1863, in Del Rio Clay. These features are lined with fine-grained sediment without any open pathways observed. Based on the point values in the geologic assessment table and criteria in the Rapid Infiltration Probability Flowchart of TCEQ-0585, the features have a low probability of rapid infiltration and are considered not sensitive.

According to the literature (Collins, 1991), there is an inferred fault (Feature S-5) mapped on the southeastern portion of the Site. This fault appears to trend North 21° East, and forms the saddle between two hilltops along the eastern property boundary. No evidence of this fault was observed in the field. This fault is not extensive relative to similar faults in the area, appears to have limited offset, and juxtaposes like formations. There were no open pathways observed in the area of the fault. Based on the point values in the geologic assessment table and criteria in the Rapid Infiltration Probability Flowchart of TCEQ-0585, the feature has a low probability of rapid infiltration and is considered not sensitive.

\_\_\_\_ The SCS will be submitted at a later date. The owner is aware that the SCS may not be installed prior to executive director approval.

The sewage collection system will convey the wastewater to the Treatment Plant. The treatment facility is:

- \_\_\_\_ existing.
- \_\_\_\_ proposed.

16. X All private service laterals will be inspected as required in 30 TAC §213.5.

#### SITE PLAN REQUIREMENTS

#### Items 17 through 27 must be included on the Site Plan.

- 17. The Site Plan must have a minimum scale of  $1^{"} = 400^{"}$ . Site Plan Scale:  $1^{"} = 100$ .
- 18. 100-year floodplain boundaries
  - Some part(s) of the project site is located within the 100-year floodplain. The floodplain is shown and labeled.
- X No part of the project site is located within the 100-year floodplain.

The 100-year floodplain boundaries are based on the following specific (including date of material) sources(s):

#### FEMA Panel Number 48091C0435F Dated 09/02/2009

19. X The layout of the development is shown with existing and finished contours at appropriate, but not greater than ten-foot contour intervals. Show lots, recreation centers, buildings, roads, etc.

The layout of the development is shown with existing contours. Finished topographic contours will not differ from the existing topographic configuration and are not shown.

- 20. All known wells (oil, water, unplugged, capped and/or abandoned, test holes, etc.):
  - X There are <u>3</u> (#) wells present on the project site and the locations are shown and labeled. (Check all of the following that apply)
    - The wells are not in use and have been properly abandoned.
    - The wells are not in use and will be properly abandoned.
    - $\overline{\mathbf{X}}$  The wells are in use and comply with 30 TAC §238.
    - There are no wells or test holes of any kind known to exist on the project site.
- 21. Geologic or manmade features which are on the site:
  - X All sensitive and possibly sensitive geologic or manmade features identified in the Geologic Assessment are shown and labeled.
  - No sensitive and possibly sensitive geologic or manmade features were identified in the Geologic Assessment.
  - \_\_\_\_ ATTACHMENT D Exception to the Required Geologic Assessment. An exception to the Geologic Assessment requirement is requested and explained in ATTACHMENT D provided at the end of this form. Geologic or manmade features were found and are shown and labeled.
  - ATTACHMENT D Exception to the Required Geologic Assessment. An exception to the Geologic Assessment requirement is requested and explained in ATTACHMENT D provided at the end of this form. No geologic or manmade features were found.

- 6. Method of collecting positional data:
  - <u>X</u> Global Positioning System (GPS) technology. Other method(s).
- 7. X The project site is shown and labeled on the Site Geologic Map.
- 8. X Surface geologic units are shown and labeled on the Site Geologic Map.
- 9. X Geologic or manmade features were discovered on the project site during the field investigation. They are shown and labeled on the Site Geologic Map and are described in the attached Geologic Assessment Table.
  - \_ Geologic or manmade features were not discovered on the project site during the field investigation.
- 10. X The Recharge Zone boundary is shown and labeled, if appropriate.
- 11. All known wells (test holes, water, oil, unplugged, capped and/or abandoned, etc.):
  - X There are <u>3</u> (#) wells present on the project site and the locations are shown and labeled. (Check all of the following that apply.)
    - The wells are not in use and have been properly abandoned.
    - **X** The wells are not in use and will be properly abandoned.
    - X The wells are in use and comply with 16 TAC Chapter 76.

There are no wells or test holes of any kind known to exist on the project site.

ADMINISTRATIVE INFORMATION

12. X One (1) original and three (3) copies of the completed assessment has been provided.

Date(s) Geologic Assessment was performed:

Date(s) April 30, 2009

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. My signature certifies that I am qualified as a geologist as defined by 30 TAC Chapter 213.

Kevin L. Wooster, P.G. Print Name of Geologist	Telephone 210-308-5884
Kevin L. Wooster	Fax 210-308-8731 June 4, 2010; revised Aug 10, 2010
Signature of Geologist	Date
Representing: <u>Arias &amp; Associates, Inc., Job No.:2009-307</u> (Name of Company)	

If you have questions on how to fill out this form or about the Edwards Aquifer protection program, please contact us at 210/490-3096 for projects located in the San Antonio Region or 512/339-2929 for projects located in the Austin Region.

Individuals are entitled to request and review their personal information that the agency gathers on its forms. They may also have any errors in their information corrected. To review such information, contact us at 512/239-3282.

(S-2 and S-6) (S-1)

Bryan W. Shaw, Ph. D, *Chairman* Buddy Garcia, *Commissioner* Carlos Rubenstein., *Commissioner* Mark R. Vickery, P.G., *Executive Director* 



TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

June 9, 2010

RECEIVED

JUN 1 1 2010

COUNTY ENGINEER

Mr. Thomas H. Hornseth, P.E. Comal County Engineer 195 David Jonas Drive New Braunfels TX 78132-3710

 Re: Edwards Aquifer, Comal County PROJECT NAME: Christ our King Anglican Church, located on FM1863 0.75 miles southwest of State Highway 46, New Braunfels, Texas PLAN TYPE: Application for Approval of a Water Pollution Abatement Plan (WPAP) 30 Texas Administration Code (TAC) Chapter 213; Edwards Aquifer Protection Program EAPP File No.: 2935.00

Dear Mr. Hornseth:

The referenced application administratively complete on June 8, 2010, is being forwarded to you pursuant to the Edwards Aquifer Rules. The Texas Commission on Environmental Quality (TCEQ) is required by 30 TAC Chapter 213 to provide copies of all applications to affected incorporated cities and underground water conservation districts for their comments prior to TCEQ approval.

Please forward your comments to this office by July 7, 2010.

The Texas Commission on Environmental Quality appreciates your assistance in this matter and your compliance efforts to ensure protection of the State's environment. If you or members of your staff have any questions regarding these matters, please feel free to contact the San Antonio Region Office at (210) 490-3096.

Sincerely

mes For

Lynn M. Bumguardner Water Section Manager San Antonio Regional Office

LMB/eg

REPLY TO: REGION 13 • 14250 JUDSON RD. • SAN ANTONIO, TEXAS 78233-4480 • 210-490-3096 • FAX 210-545-4329

# ₩2935 00

# WATER POLLUTION ABATEMENT PLAN RECEIVED

JUN 1 1 2010

### FOR

COUNTY ENGINEER

# **CHRIST OUR KING ANGLICAN CHURCH**

PREPARED FOR

### **Texas Commission on Environmental Quality**

Region 13 – San Antonio 14250 Judson Road San Antonio, Texas 78233 210-490-3096 (office) 210-545-4329 (fax)

TCEQ-R13

JUN 08 2010 SAN ANTONIO

PREPARED BY



Jeffrey D. Moeller, P.E. 410 N. Seguin St New Braunfels, TX 78130

> Prepared June 7, 2010



# RECEIVED

#### General Information Form For Regulated Activities on the

JUN 1 1 2010

Edwards Aquifer Recharge and Transition Zones and Relating to 30 TAC §213.4(b) & §213.5(b)(2)(A), (B)OUNTY ENGINEER Effective June 1, 1999

REGULATED ENTITY NAME	E: Christ Our King A	n <mark>qlican Church</mark>	Creek, Dry Comal Tributary
COUNTY: <u>Comal</u>	STRE	EAM BASIN: <b>Blieders</b> (	
EDWARDS AQUIFER:	X RECHARGE ZO	NE DNE	
PLAN TYPE:	X WPAP	AST	EXCEPTION
	SCS	UST	MODIFICATION

### **CUSTOMER INFORMATION**

1. Customer (Applicant):

Contact Person:	Charles Salsman									
Entity:	Christ Our King Anglican	Church								
Mailing Address:	111 W. San Antonio, St. St	111 W. San Antonio, St. Suite 250								
City, State:	New Braunfels, TX.		_Zip: _	78130-5158						
Telephone:	(830)632-7744	_ FAX:	(830)	632-7779						

Agent/Representative (If any):

Contact Person:	Jeffrey D. Moeller, P.E.	
Entity:	HMT Engineering & Surveying	
Mailing Address:	410 N. Seguin Street	
City, State:	New Braunfels, Texas	Zip: 78130-5085
Telephone:	(830) 625-8555 FAX:	(830) 625-8556

- 2. \_\_\_\_ This project is inside the city limits of \_
  - X This project is outside the city limits but inside the ETJ (extra-territorial jurisdiction) of New Braunfels
    - \_ This project is not located within any city's limits or ETJ.
- 3. The location of the project site is described below. The description provides sufficient detail and clarity so that the TCEQ's Regional staff can easily locate the project and site boundaries for a field investigation.

# Christ Our King Anglican Church is located on FM 1863 approximately 0.75 miles southwest of the intersection with State Highway 46.

- 4. <u>X</u> ATTACHMENT A ROAD MAP. A road map showing directions to and the location of the project site is attached at the end of this form.
- 5. X ATTACHMENT B USGS / EDWARDS RECHARGE ZONE MAP. A copy of the official 7 ½ minute USGS Quadrangle Map (Scale: 1" = 2000') of the Edwards Recharge Zone is attached behind this sheet. The map(s) should clearly show:

- X Project site.
- X USGS Quadrangle Name(s).
- **X** Boundaries of the Recharge Zone (and Transition Zone, if applicable).
- **X** Drainage path from the project to the boundary of the Recharge Zone.
- 6. <u>X</u> Sufficient survey staking is provided on the project to allow TCEQ regional staff to locate the boundaries and alignment of the regulated activities and the geologic or manmade features noted in the Geologic Assessment. The TCEQ must be able to inspect the project site or the application will be returned.
- 7. X ATTACHMENT C PROJECT DESCRIPTION. Attached at the end of this form is a detailed narrative description of the proposed project.
- 8. Existing project site conditions are noted below:
  - Existing commercial site
  - Existing industrial site
  - **X** Existing residential site
  - Existing paved and/or unpaved roads
  - Undeveloped (Cleared)
  - Undeveloped (Undisturbed/Uncleared)
  - Other:

#### PROHIBITED ACTIVITIES

- 9. X I am aware that the following activities are prohibited on the **Recharge Zone** and are not proposed for this project:
  - (1) waste disposal wells regulated under 30 TAC Chapter 331 of this title (relating to Underground Injection Control);
  - new feedlot/concentrated animal feeding operations, as defined in 30 TAC §213.3;
  - (3) land disposal of Class I wastes, as defined in 30 TAC §335.1;
  - (4) the use of sewage holding tanks as parts of organized collection systems; and
  - (5) new municipal solid waste landfill facilities required to meet and comply with Type I standards which are defined in §330.41(b), (c), and (d) of this title (relating to Types of Municipal Solid Waste Facilities).
- 10. <u>N/A</u> I am aware that the following activities are prohibited on the **Transition Zone** and are not proposed for this project:
  - (1) waste disposal wells regulated under 30 TAC Chapter 331 (relating to Underground Injection Control);
  - (2) land disposal of Class I wastes, as defined in 30 TAC §335.1; and
  - (3) new municipal solid waste landfill facilities required to meet and comply with Type I standards which are defined in §330.41 (b), (c), and (d) of this title.

#### ADMINISTRATIVE INFORMATION

- 11. The fee for the plan(s) is based on:
  - X For a Water Pollution Abatement Plan and Modifications, the total acreage of the site where regulated activities will occur.

- \_\_\_\_ For an Organized Sewage Collection System Plans and Modifications, the total linear footage of all collection system lines.
- \_\_\_\_ For a UST Facility Plan or an AST Facility Plan, the total number of tanks or piping systems.
- \_\_\_\_ A Contributing Zone Plan.
- A request for an exception to any substantive portion of the regulations related to the protection of water quality.
- \_\_\_\_ A request for an extension to a previously approved plan.
- 12. Application fees are due and payable at the time the application is filed. If the correct fee is not submitted, the TCEQ is not required to consider the application until the correct fee is submitted. Both the fee and the Edwards Aquifer Fee Form have been sent to the Commission's:
  - \_\_\_\_\_TCEQ cashier
  - Austin Regional Office (for projects in Hays, Travis, and Williamson Counties)
  - X San Antonio Regional Office (for projects in Bexar, Comal, Kinney, Medina, and Uvalde Counties)
- 13. X Submit one (1) original and three (3) copies of the completed application to the appropriate regional office for distribution by the TCEQ to the local municipality or county, groundwater conservation districts, and the TCEQ's Central Office.
- 14. X No person shall commence any regulated activity until the Edwards Aquifer Protection Plan(s) for the activity has been filed with and approved by the executive director.
  - No person shall commence any regulated activity until the Contributing Zone Plan for the activity has been filed with the executive director.

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This **GENERAL INFORMATION FORM** is hereby submitted for TCEQ review. The application was prepared by:

Jeffrey D. Moeller, P.E. Print Name of Customer/Agent

Signature of Qustomer/Agent

Date

If you have questions on how to fill out this form or about the Edwards Aquifer protection program, please contact us at 210/490-3096 for projects located in the San Antonio Region or 512/339-2929 for projects located in the Austin Region.

the state of the s

### ATTACHMENT "C" Project Description

Christ Our King Anglican Church is located on the south side of FM 1863 approximately 0.75 miles southwest of the intersection with State Highway 46. (See Location Map) There are 2 existing houses on-site along with some storage buildings. The site is divided into two watersheds, one drains north to Blieders Creek, the second drains south and west to the Dry Comal Creek. According to the Flood Insurance Rate Map No. 48091C0430F there is no existing floodplain located within the property.

The project is proposed to be constructed in 6 Phases (See Phasing Exhibit), each phase will have its own temporary and permanent BMP's installed per TCEQ requirements.

The church campus infrastructure will include a water system, electricity, telephone, cable television, and an On-Site Sewerage Facility is proposed to treat the sanitary sewer from the development. There are three on-site wells that will provide water service for the first few phases of development.

The impervious cover for the ultimate development of the 22.11 acre site will be approximately 41.2%. The site will utilize a combination of vegetative filter strips and Vortechs® Stormwater treatment systems to treat stormwater runoff generated by the proposed improvements.

Due to the construction phasing of the project, there will not be more than 10 acres of disturbed soil in one common drainage area that will occur at one time. The site is divided into two drainage areas. (See Drainage Area Map)







# **GEOLOGIC ASSESSMENT**

RECEIVED JUN 1 1 2010 COUNTY ENGINEER

For:

# WPAP GEOLOGIC ASSESSMENT PROPOSED CHRIST OUR KING ANGLICAN CHURCH 467 F.M. 1863 NEW BRAUNFELS, TEXAS



Prepared for:

Christ Our King Anglican Church C/O Charles W. Salsman 1111 W. San Antonio Street New Braunfels, Texas 78130

> Job Number 2009-307 June 2010

#### Geologic Assessment For Regulated Activities on The Edwards Aquifer Recharge/transition Zones and Relating to 30 TAC §213.5(b)(3), Effective June 1, 1999

#### REGULATED ENTITY NAME: Proposed Christ Our King Anglican Church, 467 F.M. 1863

TYPE OF PROJECT: X WPAP AST SCS UST

LOCATION OF PROJECT: X Recharge Zone Transition Zone Contributing Zone within the Transition Zone

PROJECT INFORMATION

- 1. X Geologic or manmade features are described and evaluated using the attached **GEOLOGIC ASSESSMENT TABLE**.
- 2. Soil cover on the project site is summarized in the table below and uses the SCS Hydrologic Soil Groups\* (*Urban Hydrology for Small Watersheds, Technical Release No. 55, Appendix A*, Soil Conservation Service, 1986). If there is more than one soil type on the project site, show each soil type on the site Geologic Map or a separate soils map.

Soil Units, Infi Characteristics &	 * Soil Group Definitions (Abbreviated)		
Soil Name	Group*	Thickness (feet)	A. Soils having a <u>high infiltration</u> rate when thoroughly wetted.
Krum clay, 1 to 3% slopes (KrB)	D	1.0 - 1.5	B. Soils having a <u>moderate</u> infiltration rate when thoroughly wetted.
Krum clay, 3 to 5% slopes (KrC)	D	0.5-1.0	C. Soils having a <u>slow infiltration</u> rate when thoroughly wetted.
Medlin-Eckrant association, 1 to 8% slopes	D	0.5-1.0	D. Soils having a <u>very slow</u> infiltration rate when thoroughly
Rumple-Comfort association, undulating, 1 to 8% slopes	С	1.0 - 1.5	wetted.

- 3. <u>X</u> A **STRATIGRAPHIC COLUMN** is attached at the end of this form that shows formations, members, and thicknesses. The outcropping unit should be at the top of the stratigraphic column.
- 4. <u>X</u> A NARRATIVE DESCRIPTION OF SITE SPECIFIC GEOLOGY is attached at the end of this form. The description must include a discussion of the potential for fluid movement to the Edwards Aquifer, stratigraphy, structure, and karst characteristics of the site.
- 5. <u>X</u> Appropriate **SITE GEOLOGIC MAP(S)** are attached:

The Site Geologic Map must be the same scale as the applicant's Site Plan. The minimum scale is 1" : 400'

Applicant's Site Plan Scale	1"	=	100'
Site Geologic Map Scale	1"	=	100'
Site Soils Map Scale (if more than 1 soil type)	1"	=	400'

- Method of collecting positional data: 6.
  - Global Positioning System (GPS) technology. <u>X</u> Other method(s).
- 7. Х The project site is shown and labeled on the Site Geologic Map.
- 8. Х Surface geologic units are shown and labeled on the Site Geologic Map.
- 9. Х Geologic or manmade features were discovered on the project site during the field investigation. They are shown and labeled on the Site Geologic Map and are described in the attached Geologic Assessment Table.
  - Geologic or manmade features were not discovered on the project site during the field investigation.
- 10. Х The Recharge Zone boundary is shown and labeled, if appropriate.
- 11. All known wells (test holes, water, oil, unplugged, capped and/or abandoned, etc.):
  - Х There are 3 (#) wells present on the project site and the locations are shown and labeled. (Check all of the following that apply.)
    - The wells are not in use and have been properly abandoned.
    - X The wells are not in use and will be properly abandoned. (S-2 and S-6)

X The wells are in use and comply with 16 TAC Chapter 76.

(S-1) There are no wells or test holes of any kind known to exist on the project site.

ADMINISTRATIVE INFORMATION

One (1) original and three (3) copies of the completed assessment has been provided. 12. X

Date(s) Geologic Assessment was performed:

Date(s) April 30, 2009

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. My signature certifies that I am qualified as a geologist as defined by 30 TAC Chapter 213.

Kevin L. Wooster, P.G. Print Name of Geologist	Telephone 210-308-5884
Kevin L. Wooster	Fax 210-308-8731
Signature of Geologist	Date
Representing: <u>Arias &amp; Associates, Inc., Job No.:2009-307</u> (Name of Company)	

If you have questions on how to fill out this form or about the Edwards Aquifer protection program, please contact us at 210/490-3096 for projects located in the San Antonio Region or 512/339-2929 for projects located in the Austin Region.

Individuals are entitled to request and review their personal information that the agency gathers on its forms. They may also have any errors in their information corrected. To review such information, contact us at 512/239-3282.

GEOLOGIC ASSESSMENT TABLE								PROJ	ECT N	IAME:	Pro	oposed	d Christ	Our Kir	ng Anglic	an Ch	nurch,	467	F.M.	186	3			
LOCATION FEATURE CHARACTER								RISTICS	;								EVA	ALUAT	ION	PHYSICAL SETTING				
1A		18.			1C*		2A	2B	3		4		5	5A	6	7	8A	8B	9		10	1	1	12
FEATURE ID		LATITUDE			LONGITUDE	Ĺ	FEATURE TYPE	POINTS	FORMATION	ווס	MENSIONS (FE	(ET)	TREND (DEGREES)	MOD	DENSITY (NO/FT)	APERTURE (FEET)	INFILL	RELATIVE INFILTRATION RATE	TOTAL	SENS	ΙΤΙVITY	CATCI AREA (	HMENT ACRES)	TOPOGRAPHY
	Degrees	Minutes	Seconds	Degrees	Minutes	Seconds				х	Y	z		10						<40	>40	<1.6	<u>&gt;1.6</u>	
S-1	29	42	50.9	98	11	13.1	MB	30	Kbu	1.0	1.0	>200	Water w	ell 8	& concre	ete pad	Х	5	35	Х		Х		Hilltop
S-2	29	42	52.3	98	11	14.8	MB	30	Kbu	1.0	1.0	>200	Water w	ell 8	& concre	ete pad	Х	5	35	Х		Х		Hilltop
S-3	29	42	46.8	98	11	8.0	CD	5	Kdr	90	165	8					F	5	10	Х			Х	Hillside
S-4	29	42	51.4	98	11	20.7	CD	5	Kdr	70	120	6					F	5	10	Х			Х	Hillside
S-5	29	42	46.9	98	11	5.2	F	20	Kgt/Kep	>750	nan in o		N 21 E				F	15	35	Х			Х	Hillside
S-6	29	42	49.8	98	11	16.6	MB	30	Kbu	1.0	1.0	>200	Water w	ell d	casing a	nd cap	Х	5	35	X		Х		Hilltop
																	4-41-4							
											3													

DATUM: NAD 83

2A TYPE	TYPE	2B POINTS
С	Cave	30
SC	Solution cavity h = Horizontal Feature	20
SF	Solution-enlarged fracture(s)	20
F	Fault	20
0	Other natural bedrock features	5
MB	Manmade feature in bedrock	30
SW	Swallow hole	30
SH	Sinkhole	20
CD	Non-karst closed depression	5
Z	Zone, clustered or aligned features	30

\*

Kevin L. Wooster

Geology

164 /CENS S

8A	<b>INFI</b>	LLING
----	-------------	-------

N

None, exposed bedrock
-----------------------

C Coarse - cobbles, breakdown, sand, gravel

O Loose or soft mud or soil, organics, leaves, sticks, dark colors

F Fines, compacted clay-rich sediment, soil profile, gray or red colors

V Vegetation. Give details in narrative description

FS Flowstone, cements, cave deposits

X Other materials

12 TOPOGRAPHY Cliff, Hilltop, Hillside, Drainage, Floodplain, Streambed

I have read, I understood, and I have followed the Texas Commission on Environmental Quality's Instructions to Geologists. The

information presented here complies with that document and is a true representation of the conditions observed in the field.

My signature certifies that I am qualified as a geologist as defined by 30 TAC Chapter 213.

Kevin L. Wooster

Date: June 4, 2010

Sheet 1 of 1

TCEQ-0585-Table (Rev. 10-01-04)

# FEATURE LOCATION TABLE

# WPAP GEOLOGIC ASSESSMENT PROPOSED CHRIST OUR KING ANGLICAN CHURCH <u>467 F.M. 1863</u> NEW BRAUNFELS, TEXAS

		Latitude		L	.ongitud	е					
Feature No.	Deg	Min	Sec	Deg	g Min Se		Type Date		Measured By		
S-1	29	42	50.9	98	11	13.1	MB	4/30/09	K.Wooster		
S-2	29	42	52.3	98	11	14.8	MB	4/30/09	K.Wooster		
S-3	29	42	46.8	98	11	8	CD	4/30/09	K.Wooster		
S-4	29	42	51.4	98	11	20.7	CD	4/30/09	K.Wooster		
S-5	29	42	46.9	98	11	5.2	F	4/30/09	K.Wooster		
S-6	29	42	49.8	98	11	16.6	MB	6/10/2010	K.Wooster		

# SOIL NARRATIVE

### <u>WPAP GEOLOGIC ASSESSMENT</u> <u>PROPOSED CHRIST OUR KING ANGLICAN CHURCH</u> <u>467 F.M. 1863</u> <u>NEW BRAUNFELS, TEXAS</u>

Most of the site has been used as a small ranch and residence. There are several structures, and one gravel road. Native soils remaining at the site consist of black and brown calcareous stony clay. The clay includes rock fragments ranging up to pebbles in size. Although the clay content of the soils would tend to impede the downward flow of water, in areas where the rock fragments are more abundant, the water infiltration would increase. The soils on the site are typical of those found on the Edwards plateau and hill country. They range up to a maximum thickness of about one-half to one foot in some areas. Soils and vegetation cover most of the site. There are areas of rock outcrops on the west and south portions of the site. See the attached soil map for soil type distribution.

According to the U.S.D.A. Soil Survey of Comal and Hays Counties, Texas, dated 1984, the natural surface soils have been mapped as within four primary soil groups.

**Krum clay, 1 to 3% slopes** (KrB) soils are mapped within the east corner of the site. This is deep soil typically found on stream terraces and valley fills. The surface layer of Krum clay is a dark brown clay with some calcareous nodules to a depth of approximately 16 inches which overlies a lighter colored clay layer that ranges up to 80 inches thick or more. Permeability of this soil ranges from 0.2 to 0.57 inches per hour and surface runoff is slow.

**Krum clay, 3 to 5% slopes** (KrC) soils are mapped within the west corner of the site. This is a deep soil typically found on slightly sloping stream terraces. The surface layer of Krum clay is a dark brown clay with some calcareous nodules to a depth of approximately 19 inches which overlies a lighter colored clay layer that ranges up to 80 inches thick or more. Permeability of this soil ranges from 0.2 to 0.6 inches per hour and surface runoff is slow.

**Medlin-Eckrant association, 1 to 8% slopes** soils are mapped within the majority of the site, covering a hillside and ridge forming the central portion of the site. This shallow, well-drained, stony clay occurs on undulating to steep, hilly terrain. The permeability of Medlin-Eckrant soil ranges from less than 0.00 to 6.0 inches per hour, its shrink-swell potential is low to moderate, and its corrosivity potential is high for uncoated steel.

**Rumple Comfort association (RUD)** soils are mapped within the south portion of the site, at the base of the hillside sloping to the south property boundary. The RUD soils are typically shallow to moderately deep soils consisting of dark reddish brown very cherty clay loam with limestone fragments. Overall soil depth is typically 14 inches. RUD soils are well drained and moderately slow permeability with a very low available water capacity and shallow rooting depth. Runoff is moderate and the hazard of water erosion is moderate.



Web Soil Survey 2.2 National Cooperative Soil Survey



# Map Unit Legend

Comal and Hays Counties, Texas (TX604)				
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI	
KrB	Krum clay, 1 to 3 percent slopes	0.6	2.4%	
KrC	Krum clay, 3 to 5 percent slopes	0.1	0.4%	
MEC	Medlin-Eckrant association, 1 to 8 percent slopes	23.0	86.4%	
RUD	Rumple-Comfort association, 1 to 8 percent slopes	2.9	10.8%	
Totals for Area of Inter	rest	26.6	100.0%	



# STRATIGRAPHIC COLUMN

# WPAP GEOLOGIC ASSESSMENT PROPOSED CHRIST OUR KING ANGLICAN CHURCH 467 F.M. 1863 NEW BRAUNFELS, TEXAS

Hydrogeologic subdivision		Group formation or member		Hydro- logic fuction	Thick- ness (feet)	Lithology	Cavern develop- ment	Porosity / permeability type		
Quaternary			Т	errac	e Deposits	CU	0-30	Gravel and sand	None	High porosity / high permeability
Der Contining Contining Unit			Aus	tin Group	CU	130-150	White to gray limestone	None	Low porosity / low permeability	
	per	E	Eagle Ford Group		CU	30-50	Buff, light gray, dense mudstone	None	Low porosity / low permeability	
	ining nit	Buda		Limestone	CU	40-50	Brown flaggy shale and argillaceous limestone	None	Low porosity / low permeability	
đ				Del	Rio Clay	CU	40-50	Blue-green to yellow- brown clay	None	None / primary upper confining unit
	1		(	Seoro Forn	getown nation	CU	10	Reddish-brown, gray to light tan marly limestone	None	Low porosity / low permeability
aceous <	11	aquifer		Ë	Cyclic & marine members undivided	AQ	80-100	Mudstone to packstone; miliolid grainstone; chert	Many sub- surface	Laterally extensive; water yielding
	111		Group Person	u o s	Leached & col- lapsed members	AQ	80-100	Crystalline limestone; mudstone to grainstone; chert collapsed breccia	Extensive lateral devel- opment; large rooms	Majority not fabric / one of the most permeable
	١٧			Рег	Regional dense member	CU	20-24	Dense, argillaceous mudstone	Very few; only vertical fracture enlargement	Not fabric / low permeability; vertical barrier
ret	v	s q	r d s		Grainstone member	AQ	50-60	Miliolid grainstone; mudstone to wackestone; chert	Few	Not fabric / recrystal- lization reduces permeability
0 Le	VI	war	d w a	F m.	Kirschberg evaporite member	AQ	50-60	Highly altered crystalline limestone; chalky mudstone; chert	Probably extensive cave devel.	Majority fabric / one of the most permeable
L O W	VII	ъ Ш	ш	i n e r	Dolomitic member	AQ	110-130	Mudstone to grainstone; crystalline limestone; chert	Caves rela- ted to struc- ture or bed- ding planes	Mostly not fabric; some bedding plane fabric / water-yielding
	VIII		жа	Basal nodular member	Karst AQ; not karst CU	50-60	Shaly, nodular limestone; mudstone and miliolid grainstone	Large lateral caves at surface	Fabric; stratigraph- ically controlled / large conduit flow at surface; no permea- bility in subsurface	
Lower confining unit		Upper member of the Glen Rose Limestone		CU; evaporite beds AQ	350-500	Yellowish tan, thinly bedded limestone and marl	Some sur- face cave development	Some water product- ion at evaporite beds / relatively impermeable		

Reference: U.S.G.S. Geologic Framework and Hydrogeologic Characteristics of the Edwards Aquiler Outcrop,

Comal County, Texas; Water-Resources Investigations Report 94-4117

Note: CU = Confining Unit; AQ = Aquifer

Indicates Upper Most Surface Bedrock Formation

# **GEOLOGY NARRATIVE**

## WPAP GEOLOGIC ASSESSMENT PROPOSED CHRIST OUR KING ANGLICAN CHURCH <u>467 F.M. 1863</u> NEW BRAUNFELS, TEXAS

The site lies along FM 1863 and forms the crest of a hilltop and ridge with sloping north and south flanks. No portion of the site lies within the 100-year floodplain. The outcropping geologic formations mapped at the Site consists of the Buda Limestone, Del Rio Clay, Georgetown Formation, and Edwards Person Formation, according to the San Antonio Sheet of the Geologic Atlas of Texas (BEG, 1983). The outcropping surface geologic units observed at the Site by the project geologist are as described below:

**Buda Limestone (Kbu)** The Buda Limestone formation is fine grained, bioclastic, commonly glauconitic, pyritiferous, hard, massive, poorly bedded to nodular, thinner bedded and argillaceous limestone near the upper contact; light gray to pale orange; weathers dark gray to brown; burrows filled with chalky marl, abundant pelecypods; thickness 60-100 feet, thickens westward. This formation was observed to cover the hilltop and ridge top of the central and north portions of the Site.

**Del Rio Clay (Kdr)** The Del Rio Clay formation is calcareous and gypsiferous, becoming less calcareous and more gypsiferous upward, with pyrite common; blocky, medium gray, weathers light gray to yellowish gray; some thin lenticular beds of highly calcareous siltstone; marine megafossils include abundant Exogyra arietina and other pelecypods; thickness 60-120 feet, thickens westward. This formation was observed to cover the southern slope of the central portion of the Site, and the northern slope adjacent to F.M. 1863.

**Georgetown Formation (Kgt)** The Georgetown Formation is reddish brown, gray to light tan marly limestone, with low porosity and low permeability. This formation was observed to cover the north property boundary, and part of the southern portion of the Site.

**Edwards Person Limestone (Kep)** This formation is generally up to 200 feet thick or more, consists of limestone and marlstone, and forms the upper portions of the Edwards Group. According to Small and Hanson, the outcropping unit is the Cyclic and Marine member, of the Person Formation. The outcropping surface geologic unit observed at the Site by the project geologist is the Cyclic and Marine member, of the Edwards Person Formation, in the south portion of the Site. This member consists of mudstone, grainstone, and chert, and is medium gray to grayish brown.

Most of the site was covered with soil, with a few rock outcrops visible. Much of the visible rock at the site was float, or weathered bedrock laying on ground surface. Some of the float rock showed varying signs of mostly weathered appearance, along with iron-stained mudstone.

There was no evidence of structural faulting or fracturing observed in the field. There were no solution features found. There were no open vugs observed. No karst features were noted during the site reconnaissance. Potential for fluid movement to the aquifer is low due to absence of karst and structural features, along with very low permeability soil cover.

# FEATURE NARRATIVE

### WPAP GEOLOGIC ASSESSMENT PROPOSED CHRIST OUR KING ANGLICAN CHURCH <u>467 F.M. 1863</u> NEW BRAUNFELS, TEXAS

Five features found are described as follows:

Three man-made features in bedrock were observed on Site. Features S-1 and S-2 are existing water wells located on the hilltop and ridge in the north central portion of the Site. Feature S-3 is a water well casing and riser plug, not currently used as a well, with grout surrounding the casing at the ground surface. Features S-1 and S-2 were surrounded by concrete surface completion pads that are in good shape without any open pathways observed between the casing and native ground. Based on the point values in the geologic assessment table and criteria in the Rapid Infiltration Probability Flowchart of TCEQ-0585, the features have a low probability of rapid infiltration and are considered not sensitive.

Two non-karst closed depressions were observed on Site. Feature S-3 is a manmade stock tank on the south portion of the Site in Del Rio Clay. Feature S-4 is a manmade stock tank on the west portion of the Site, near F.M. 1863, in Del Rio Clay. These features are lined with fine-grained sediment without any open pathways observed. Based on the point values in the geologic assessment table and criteria in the Rapid Infiltration Probability Flowchart of TCEQ-0585, the features have a low probability of rapid infiltration and are considered not sensitive.

According to the literature (Collins, 1991), there is an inferred fault (Feature S-5) mapped on the southeastern portion of the Site. This fault appears to trend North 21° East, and forms the saddle between two hilltops along the eastern property boundary. No evidence of this fault was observed in the field. This fault is not extensive relative to similar faults in the area, appears to have limited offset, and juxtaposes like formations. There were no open pathways observed in the area of the fault. Based on the point values in the geologic assessment table and criteria in the Rapid Infiltration Probability Flowchart of TCEQ-0585, the feature has a low probability of rapid infiltration and is considered not sensitive.

# REFERENCES

- Barnes V.L. 1983, <u>Geologic Atlas of Texas, San Antonio, Sheet</u>, Bureau of Economic Geology, The University of Texas at Austin, Texas.
- Collins, E.W., 1991. <u>Geology of New Braunfels West Quadrangle, Comal County, Texas, Open File</u> <u>Map</u>. Bureau of Economic Geology, The University of Texas at Austin, Texas.
- Small, T.A. and Hanson, J.A. 1994. <u>Geologic Framework and Hydrogeologic Characteristics of the Edwards Aquifer Outcrop, Comal County, Texas.</u> U.S. Geol. Survey, Water Resources Investigations Report 94-4117. 8 pp., Plate, Fig., Table.
- Texas Commission on Environmental Quality, (TCEQ), <u>Instructions to Geologists for Geologic</u> <u>Assessments on the Edwards Aquifer Recharge Zone</u>, TCEQ-0585-Instructions (Rev. 10-01-04).
- United States Department of Agriculture. 1984 <u>Soil Survey of Comal and Hays Counties, Texas</u>, Natural Resource Conservation Service.
- United States Department of Agriculture. <u>Urban Hydrology for Small Watersheds, Technical Release</u> <u>No. 55., Appendix A</u>. Natural Resource Conservation Service, <a href="http://www.info.usda.gov/CED/ftp/CED/tr55.pdf">http://www.info.usda.gov/CED/ftp/CED/tr55.pdf</a> July, 1986.
- United Stated Geologic Survey, Rev. 1994. <u>New Braunfels West Quadrangle.</u> USGS, Denver, Colorado.



#### Water Pollution Abatement Plan Application

for Regulated Activities on the Edwards Aquifer Recharge Zone and Relating to 30 TAC §213.5(b), Effective June 1, 1999

RECEIVED JUN 1 1 2010

### REGULATED ENTITY NAME: Christ Our King Anglican Church

COUNTY ENGINEER

#### **REGULATED ENTITY INFORMATION**

2. Total site acreage (size of property): 22.11

- 3. Projected population:
- 4. The amount and type of impervious cover expected after construction are shown below:

4000

Impervious Cover of Proposed Project	Sq. Ft.	Sq. Ft./Acre	Acres
Structures/Rooftops	123,606	÷ 43,560 =	2.84
Parking (Driveway)	230,500	÷ 43,560 =	5.29
Other paved surfaces (Sidewalk)	42,625	÷ 43,560 =	0.98
Total Impervious Cover	305,420	÷ 43,560 =	9.11
Total Impervious Cover ÷ Total Acr	41.2%		

- 5. <u>X</u> ATTACHMENT A Factors Affecting Water Quality. A description of any factors that could affect surface water and groundwater quality is provided at the end of this form.
- 6. X Only inert materials as defined by 30 TAC §330.2 will be used as fill material.

#### FOR ROAD PROJECTS ONLY Complete questions 7-12 if this application is exclusively for a road project.

- 7. Type of project:
  - \_\_\_\_\_ TXDOT road project.
  - County road or roads built to county specifications.
  - City thoroughfare or roads to be dedicated to a municipality.
  - \_\_\_\_ Street or road providing access to private driveways.
- 8. Type of pavement or road surface to be used:
  - \_\_\_\_ Concrete
  - Asphaltic concrete pavement
  - Other:

- 9. Length of Right of Way (R.O.W.): \_\_\_\_\_\_ feet. Width of R.O.W.: \_\_\_\_\_\_ feet. L x W = \_\_\_\_\_ Ft<sup>2</sup> ÷ 43,560 Ft<sup>2</sup>/Acre = \_\_\_\_\_\_ acres.
  10. Length of pavement area: \_\_\_\_\_\_ feet. Width of pavement area: \_\_\_\_\_\_ feet. L x W = \_\_\_\_\_ Ft<sup>2</sup> ÷ 43,560 Ft<sup>2</sup>/Acre = \_\_\_\_\_ acres.
- Pavement area \_\_\_\_\_ acres ÷ R.O.W. area \_\_\_\_\_ acres x 100 = \_\_\_% impervious cover.
- 11. \_\_\_\_ A rest stop will be included in this project. A rest stop will **not** be included in this project.
- 12. \_\_\_\_ Maintenance and repair of existing roadways that do not require approval from the TCEQ Executive Director. Modifications to existing roadways such as widening roads/adding shoulders totaling more than one-half (1/2) the width of one (1) existing lane require prior approval from the TCEQ.

### STORMWATER TO BE GENERATED BY THE PROPOSED PROJECT

13. **ATTACHMENT B - Volume and Character of Stormwater.** A description of the volume and character (quality) of the stormwater runoff which is expected to occur from the proposed project is provided at the end of this form. The estimates of stormwater runoff quality and quantity should be based on area and type of impervious cover. Include the runoff coefficient of the site for both pre-construction and post-construction conditions.

#### WASTEWATER TO BE GENERATED BY THE PROPOSED PROJECT

14. The character and volume of wastewater is shown below:

100 % Domestic	23,320 gallons/day
% Industrial	gallons/day
% Commingled	gallons/day

TOTAL\_23,320 gallons/day

- 15. Wastewater will be disposed of by:
  - X On-Site Sewage Facility (OSSF/Septic Tank):
    - **ATTACHMENT C** Suitability Letter from Authorized Agent. An on-site sewage facility will be used to treat and dispose of the wastewater. The appropriate licensing authority's (authorized agent) written approval is provided at the end of this form. It states that the land is suitable for the use of an on-site sewage facility or identifies areas that are not suitable.
    - Each lot in this project/development is at least one (1) acre (43,560 square feet) in size. The system will be designed by a licensed professional engineer or registered sanitarian and installed by a licensed installer in compliance with 30 TAC Chapter 285.

\_\_\_ Sewage Collection System (Sewer Lines):

- Private service laterals from the wastewater generating facilities will be connected to an existing SCS.
- Private service laterals from the wastewater generating facilities will be connected to a proposed SCS.
  - The SCS was previously submitted on \_\_\_\_\_
  - The SCS was submitted with this application.

\_\_\_\_ The SCS will be submitted at a later date. The owner is aware that the SCS may not be installed prior to executive director approval.

The sewage collection system will convey the wastewater to the Treatment Plant. The treatment facility is:

- \_\_\_\_ existing.
- \_\_\_\_ proposed.
- 16. X All private service laterals will be inspected as required in 30 TAC §213.5.

#### SITE PLAN REQUIREMENTS

#### Items 17 through 27 must be included on the Site Plan.

- 17. The Site Plan must have a minimum scale of 1" = 400'. Site Plan Scale:  $1" = \_100$ \_'.
- 18. 100-year floodplain boundaries
  - Some part(s) of the project site is located within the 100-year floodplain. The floodplain is shown and labeled.
- X No part of the project site is located within the 100-year floodplain.

The 100-year floodplain boundaries are based on the following specific (including date of material) sources(s):

#### FEMA Panel Number 48091C0435F Dated 09/02/2009

19. X The layout of the development is shown with existing and finished contours at appropriate, but not greater than ten-foot contour intervals. Show lots, recreation centers, buildings, roads, etc.

The layout of the development is shown with existing contours. Finished topographic contours will not differ from the existing topographic configuration and are not shown.

- 20. All known wells (oil, water, unplugged, capped and/or abandoned, test holes, etc.):
  - X There are <u>3</u> (#) wells present on the project site and the locations are shown and labeled. (Check all of the following that apply)
    - The wells are not in use and have been properly abandoned.
    - The wells are not in use and will be properly abandoned.
    - X The wells are in use and comply with 30 TAC §238.
    - There are no wells or test holes of any kind known to exist on the project site.
- 21. Geologic or manmade features which are on the site:
  - X All **sensitive and possibly sensitive** geologic or manmade features identified in the Geologic Assessment are shown and labeled.
  - \_\_\_\_ No sensitive and possibly sensitive geologic or manmade features were identified in the Geologic Assessment.
  - \_\_\_\_\_ ATTACHMENT D Exception to the Required Geologic Assessment. An exception to the Geologic Assessment requirement is requested and explained in ATTACHMENT D provided at the end of this form. Geologic or manmade features were found and are shown and labeled.
  - **ATTACHMENT D Exception to the Required Geologic Assessment.** An exception to the Geologic Assessment requirement is requested and explained in ATTACHMENT D provided at the end of this form. No geologic or manmade features were found.

- 22. X The drainage patterns and approximate slopes anticipated after major grading activities.
- 23. Х Areas of soil disturbance and areas which will not be disturbed.
- 24. X Locations of major structural and nonstructural controls. These are the temporary and permanent best management practices.
- 25. Locations where soil stabilization practices are expected to occur. Х
- 26. Х Surface waters (including wetlands).
- 27. Locations where stormwater discharges to surface water or sensitive features. 3 X There will be no discharges to surface water or sensitive features.

#### **ADMINISTRATIVE INFORMATION**

- 28. Х One (1) original and three (3) copies of the completed application have been provided.
- 29. X Any modification of this WPAP will require TCEQ executive director approval, prior to construction, and may require submission of a revised application, with appropriate fees.

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This WATER POLLUTION ABATEMENT PLAN APPLICATION FORM is hereby submitted for TCEQ review and executive director approval. The form was prepared by:

#### Jeffrey D. Moeller, P.E.

Print Name of Customer/Agent

of Customer/Agent

1/10

### <u>ATTACHMENT "A"</u> Factors Affecting Water Quality

The development will consist of an asphalt parking lot and multiple structures varying in size from 1,250 to 44,900 square feet. This will result in minimal to no pollution from the site. Some pollution may originate from the asphalt streets, automobile wastes, and cleaning chemicals, which may have an effect on surface water by sediments leaving the site after a rainfall event.

### ATTACHMENT "B" Volume and Character of Stormwater

The overall drainage patterns of the site will remain unchanged. There will be an increase in storm water runoff generated by the development. The hydrology calculations for the existing and proposed conditions are broken out in the tables below.

### <u>ATTACHMENT "C"</u> Suitability Letter from Authorized Agent

See attached Suitability Letter.

### <u>ATTACHMENT "D"</u> Exception to the Required Geologic Assessment

No exception will be requested.


Comal County OFFICE OF COMAL COUNTY ENGINEER

June 7, 2010

Mr. James Ingalls HMT Engineering & Surveying, Inc. 410 N. Seguin Avenue New Braunfels, TX 78130

Re: Christ Our King Anglican Church On-Site Sewage Facility Suitability Letter, within Comal County, Texas

Dear Mr. Ingalls:

In accordance with TAC  $\S213.5(b)(4)(F)(ii)$ , Comal County has found that the entire referenced site (except for areas listed below) is suitable for the use of private sewage facilities and will meet the special requirements for on-site sewage facilities located on the Edwards Aquifer recharge zone as specified in TAC  $\S285.40-42$  based on the following information submitted to our office on June 3, 2010:

- The Geologic Assessment, prepared by Arias & Associates
- The Water Pollution Abatement Plan (WPAP), prepared by HMT Engineering & Surveying, Inc.

#### Areas that are not Suitable

There are three water wells located on the referenced site and detailed below:

Feature ID	<u>Latitude</u>	Longitude [Variable]
S-1	29°42'50.9"	98°11'13.1"
S-2	29°42'52.3"	98°11'14.8"
S-3	29°42'49.8"	98°11'16.6"

According to the WPAP, there will be a 150' setback from these three features for all aspects of the OSSF.

Moreover, according to TAC §285.41(b), Christ the King Anglican Church, the owner of the referenced site, must inform, in writing, each prospective purchaser, lessee, or renter of the following:

- A Permit to Construct is required from Comal County before an OSSF can be constructed on the Christ the King Anglican Church land;
- A License to Operate is required from Comal County before an OSSF can be operated on the Christ the King Anglican Church land;
- That an application for a water pollution abatement plan, as defined in TAC §213, has been made, whether it has been approved, and if any restrictions or conditions have been placed on that approval; and

# Comal County

James Ingalls 6/7/10 Page 2

Minimum separation distances, as outlined in Table 10 of TAC §285.

Furthermore, according to TAC §285.42(a), if any recharge feature, not listed above, is discovered during construction of an OSSF, all regulated activities near the feature shall be suspended immediately. The owner shall immediately notify the TCEQ San Antonio office of the discovery of the feature. All activities regulated under TAC §213 shall not proceed near the feature until Comal County, in conjunction with the TCEQ San Antonio office, has reviewed and approved a plan proposed to protect the feature, the structural integrity of the OSSF, and the water quality of the aquifer. The plan shall be sealed, signed, and dated by a professional engineer.

Finally, on a separate matter, if, in the future, a residential subdivision, a manufactured housing community, a multi-unit residential development, a business park, or another similar structure that uses OSSFs for sewage disposal is proposed for this property, TAC §285.4(c) requires the submittal of planning materials for these developments. The planning materials shall be prepared by a professional engineer or professional sanitarian and shall include an overall site plan, topographic map, 100-year floodplain map, soil survey, location of water wells, locations of easements as identified in TAC §285.91(10) (relating to Tables), a comprehensive drainage plan, a complete report detailing the types of OSSFs to be considered and their compatibility with area-wide drainage and groundwater, and Edwards Aquifer requirements that are pertinent to the proposed OSSF. We have included Comal County's *Application for Licensing Authority Recommendation for Private Sewerage Facilities for a Proposed Subdivision* for your use if necessary.

If you have any questions or need additional information, please do not hesitate to contact our office.

Sincerely,

Robert Boyd, P.E. Comal County Assistant Engineer

cc: Jay Millikin, Comal County Commissioner, Precinct No. 2

# Greg W. Johnson, P.E., R.S.

170 Hollow Oak New Braunfels, Texas 78132 830/905-2778

June 3, 2010

#### Jeff Moeller, P.E.

Hollmig Moeller Thornhill, Inc. 410 North Seguin St. New Braunfels, Texas 78130

RE: Soil survey & OSSF compatibility Christ Our King Anglican Church FM 1863, Comal County

#### TYPE SOILS AND DRAINAGE

The referenced location was surveyed for the type soils and their compatibility with development and installation of individual septic systems for a church and associated facilities. Soil observations made throughout the property indicate shallow soil depths with restrictive rock layers being found. The soils have a moderate clay content and are a part of the Medlin-Eckrant association, undulating, (MEC), and the Krum Clay, (KrB) gently sloping one to five percent slopes and moderately well drained According to F.E.M.A. Map 48091C0430F/48091C0435C the site is not located within the 100 year floodplain. The soil profile consists of a dark grayish brown clay/ clay loam to 10-20" over a gray brown to yellow brown clay from 15-40" with blocky structure over limestone.

#### **OSSF TYPES**

Since the site contains Type III & IV soil having moderate to high clay content and poor soil absorption characteristics with shallow depth, a limited number of types of septic systems are suitable. The recommended On Site Sewage Facilities (OSSF) for this site is Aerobic Treatment with spray or drip irrigation. Future addition of a school and dormitory may increase waster use to a point at 5000 gallons per day that a state permitted sewage system may be required. This tract, is served by public water. Adequate space is available for the referenced OSSF and replacement area.

Respectfully yours,

FLSBS hnson P.E.



#### **OSSF Sizing**

Water usage and field requirements:

Church w/ 500 members Qavg = 500 GPD Church w/ Fellowship Hall Qavg = 800 GPD Church w/ Fellowship Hall & Community Center Qavg = 1300 GPD

Aerobic Treatment Plant (Spray Irrigation)

A = Q / Ri Ri = 0.064 g/sf

Church A = 500/0.064 = 7813 sf. Church + Fellowship Hall A = 800/0.064 = 12,500 sf. Church + Fellowship + Community A = 1300/0.064 = 20,313 sf.

Drip Irrigation

A = Q/Ra Ra = 0.2 g/sf (Type III Soil)

Church A = 500/0.2 = 2500 sf. Church + Fellowship A = 800/0.2 = 4000 sf. Church + Fellowship + Community A = 1300/0.2 = 6500 sf.

A = Q/Ra Ra = 0.1 g/sf (Type IV Soil)

Church A = 500/0.1 = 5000 sf. Church + Fellowship A = 800/0.1 = 8000 sf. Church + Fellowship + Community A = 1300/0.1 = 13,000 sf.

#### ON-SITE SEWERAGE FACILITY SOIL EVALUATION REPORT INFORMATION

Date Soil Survey Performed: \_\_\_\_\_June 02, 2010

Site Location: Christ our King Anglican Church - FM 1863

Proposed Excavation Depth: \_\_\_\_\_10-20"

**Requirements:** 

At least two soil excavations must be performed on the site, at opposite ends of the proposed disposal area. Locations of soil boring or dug pits must be shown on the site drawing. For subsurface disposal, soil evaluations must be performed to a depth of at least two feet below the proposed excavation depth. For surface disposal, the surface horizon must be evaluated. Describe each soil horizon and identify any restrictive features on the form. Indicate depths where features appear.

soi	L BORING	NUMBER	1				
	Depth (Feet)	Texture Class	Soil Texture	Gravel Analysis	Drainage (Mottles/ Water Table)	Restrictive Horizon	Observations
0	10''-20''	III/IV	CLAY/ CLAY LOAM				GRAY/BROWN
2 3 5	15"-40"	III/IV	CLAY/ CLAY LOAM	N/A	NO	LIMESTONE @ 30''-40''	YELLOW/ BROWN

so	IL BORING	NUMBER	2				
	Depth (Feet)	Texture Class	Soil Texture	Gravel Analysis	Drainage (Mottles/ Water Table)	Restrictive Horizon	Observations
0		SAME	AS	ABOVE			
2							
3							
4							

I certify that the findings of this report are based on my field observations and are accurate to the best of my ability.

Innson, P.E. 67587, S.E. 11561

102/2010



#### **Temporary Stormwater Section**

COUNTY ENGINEER for Regulated Activities on the Edwards Aquifer Recharge Zone and Relating to 30 TAC §213.5(b)(4)(A), (B), (D)(I) and (G); Effective June 1, 1999

#### REGULATED ENTITY NAME: Christ Our King Anglican Church

#### POTENTIAL SOURCES OF CONTAMINATION

Examples: Fuel storage and use, chemical storage and use, use of asphaltic products, construction vehicles tracking onto public roads, and existing solid waste.

- 1. Fuels for construction equipment and hazardous substances which will be used during construction:
  - Aboveground storage tanks with a cumulative storage capacity of less that 250 gallons will be stored on the site for less than one (1) year.
  - Aboveground storage tanks with a cumulative storage capacity between 250 gallons and 499 gallons will be stored on the site for less than one (1) year.
  - Aboveground storage tanks with a cumulative storage capacity of 500 gallons or more will be stored on the site. An Aboveground Storage Tank Facility Plan application must be submitted to the appropriate regional office of the TCEQ prior to moving the tanks onto the project.
  - Fuels and hazardous substances will not be stored on-site. X
- 2 X ATTACHMENT A - Spill Response Actions. A description of the measures to be taken to contain any spill of hydrocarbons or hazardous substances is provided at the end of this form.
- 3. N/A Temporary aboveground storage tank systems of 250 gallons or more cumulative storage capacity must be located a minimum horizontal distance of 150 feet from any domestic, industrial, irrigation, or public water supply well, or other sensitive feature.
- 4. X ATTACHMENT B - Potential Sources of Contamination. Describe in an attachment at the end of this form any other activities or processes which may be a potential source of contamination.
  - There are no other potential sources of contamination.

#### SEQUENCE OF CONSTRUCTION

- 5. X ATTACHMENT C - Sequence of Major Activities. A description of the sequence of maior activities which will disturb soils for major portions of the site (grubbing, excavation, grading, utilities, and infrastructure installation) is provided at the end of this form. For each activity described, an estimate of the total area of the site to be disturbed by each activity is given.
- 6. X Name the receiving water(s) at or near the site which will be disturbed or which will receive discharges from disturbed areas of the project: **Blieders Creek** and Unnamed Tributary of Dry Comal Creek

#### TEMPORARY BEST MANAGEMENT PRACTICES (TBMPs)

Erosion control examples: tree protection, interceptor swales, level spreaders, outlet stabilization, blankets or matting, mulch, and sod. Sediment control examples: stabilized construction exit, silt fence, filter dikes, rock berms, buffer strips, sediment traps, and sediment basins. Please refer to the

Technical Guidance Manual for guidelines and specifications. All structural BMPs must be shown on the site plan.

- 7. X ATTACHMENT D Temporary Best Management Practices and Measures. A description of the TBMPs and measures that will be used during and after construction are provided at the end of this form. For each activity listed in the sequence of construction, include appropriate control measures and the general timing (or sequence) during the construction process that the measures will be implemented.
  - X TBMPs and measures will prevent pollution of surface water, groundwater, and stormwater. The construction-phase BMPs for erosion and sediment controls have been designed to retain sediment on site to the extent practicable. The following information has been provided in the attachment at the end of this form
  - a. A description of how BMPs and measures will prevent pollution of surface water, groundwater or stormwater that originates upgradient from the site and flows across the site.
  - b. A description of how BMPs and measures will prevent pollution of surface water or groundwater that originates on-site or flows off site, including pollution caused by contaminated stormwater runoff from the site.
  - c. A description of how BMPs and measures will prevent pollutants from entering surface streams, sensitive features, or the aquifer.
  - d. A description of how, to the maximum extent practicable, BMPs and measures will maintain flow to naturally-occurring sensitive features identified in either the geologic assessment, TCEQ inspections, or during excavation, blasting, or construction.
- 8. The temporary sealing of a naturally-occurring sensitive feature which accepts recharge to the Edwards Aquifer as a temporary pollution abatement measure during active construction should be avoided.
  - ATTACHMENT E Request to Temporarily Seal a Feature. A request to temporarily seal a feature is provided at the end of this form. The request includes justification as to why no reasonable and practicable alternative exists for each feature.
     X There will be no temporary sealing of naturally-occurring sensitive features on the site.
- 9. X ATTACHMENT F Structural Practices. Describe the structural practices that will be used to divert flows away from exposed soils, to store flows, or to otherwise limit runoff discharge of pollutants from exposed areas of the site. Placement of structural practices in floodplains has been avoided.
- 10. X ATTACHMENT G Drainage Area Map. A drainage area map is provided at the end of this form to support the following requirements.
  - \_\_\_\_ For areas that will have more than 10 acres within a common drainage area disturbed at one time, a sediment basin will be provided.
  - \_\_\_\_ For areas that will have more than 10 acres within a common drainage area disturbed at one time, a smaller sediment basin and/or sediment trap(s) will be used.
  - For areas that will have more than 10 acres within a common drainage area disturbed at one time, a sediment basin or other equivalent controls are not attainable, but other TBMPs and measures will be used in combination to

protect down slope and side slope boundaries of the construction area.

- X There are no areas greater than 10 acres within a common drainage area that will be disturbed at one time. A smaller sediment basin and/or sediment trap(s) will be used in combination with other erosion and sediment controls within each disturbed drainage area.
- 11. <u>N/A</u> ATTACHMENT H Temporary Sediment Pond(s) Plans and Calculations. Temporary sediment pond or basin construction plans and design calculations for a proposed temporary BMP or measure has been prepared by or under the direct supervision of a Texas Licensed Professional Engineer. All construction plans and design information must be signed, sealed, and dated by the Texas Licensed Professional Engineer. Construction plans for the proposed temporary BMPs and measures are provided as at the end of this form.
- 12. X ATTACHMENT I Inspection and Maintenance for BMPs. A plan for the inspection of temporary BMPs and measures and for their timely maintenance, repairs, and, if necessary, retrofit is provided at the end of this form. A description of documentation procedures and recordkeeping practices is included in the plan.
- 13. X All control measures must be properly selected, installed, and maintained in accordance with the manufacturer's specifications and good engineering practices. If periodic inspections by the applicant or the executive director, or other information indicate a control has been used inappropriately, or incorrectly, the applicant must replace or modify the control for site situations.
- 14. X If sediment escapes the construction site, off-site accumulations of sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain).
- 15. **N/A** Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50%. A permanent stake will be provided that can indicate when the sediment occupies 50% of the basin volume.
- 16. <u>X</u> Litter, construction debris, and construction chemicals exposed to stormwater shall be prevented from becoming a pollutant source for stormwater discharges (e.g., screening outfalls, picked up daily).

#### SOIL STABILIZATION PRACTICES

Examples: establishment of temporary vegetation, establishment of permanent vegetation, mulching, geotextiles, sod stabilization, vegetative buffer strips, protection of trees, or preservation of mature vegetation.

- 17. X ATTACHMENT J Schedule of Interim and Permanent Soil Stabilization Practices. A schedule of the interim and permanent soil stabilization practices for the site is attached at the end of this form.
- 18. X Records must be kept at the site of the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 19. <u>X</u> Stabilization practices must be initiated as soon as practicable where construction activities have temporarily or permanently ceased.

#### **ADMINISTRATIVE INFORMATION**

Constant Same

- 20. X All structural controls will be inspected and maintained according to the submitted and approved operation and maintenance plan for the project.
- 21. X If any geologic or manmade features, such as caves, faults, sinkholes, etc., are discovered, all regulated activities near the feature will be immediately suspended. The appropriate TCEQ Regional Office shall be immediately notified. Regulated activities must cease and not continue until the TCEQ has reviewed and approved the methods proposed to protect the aquifer from any adverse impacts.
- 22. X Silt fences, diversion berms, and other temporary erosion and sediment controls will be constructed and maintained as appropriate to prevent pollutants from entering sensitive features discovered during construction.

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This **TEMPORARY STORMWATER SECTION** is hereby submitted for TCEQ review and executive director approval. The application was prepared by:

Jeffrey D. Moeller, P.E.

Print Name of Customer/Agent

ure of Eustomer/Agent

6/7/10

# ATTACHMENT "A" Spill Response Actions

Spill Prevention and Control

The objective of this section is to describe measures to prevent or reduce the discharge of pollutants to drainage systems or watercourses from leaks and spills by reducing the chance for spills, stopping the source of spills, containing and cleaning up spills, properly disposing of spill materials, and training employees.

The following steps will help reduce the stormwater impacts of leaks and spills:

## Education

(1) Be aware that different materials pollute in different amounts. Make sure that each employee knows what a "significant spill" is for each material they use, and what is the appropriate response for "significant" and "insignificant" spills. Employees should also be aware of when spill must be reported to the TCEQ. Information available in 30 TAC 327.4 and 40 CFR 302.4.

(2) Educate employees and subcontractors on potential dangers to humans and the environment from spills and leaks.

(3) Hold regular meetings to discuss and reinforce appropriate disposal procedures (incorporate into regular safety meetings).

(4) Establish a continuing education program to indoctrinate new employees.

(5) Have contractor's superintendent or representative oversee and enforce proper spill prevention and control measures.

#### **General Measures**

(1) To the extent that the work can be accomplished safely, spills of oil, petroleum products, and substances listed under 40 CFR parts 110,117, and 302, and sanitary and septic wastes should be contained and cleaned up immediately.

(2) Store hazardous materials and wastes in covered containers and protect from vandalism.

(3) Place a stockpile of spill cleanup materials where it will be readily accessible.

(4) Train employees in spill prevention and cleanup.

(5) Designate responsible individuals to oversee and enforce control measures.

(6) Spills should be covered and protected from stormwater runoff during rainfall to the extent that it doesn't compromise clean up activities.

(7) Do not bury or wash spills with water.

(8) Store and dispose of used clean up materials, contaminated materials, and recovered spill material that is no longer suitable for the intended purpose in conformance with the provisions in applicable BMP's.

(9) Do not allow water used for cleaning and decontamination to enter storm drains or watercourses. Collect and dispose of contaminated water in accordance with applicable regulations.

(10) Contain water overflow or minor water spillage and do not allow it to discharge into drainage facilities or watercourses.

(11) Place Material Safety Data Sheets (MSDS), as well as proper storage, cleanup, and spill reporting instructions for hazardous materials stored or used on the project site in an open, conspicuous, and accessible location.

(12) Keep waste storage areas clean, well organized, and equipped with ample cleanup supplies as appropriate for the materials being stored. Perimeter controls, containment structures, covers, and liners should be repaired or replaced as needed to maintain proper function.

# Cleanup

(1) Clean up leaks and spills immediately.

(2) Use a rag for small spills on paved surfaces, a damp mop for general cleanup, and absorbent material for larger spills. If the spilled material is hazardous, then the used cleanup materials are also hazardous and must be disposed of as hazardous waste.

(3) Never hose down or bury dry material spills. Clean up as much of the material as possible and dispose of properly. See the waste management BMP's in this section for specific information.

## Minor Spills

(1) Minor spills typically involve small quantities of oil, gasoline, paint, etc. which can be controlled by the first responder at the discovery of the spill.

(2) Use absorbent materials on small spills rather than hosing down or burying the spill.

(3) Absorbent materials should be promptly removed and disposed of properly.

(4) Follow the practice below for a minor spill:

- (5) Contain the spread of the spill.
- (6) Recover spilled materials.

(7) Clean the contaminated area and properly dispose of contaminated materials.

# Semi-Significant Spills

Semi-significant spills still can be controlled by the first responder along with the aid of other personnel such as laborers and the foreman, etc. This response may require the cessation of all other activities.

Spills should be cleaned up immediately:

(1) Contain spread of the spill.

(2) Notify the project foreman immediately.

(3) If the spill occurs on paved or impermeable surfaces, clean up using "dry" methods (absorbent materials, cat litter and/or rags). Contain the spill by encircling with absorbent materials and do not let the spill spread widely.

(4) If the spill occurs in dirt areas, immediately contain the spill by constructing an earthen dike. Dig up and properly dispose of contaminated soil.

(5) If the spill occurs during rain, cover spill with tarps or other material to prevent contaminating runoff.

## Significant/Hazardous Spills

For significant or hazardous spills that are in reportable quantities:

(1) Notify the TCEQ by telephone as soon as possible and within 24 hours at 512-339-2929 (Austin) or 210-490-3096 (San Antonio) between 8 AM and 5 PM. After hours, contact the Environmental Release Hotline at 1-800-832-8224. It is the contractor's responsibility to have all emergency phone numbers at the construction site.

(2) For spills of federal reportable quantities, in conformance with the requirements in 40 CFR parts 110,119, and 302, the contractor should notify the National Response Center at (800) 424-8802.

(3) Notification should first be made by telephone and followed up with a written report.

(4) The services of a spills contractor or a Haz-Mat team should be obtained immediately. Construction personnel should not attempt to clean up until the appropriate and qualified staffs have arrived at the job site.

(5) Other agencies which may need to be consulted include, but are not limited to, the City Police Department, County Sheriff Office, Fire Departments, etc.

More information on spill rules and appropriate responses is available on the TCEQ website at: http://www.tnrcc.state.tx.us/enforcement/emergency\_response.html

# Vehicle and Equipment Maintenance

(1) If maintenance must occur onsite, use a designated area and a secondary containment, located away from drainage courses, to prevent the runoff of stormwater and the runoff of spills.

(2) Regularly inspect onsite vehicles and equipment for leaks and repair immediately

(3) Check incoming vehicles and equipment (including delivery trucks, and employee and subcontractor vehicles) for leaking oil and fluids. Do not allow leaking vehicles or equipment onsite.

(4) Always use secondary containment, such as a drain pan or drop cloth, to catch spills or leaks when removing or changing fluids.

(5) Place drip pans or absorbent materials under paving equipment when not in use.

(6) Use absorbent materials on small spills rather than hosing down or burying the spill. Remove the absorbent materials promptly and dispose of properly.

(7) Promptly transfer used fluids to the proper waste or recycling drums. Don't leave full drip pans or other open containers lying around.

(8) Oil filters disposed of in trashcans or dumpsters can leak oil and pollute stormwater. Place the oil filter in a funnel over a waste oil-recycling drum to drain excess oil before disposal. Oil filters can also be recycled. Ask the oil supplier or recycler about recycling oil filters.

(9) Store cracked batteries in a non-leaking secondary container. Do this with all cracked batteries even if you think all the acid has drained out. If you drop a battery, treat it as if it is cracked. Put it into the containment area until you are sure it is not leaking.

# Vehicle and Equipment Fueling

(1) If fueling must occur on site, use designated areas, located away from drainage courses, to prevent the runoff of stormwater and the runoff of spills.

(2) Discourage "topping off" of fuel tanks.

(3) Always use secondary containment, such as a drain pan, when fueling to catch spills/ leaks.

# ATTACHMENT "B" Potential Sources of Contamination

The only potential sources of contamination are construction equipment leaks, re-fueling spills, as well as potential from port-o-lets, and the total suspended solids (TSS) due to the construction activities on-site. There are no other anticipated potential sources of contamination.

#### ATTACHMENT "C" Sequence of Major Activities

Stages of construction:

- 1. Install temporary BMP's.
- 2. Phase 1 Construction
  - a. Minor site grading: This includes the removal of organic material and other debris within the proposed parking and building site. Approximate disturbed area 3.05 acres.
  - b. Grading: Cutting and filling of the proposed site to prepare the site for parking and foundation construction. Approximate disturbed area 3.05 acres.
  - c. Vortechs® System #1 & #2 Installation: Vortechs® System #1 will be installed at the southwest corner of the parking area. Vortechs® System #2 will be installed at the southeast corner of the parking area. See Permanent Storm water Section.
  - d. Utility Installation: Water service will be provided by the existing well, and sewer service will be provided by a septic system that will be designed and constructed in this phase. Small sewer, water, and electric services will be installed at this time.
  - e. Finished Grading: Final landscaping, asphalt parking, and building infrastructure are installed. Approximate disturbed area 3.05 acres.
  - f. Vegetative Filter Strip Installation: Upon completion of the paved areas and final grading, the vegetative filter strips are installed, See Permanent Storm water Section.
- 3. Phase 2 Construction
  - a. Minor site grading: This includes the removal of organic material and other debris within the proposed parking and building site. Approximate disturbed area 2.23 acres.
  - b. Grading: Cutting and filling of the proposed site to prepare the site for parking and foundation construction. Approximate disturbed area 2.23 acres.
  - c. Vortechs® System #3 Installation: Vortechs® System #3 will be installed at the northeast corner of the parking area. See Permanent Storm water Section.
  - d. Utility Installation: Primary utility have were constructed in Phase 1. Small sewer, water, and electric services will be installed at this time.
  - e. Finished Grading: Final landscaping, asphalt parking, and building infrastructure are installed. Approximate disturbed area 2.23 acres.

- f. Vegetative Filter Strip Installation: Upon completion of the paved areas and final grading, the vegetative filter strips are installed, See Permanent Storm water Section.
- 4. Phase 3 Construction
  - a. Minor site grading: This includes the removal of organic material and other debris within the proposed parking and building site. Approximate disturbed area 0.65 acres.
  - b. Grading: Cutting and filling of the proposed site to prepare the site for parking and foundation construction. Approximate disturbed area 0.65 acres.
  - c. Utility Installation: Primary utility have were constructed in earlier phases. Small sewer, water, and electric services will be installed at this time.
  - d. Finished Grading: Final landscaping, asphalt parking, and building infrastructure are installed. Approximate disturbed area 0.65 acres.
  - e. Vegetative Filter Strip Installation: Upon completion of the paved areas and final grading, the vegetative filter strips are installed, See Permanent Storm water Section.
- 5. Phase 4 Construction
  - a. Minor site grading: This includes the removal of organic material and other debris within the proposed parking and building site. Approximate disturbed area 1.88 acres.
  - b. Grading: Cutting and filling of the proposed site to prepare the site for parking and foundation construction. Approximate disturbed area 1.88 acres.
  - c. Utility Installation: Primary utility have were constructed in earlier phases. Small sewer, water, and electric services will be installed at this time.
  - d. Finished Grading: Final landscaping, asphalt parking, and building infrastructure are installed. Approximate disturbed area 1.88 acres.
  - e. Vegetative Filter Strip Installation: Upon completion of the paved areas and final grading, the vegetative filter strips are installed, See Permanent Storm water Section.
- 6. Phase 5 Construction
  - a. Minor site grading: This includes the removal of organic material and other debris within the proposed parking and building site. Approximate disturbed area 1.08 acres.
  - b. Grading: Cutting and filling of the proposed site to prepare the site for parking and foundation construction. Approximate disturbed area 1.08 acres.
  - c. Utility Installation: Primary utility have were constructed in earlier phases. Small sewer, water, and electric services will be installed at this time.
  - d. Finished Grading: Final landscaping, asphalt parking, and building infrastructure are installed. Approximate disturbed area 1.08 acres.
  - e. Vegetative Filter Strip Installation: Upon completion of the paved areas and final grading, the vegetative filter strips are installed, See Permanent Storm water Section.
- 7. Phase 6 Construction
  - a. Minor site grading: This includes the removal of organic material and other debris within the proposed parking and building site. Approximate disturbed area 4.57 acres.

- b. Grading: Cutting and filling of the proposed site to prepare the site for parking and foundation construction. Approximate disturbed area 4.57 acres.
- c. Vortechs® System #4 & #5 Installation: Vortechs® System #4 will be installed at the southwest corner of the parking area. Vortechs® System #5 will be installed at the southeast corner of the parking area. See Permanent Storm water Section.
- d. Utility Installation: Primary utility have were constructed in earlier phases. Small sewer, water, and electric services will be installed at this time.
- e. Finished Grading: Final landscaping, asphalt parking, and building infrastructure are installed. Approximate disturbed area 4.57 acres.
- f. Vegetative Filter Strip Installation: Upon completion of the paved areas and final grading, the vegetative filter strips are installed, See Permanent Storm water Section.

## ATTACHMENT "D" Temporary BMP's and Measures

The following sequence will be followed for installing temporary BMP's:

- 1. Silt fence will be constructed on the downgradient side of proposed site.
- 2. A stabilized construction exit will be installed prior to any site work.
- 3. A rock berm will be installed at the southernmost downstream.

A. There is no upgradient stormwater, since the site is at the top of the watershed. All stormwater affecting this site is generated on site and described is section B below.

B. Silt fence will be placed on the downgradient side of each proposed improvement to contain pollutants generated from onsite runoff. Soil disturbance will be limited to a minimal distance outside the proposed pavement and building pads. Disturbed areas will be seeded to replace destroyed vegetation. The existing vegetation located downgradient of each proposed improvement will work in conjunction with the silt fence, rock berms, and stabilized construction entrance to prevent pollution of water originating onsite and/or flowing offsite.

C. The proposed silt fences, rock berm, and stabilized construction entrances constructed upgradient of the existing streams will prevent pollutants from entering them as well as the aquifer. According to the Geologic Assessment, there are no sensitive features with the project boundary.

D. There were no sensitive features identified in the Geologic Assessment.

Christ Our King Anglican Church Water Pollution Abatement Plan

## <u>ATTACHMENT "E"</u> Request to Temporarily Seal a Feature

There will be no request to temporarily seal a feature.

#### ATTACHMENT "F" Structural Practices

Rock berms and silt fence will be used to protect disturbed soils and to prevent contamination from leaving the project site.

#### ATTACHMENT "G" Drainage Area Map

See Drainage Area Map at the end of this section.

# **<u>ATTACHMENT "H"</u> Temporary Sediment Pond Plans and Calculations**

There will not be more than 10 acres of disturbed soil in one common drainage area that will occur at one time. Silt fence will be used for small drainage areas. No sediment ponds will be constructed due to the minimal amount of soil disturbance.

# ATTACHMENT "I" Inspection and Maintenance for BMP's

## Inspection and Maintenance Plan

The contractor is required to inspect the control and fences at weekly intervals and after any rainfall events to insure that they are functioning properly. The person(s) responsible for maintenance controls and fences shall immediately make any necessary repairs to damaged areas.

<u>Temporary Construction Entrance/Exit</u>: The entrance should be maintained in a condition, which will prevent tracking or flowing of sediment onto public rights-of-way. This may require periodic top dressing with additional stone as conditions demand and repair and/or cleanout of any measures used to trap sediment. All sediment spilled, dropped, washed or tracked onto public rights-of-way should be removed immediately by contractor. When necessary, wheels should be cleaned to remove sediment prior to entrance onto public right-of-way. When washing is required, it should be done on an area stabilized with crushed stone that drains into an approved sediment trap or sediment basin. All sediment should be prevented from entering any storm drain, ditch or water course by using approved methods.

<u>Silt Fence:</u> Remove sediment when buildup reaches 6 inches. Replace any torn fabric or install a second line of fencing parallel to the torn section. Replace or repair any sections crushed or

Christ Our King Anglican Church Water Pollution Abatement Plan

collapsed in the course of construction activity. If a section of fence is obstructing vehicular access, consider relocating it to a spot where it will provide equal protection, but will not obstruct vehicles. A triangular filter dike may be preferable to a silt fence at common vehicle access points. When construction is complete, the sediment should be disposed of in a manner that will not cause additional siltation and the prior location of the silt fence should be revegetated. The fence itself should be disposed of in an approved landfill.

<u>Rock Berms</u>: For installation in streambeds, additional daily inspections shall be made. Remove sediment and other debris when buildup reaches 6 inches and dispose of the accumulated silt in an approved manner that will not cause any additional siltation. Repair any loose wire sheathing. The berm shall be reshaped as needed during inspection. The berm shall be replaced when the structure ceases to function as intended due to silt accumulation among the rocks, washout, construction traffic damage, etc. The rock berm shall be left in place until all upstream areas are stabilized and accumulated silt removed.

TCEQ staff will be allowed full access to the property during construction of the project for inspecting controls and fences and to verify that the accepted plan is being utilized in the field. TCEQ staff has the right to speak with the contractor to verify plan changes and modifications.

Documentation: All scheduled inspection and maintenance measures made to the temporary BMPs must be documented clearly on the WPAP Site Plan showing inspection/maintenance measures performed, date, and person responsible for inspection and maintenance. Any changes made to the location or type of controls shown on the accepted plans, due to onsite conditions, shall be documented on the site plan that is part of this Water Pollution Abatement Plan. No other changes shall be made unless approved by TCEQ and the Design Engineer. Documentation shall clearly show changes made, date, and person responsible and reason change was made.

## **Owner's Information:**

Owner:	Christ Our King Anglican Church
Contact:	Charles Salsman
Phone:	(830) 632-7744
Address:	111 W. San Antonio St, Suite 250
	New Braunfels, TX 78130

## **Design Engineer:**

Company:	HMT Engineering & Surveying
Contact:	Jeffrey D. Moeller, P.E.
Phone:	(830) 625-8555
Address:	410 N. Seguin Street
	New Braunfels, Texas 78130

Christ Our King Anglican Church Water Pollution Abatement Plan

# Person or Firm Responsible for Erosion/Sedimentation Control Maintenance:

Company:	
Contact:	
Phone:	
Address:	

Signature of Responsible Party:

# This portion of the form shall be filled out and signed by the responsible party prior to construction.

# <u>ATTACHMENT "J"</u> Schedule of Interim and Permanent Soil Stabilization Practices

Areas which are disturbed by construction staging and storage areas will be hydro mulched with the appropriate seed mixture. Areas between the edge of pavement and property line will also be hydro mulched. There will be no fill slopes exceeding a 3:1 slope and all fill slopes will be hydro mulched. <u>All disturbed soils should be seeded or otherwise stabilized within 14 calendar days after final grading or where construction activity has temporarily ceased for more than 21 days.</u> Installation and acceptable mixtures of hydro mulch are as follows:

## Materials:

<u>Hydraulic Mulches:</u> Wood fiber mulch can be applied alone or as a component of hydraulic matrices. Wood fiber applied alone is typically applied at the rate of 2,000 to 4,000 lb/acre. Wood fiber mulch is manufactured from wood or wood waste from lumber mills or from urban sources.

<u>Hydraulic Matrices:</u> Hydraulic matrices include a mixture of wood fiber and acrylic polymer or other tackifier as binder. Apply as a liquid slurry using a hydraulic application machine (i.e., hydro seeder) at the following minimum rates, or as specified by the manufacturer to achieve complete coverage of the target area: 2,000 to 4,000 lb/acre wood fiber mulch, and 5 to 10% (by weight) of tackifier (acrylic copolymer, guar, psyllium, etc.)

Bonded Fiber Matrix: Bonded fiber matrix (BFM) is a hydraulically applied system of fibers and adhesives that upon drying forms an erosion resistant blanket that promotes vegetation, and prevents soil erosion. BFMs are typically applied at rates from 3,000 lb/acre to 4,000 lb/acre based on the manufacturer's recommendation. A biodegradable BFM is composed of materials that are 100% biodegradable. The binder in the BFM should also be biodegradable and should not dissolve or disperse upon re-wetting. Typically, biodegradable BFMs should not be applied immediately before, during or immediately after rainfall if the soil is saturated. Depending on the product, BFMs typically require 12 to 24 hours to dry and become effective.

Seed	Mixtures:
1	

Dates	Climate	Species	(lb/ac.)
Sept. 1 to Nov. 30	Temporary Cool Season	Tall Fescue	4.0
		Oats	21.0
		Wheats	30.0
		Total	55.0
Sept. 1 to Nov. 30	Cool Season Legume	Hairy Vetch	8.0
May 1 to Aug. 31	Temporary Warm Season	Foxtail Millet	30.0

<u>Fertilizer:</u> Fertilizer should be applied at the rate of 40 pounds of nitrogen and 40 pounds of phosphorus per acre, which is equivalent to about 1.0 pounds of nitrogen and phosphorus per 1000 square feet.

## Installation:

(1) Prior to application, roughen embankment and fill areas by rolling with a crimping or punching type roller or by track walking. Track walking shall only be used where other methods are impractical.

(2) To be effective, hydraulic matrices require 24 hours to dry before rainfall occurs.

(3) Avoid mulch over spray onto roads, sidewalks, drainage channels, existing vegetation, etc.



Drainage Area ID	Phase	Total Area	Impervious Are
1	1	0.15	0.15
2	2	0.11	0.11
3	2	0.23	0.23
4	2	0.16	0.19
5	2	0.04	0.04
6	1	0.14	0.13
7	2	0.17	0.14
8	2	0.19	0.11
9	2	0.97	0.00
10	3	0.12	0.12
11	1	0.06	0.06
12	2	0.47	0.20
13	2	0.05	0.05
14	2	0.45	0.26
15	3	0.53	0.33
16	4	0.24	0.12
17	4	0.73	0.41
18	4	0.04	0.04
19	4	0.87	0.53
20	5	0.88	0.59
21	1	1.15	0.96
22	1	1.62	1.31
23	6	1.98	1.40
24	6	2.59	1.88

<ul> <li>LECEND</li> <li>IAGUIDADA</li> <li>IAGUIDA</li></ul>	And N. SEGUIN ST. NEW BRAUNFELS TEXAS, 78130 HD R. 830–625–8555 Fax: 830–625–8556	DRAINAGE AREA MAP	CHRIST OUR KING ANGLICAN CHURCH 111 W. SAN ANTONIO ST, SUITE 250 NEW BRAUNFELS, TEXAS 78130	DATE: 6/7/2010 DRAWN BY: JII DESIGNED BY: JII CHECKED BY: JOS REVIEWED BY: JDM PROJECT NUMBER: COKOO1.101
LEGEND LARI BOUNDARY ACK BERM BITS OF DRAINAGE AREA ROCK BERM BIT FENCE CACK BERM CACK BERM CACK BOUNDARY CACK BERM CACK BERM				
	LEGAL BOUNDARY LIMITS OF DRAINAGE AREA ROCK BERM SILT FENCE STABILIZED CONSTRUCTION ENTRANCE VEGETATIVE FILTER STRIP	<ul> <li>9.11 AC</li> <li>41.2%</li> </ul>		

RECEIVED

JUN 1 1 2010

#### Permanent Stormwater Section

for Regulated Activities on the Edwards Aquifer Recharge Zone COUNTY ENGINEER and Relating to 30 TAC §213.5(b)(4)(C), (D)(Ii), (E), and (5), Effective June 1, 1999

#### REGULATED ENTITY NAME: Christ Our King Anglican Church

# Permanent best management practices (BMPs) and measures that will be used during and after construction is completed.

- 1. X Permanent BMPs and measures must be implemented to control the discharge of pollution from regulated activities after the completion of construction.
- 2. X These practices and measures have been designed, and will be constructed, operated, and maintained to insure that 80% of the incremental increase in the annual mass loading of total suspended solids (TSS) from the site caused by the regulated activity is removed. These quantities have been calculated in accordance with technical guidance prepared or accepted by the executive director.
  - X The TCEQ Technical Guidance Manual (TGM) was used to design permanent BMPs and measures for this site.
  - A technical guidance other than the TCEQ TGM was used to design permanent BMPs and measures for this site. The complete citation for the technical guidance that was used is provided below:
- 3. X Owners must insure that permanent BMPs and measures are constructed and function as designed. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the appropriate regional office within 30 days of site completion.
- 4. **N/A** Where a site is used for low density single-family residential development and has 20 % or less impervious cover, other permanent BMPs are not required. This exemption from permanent BMPs must be recorded in the county deed records, with a notice that if the percent impervious cover increases above 20% or land use changes, the exemption for the whole site as described in the property boundaries required by 30 TAC §213.4(g) (relating to Application Processing and Approval), may no longer apply and the property owner must notify the appropriate regional office of these changes.
  - \_\_\_\_ This site will be used for low density single-family residential development and has 20% or less impervious cover.
  - \_\_\_\_ This site will be used for low density single-family residential development but has more than 20% impervious cover.
  - \_\_\_\_ This site will not be used for low density single-family residential development.
- 5. **N/A** The executive director may waive the requirement for other permanent BMPs for multifamily residential developments, schools, or small business sites where 20% or less impervious cover is used at the site. This exemption from permanent BMPs must be recorded in the county deed records, with a notice that if the percent impervious cover increases above 20% or land use changes, the exemption for the whole site as described in the property boundaries required by 30 TAC §213.4(g) (relating to Application Processing and Approval), may no longer apply and the property owner must notify the appropriate regional office of these changes.

- ATTACHMENT A 20% or Less Impervious Cover Waiver. This site will be used for multi-family residential developments, schools, or small business sites and has 20% or less impervious cover. A request to waive the requirements for other permanent BMPs and measures is found at the end of this form.
- X This site will be used for multi-family residential developments, schools, or small business sites but has more than 20% impervious cover.
- \_\_\_\_ This site will not be used for multi-family residential developments, schools, or small business sites.

#### 6. ATTACHMENT B - BMPs for Upgradient Stormwater.

- A description of the BMPs and measures that will be used to prevent pollution of surface water, groundwater, or stormwater that originates upgradient from the site and flows across the site is identified as **ATTACHMENT B** at the end of this form.
- X If no surface water, groundwater or stormwater originates upgradient from the site and flows across the site, an explanation is provided as **ATTACHMENT B** at the end of this form.
- \_\_\_\_\_ If permanent BMPs or measures are not required to prevent pollution of surface water, groundwater, or stormwater that originates upgradient from the site and flows across the site, an explanation is provided as **ATTACHMENT B** at the end of this form.

#### 7. ATTACHMENT C - BMPs for On-site Stormwater.

- X A description of the BMPs and measures that will be used to prevent pollution of surface water or groundwater that originates on-site or flows off the site, including pollution caused by contaminated stormwater runoff from the site is identified as **ATTACHMENT C** at the end of this form.
- \_\_\_\_\_ If permanent BMPs or measures are not required to prevent pollution of surface water or groundwater that originates on-site or flows off the site, including pollution caused by contaminated stormwater runoff, an explanation is provided as **ATTACHMENT C** at the end of this form.
- 8. X ATTACHMENT D BMPs for Surface Streams. A description of the BMPs and measures that prevent pollutants from entering surface streams, sensitive features, or the aquifer is provided at the end of this form. Each feature identified in the Geologic Assessment as "sensitive" has been addressed.
- 9. X The applicant understands that to the extent practicable, BMPs and measures must maintain flow to naturally occurring sensitive features identified in either the geologic assessment, executive director review, or during excavation, blasting, or construction.
  - X The permanent sealing of or diversion of flow from a naturally-occurring "sensitive" or "possibly sensitive" feature that accepts recharge to the Edwards Aquifer as a permanent pollution abatement measure has not been proposed for any naturally-occurring "sensitive" or "possibly sensitive" features on this site.
  - **N/A ATTACHMENT E Request to Seal Features.** A request to seal a naturallyoccurring "sensitive" or "possibly sensitive" feature, that includes a justification as to why no reasonable and practicable alternative exists, is found at the end of this form. A request and justification has been provided for each feature.
- 10. X ATTACHMENT F Construction Plans. Construction plans and design calculations for the proposed permanent BMPs and measures have been prepared by or under the direct supervision of a Texas Licensed Professional Engineer. All construction plans and design information have been signed, sealed, and dated by the Texas Licensed Professional Engineer. Construction plans for the proposed permanent BMPs and measures are provided at the end of this form. Design Calculations, TCEQ

Construction Notes, all man-made or naturally occurring geologic features, all proposed structural measures, and appropriate details must be shown on the construction plans.

- ATTACHMENT G Inspection, Maintenance, Repair and Retrofit Plan. A plan for the 11. X inspection, maintenance, repair, and, if necessary, retrofit of the permanent BMPs and measures is provided at the end of this form. The plan has been prepared and certified by the engineer designing the permanent BMPs and measures. The plan has been signed by the owner or responsible party. The plan includes procedures for documenting inspections, maintenance, repairs, and, if necessary, retrofits as well as a discussion of record keeping procedures.
- 12. Х The TCEQ Technical Guidance Manual (TGM) was used to design permanent BMPs and measures for this site.
  - Pilot-scale field testing (including water quality monitoring) may be required for BMPs that are not contained in technical guidance recognized by or prepared by the executive director.
    - ATTACHMENT H Pilot-Scale Field Testing Plan. A plan for pilot-scale field testing is provided at the end of this form.
- 13. ATTACHMENT I -Measures for Minimizing Surface Stream Contamination. X Α description of the measures that will be used to avoid or minimize surface stream contamination and changes in the way in which water enters a stream as a result of the construction and development is provided at the end of this form. The measures address increased stream flashing, the creation of stronger flows and in-stream velocities, and other in-stream effects caused by the regulated activity which increase erosion that results in water quality degradation.

#### Responsibility for maintenance of permanent BMPs and measures after construction is complete.

- 14. Х The applicant is responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. Such entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred.
- 15. Х A copy of the transfer of responsibility must be filed with the executive director at the appropriate regional office within 30 days of the transfer if the site is for use as a multiple single-family residential development, a multi-family residential development, or a non-residential development such as commercial, industrial, institutional, schools, and other sites where regulated activities occur.

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This PERMANENT STORMWATER SECTION is hereby submitted for TCEQ review and executive director approval. The application was prepared by:

Jeffrey D. Moeller, P.E. Print Name of Customer/Agent

Customer/Agent

TCEQ-0600 (Rev. 10/01/04)

# <u>ATTACHMENT "A"</u> 20% of Less Impervious Cover Waiver

The proposed development is a church campus and the 20% Impervious Cover Waiver does not apply. Permanent BMP's will be designed in accordance with TCEQ requirements for the removal of TSS generated by the proposed development.

# <u>ATTACHMENT "B"</u> BMP's for Upgradient Stormwater

The proposed site is at the top of the drainage area, thus no upgradient stormwater is accepted by the site.

## <u>ATTACHMENT "C"</u> BMP's for On-Site Stormwater

The permanent BMP's used to treat on-site stormwater runoff will be a combination of the Vortechs® system and vegetative filter strips. Please refer to the Drainage Area Map in the Temporary Stormwater Section for areas of treatment and BMP structures used.

## ATTACHMENT "D" BMP's for Surface Streams

The vegetative filter strips and Vortechs® Storm water treatment system will be installed to prevent pollutants from entering surface streams and ultimately the aquifer. There were no sensitive features identified by the Geologic Assessment.

The natural vegetation located down gradient of proposed improvements will provide additional filtration to help prevent pollutant from entering streams, sensitive features, and the aquifer.

## <u>ATTACHMENT "G"</u> Inspection, Maintenance, Repair and Retrofit Plan

# **Vegetative Filter Strips Maintenance and Monitoring Procedures**

- *Pest Management* An Integrated Pest Management (IPM) Plan should be developed for vegetated areas. This plan should specify how problem insects and weeds will be controlled with minimal or no use of insecticides and herbicides.
- Seasonal Mowing and Lawn Care If the filter strip is made up of turf grass, it should be mowed as needed to limit vegetation height to 18 inches, using a mulching mower (or removal of clippings). If native grasses are used, the filter may require less frequent mowing, but a minimum of twice annually. Grass clippings and brush debris should not be deposited on vegetated filter strip areas. Regular mowing should also include weed control practices, however herbicide use should be kept to a minimum (Urbonas et al., 1992). Healthy grass can be maintained without using fertilizers because runoff usually contains sufficient nutrients. Irrigation of the site can help assure a dense and healthy vegetative cover.
- *Inspection* Inspect filter strips at least twice annually for erosion or damage to vegetation; however, additional inspection after periods of heavy runoff is most desirable. The strip should be checked for uniformity of grass cover, debris and litter, and areas of sediment accumulation. More frequent inspections of the grass cover during the first few years after establishment will help to determine if any problems are developing, and to plan for long-term restorative maintenance needs. Bare spots and areas of erosion identified during semi-annual inspections must be replanted and restored to meet specifications. Construction of a level spreader device may be necessary to reestablish shallow overland flow.
- *Debris and Litter Removal* Trash tends to accumulate in vegetated areas, particularly along highways. Any filter strip structures (i.e. level spreaders) should be kept free of obstructions to reduce floatables being flushed downstream, and for aesthetic reasons. The need for this practice is determined through periodic inspection, but should be performed no less than 4 times per year.
- Sediment Removal Sediment removal is not normally required in filter strips, since the vegetation normally grows through it and binds it to the soil. However, sediment may accumulate along the upstream boundary of the strip preventing uniform overland flow. Excess sediment should be removed by hand or with flatbottomed shovels.
- *Grass Reseeding and Mulching* A healthy dense grass should be maintained on the filter strip. If areas are eroded, they should be filled, compacted, and resceded

so that the final grade is level. Grass damaged during the sediment removal process should be promptly replaced using the same seed mix used during filter strip establishment. If possible, flow should be diverted from the damaged areas until the grass is firmly established. Bare spots and areas of erosion identified during semi-annual inspections must be replanted and restored to meet specifications. Corrective maintenance, such as weeding or replanting should be done more frequently in the first two to three years after installation to ensure stabilization. Dense vegetation may require irrigation immediately after planting, and during particularly dry periods, particularly as the vegetation is initially established.

## <u>ATTACHMENT "I"</u> Measures for Minimizing Surface Stream Contamination

All surface streams will be protected from erosion by not allowing runoff to exceed existing velocities. A portion of the runoff from the proposed development will sheet flow into the vegetative filter strips. The vegetative filter strips will be designed in order to maintain existing runoff velocities prior to leaving the site. The stormwater runoff for the remainder of the property will be concentrated into the Vortechs® system where the pollutants will be removed.

# Vortechs<sup>®</sup> Maintenance

The Vortechs system should be inspected at regular intervals and maintained when necessary to ensure optimum performance. The rate at which the system collects pollutants will depend more heavily on site activities than the size of the unit, e.g., unstable soils or heavy winter sanding will cause the swirl chamber to fill more quickly but regular sweeping will slow accumulation.

#### Inspection

Inspection is the key to effective maintenance and is easily performed. Pollutant deposition and transport may vary from year to year and regular inspections will help ensure that the system is cleaned out at the appropriate time. Inspections should be performed twice per year (i.e. spring and fall) however more frequent inspections may be necessary in equipment washdown areas and in climates where winter sanding operations may lead to rapid accumulations. It is useful and often required as part of a permit to keep a record of each inspection. A simple inspection and maintenance log form for doing so is provided on the following page, and is also available on contechstormwater.com.

The Vortechs system should be cleaned when inspection reveals that the sediment depth has accumulated to within 12 to 18 inches (300 to 450 mm) of the dry-weather water surface elevation. This determination can be made by taking two measurements with a stadia rod or similar measuring device; one measurement from the manhole opening to the top of the sediment pile and the other from the manhole opening to the water surface. <u>Note</u>: To avoid underestimating the volume of sediment in the chamber, the measuring device must be carefully lowered to the top of the sediment pile. Finer, silty particles at the top of the pile typically offer less resistance to the end of the rod than larger particles toward the bottom of the pile.

#### Cleaning

Cleaning of the Vortechs system should be done during dry weather conditions when no flow is entering the system. Cleanout of the Vortechs system with a vacuum truck is generally the most effective and convenient method of excavating pollutants from the system. If such a truck is not available, a "clamshell" grab may be used, but it is difficult to remove all accumulated pollutants using a "clamshell".

In installations where the risk of petroleum spills is small, liquid contaminants may not accumulate as quickly as sediment. However, an oil or gasoline spill should be cleaned out immediately. Motor oil and other hydrocarbons that accumulate on a more routine basis should be removed when an appreciable layer has been captured. To remove these pollutants, it may be preferable to use adsorbent pads to solidify the oil since these pads are usually much easier to remove from the unit individually and less expensive to dispose of than the oil/water emulsion that may be created by vacuuming the oily layer. Floating trash can be netted out if you wish to separate it from the other pollutants.

Cleaning of a Vortechs system is typically done by inserting a vacuum hose into the swirl chamber and evacuating this chamber of water and pollutants. As water is evacuated, the water level outside of the swirl chamber will drop to a level roughly equal to the crest of the lower aperture of the swirl chamber. The water outside the swirl chamber should remain near this level throughout pumping as the bottom and sides of the swirl chamber are sealed to the tank floor and walls. This "water lock" feature prevents water from migrating into the swirl chamber, exposing the bottom of the baffle wall and creating excess pump-out volume. Floating pollutants will decant into the swirl chamber as the water level is drawn down. This allows most floating material to be withdrawn from the same access point above the swirl chamber. Floating material that does not decant into the swirl chamber. Floating material that should be skimmed from the baffle chamber. If maintenance is not performed as recommended, sediment may accumulate outside the swirl chamber. If this is the case, it may be necessary to pump out other chambers. It is advisable to check for sediment accumulation in all chambers during inspection and maintenance.

These maintenance recommendations apply to all Vortechs systems with the following exceptions:

- It is strongly recommended that when cleaning systems larger than the Model 16000 the baffle chamber be drawn down to depth of three feet prior to beginning clean-out of the swirl chamber. Drawing down this chamber prior to the swirl chamber reduces adverse structural forces pushing upstream on the swirl chamber once that chamber is empty.
- 2. Entry into a Vortechs system is generally not required as cleaning can be done from the ground surface. However, if manned entry into a system is required the entire system should be evacuated of water prior to entry regardless of the system size.

Manhole covers should be securely seated following cleaning activities to prevent leakage of runoff into the system from above and also to ensure proper safety precautions. If anyone physically enters the unit, Confined Space Entry procedures need to be followed.

Disposal of all material removed from the Vortechs system should be done in accordance with local regulations. In many locations, disposal of evacuated sediments may be handled in the same manner as disposal of sediments removed from catch basins or deep sump manholes. Check your local regulations for specific requirements on disposal.

For assistance with maintaining your Vortechs system, contact us regarding the CONTECH Maintenance Compliance Certification Program.



# **Vortechs Inspection & Maintenance Log**

rtech M	ouel:		LO		η
Date	Water depth to sediment <sup>1</sup>	Floatable Layer Thickness²	Describe Maintenance Performed	Maintenance Personnel	Comments

- 1. The water depth to sediment is determined by taking two measurements with a stadia rod: one measurement from the manhole opening to the top of the sediment pile and the other from the manhole opening to the water surface. If the difference between these measurements is less than eighteen inches the system should be cleaned out. Note: To avoid underestimating the volume of sediment in the chamber, the measuring device must be carefully lowered to the top of the sediment pile.
- 2. For optimum performance, the system should be cleaned out when the floating hydrocarbon layer accumulates to an appreciable thickness. In the event of an oil spill, the system should be cleaned immediately.

#### Attachment "G"

# **Maintenance Plan for Vegetative Filter Strips**

Location:

Phase 1 - West side of the entrance drive

Phase 2 - North side of northern parking isle

Owner:

Christ Our King Anglican Church 111 W. San Antonio St. Suite 250 New Braunfels, Texas 78130 Phone: 830-632-7744

I agree that the attached Vegetative Filter Maintenance and Monitoring Procedures will be implemented to ensure that the proposed BMP functions as designed.

Charles Salsman Christ Our King Anglican Church

<u>6/7/10</u> Date

I have reviewed the attached maintenance and monitoring procedures and to the best of my knowledge certify that if they are followed as outlined the vegetative filter strips will function as designed.

Jeffref D. Mæller, P.F.



# Attachment "G"

## Maintenance Plan for Vortechs Model 16000 & 1421

Vortechs Location:	1 - Southwest corner of Phase 1
	2 - Southeast corner of Phase 2
	3 - Northeast corner of Phase 3
	4 - Southwest corner of Phase 6
	5 - Southeast corner of Phase 6
Owner:	Christ Our King Anglican Church 111 W. San Antonio St. Suite 250 New Braunfels, Texas 78130 Phone: 830-632-7744

I agree that the attached Vortechs Maintenance and Monitoring Procedures will be implemented to ensure that the proposed system functions as designed.

\_\_\_\_ Amin Charles Salsman

Charles Salsman Christ Our King Anglican Church

<u>6/7//0</u> Date

I have reviewed the attached maintenance and monitoring procedures and to the best of my knowledge certify that if they are followed as outlined the Vortechs units will function as designed.

Jeffrey - Woll-



#### SECTION 02721

# STORMWATER TREATMENT SYSTEM

#### PART 1.00 GENERAL

#### 1.1 DESCRIPTION

A. Work included:

The Contractor, and/or a manufacturer selected by the Contractor and approved by the Engineer, shall furnish all labor, materials, equipment and incidentals required and install all precast concrete stormwater treatment systems and appurtenances in accordance with the Drawings and these specifications.

#### 1.2 QUALITY CONTROL INSPECTION

- A. The quality of materials, the process of manufacture, and the finished sections shall be subject to inspection by the Engineer. Such inspection may be made at the place of manufacture, or on the work site after delivery, or at both places, and the sections shall be subject to rejection at any time if material conditions fail to meet any of the specification requirements, even though sample sections may have been accepted as satisfactory at the place of manufacture. Sections rejected after delivery to the site shall be marked for identification and shall be removed from the site at once. All sections which have been damaged beyond repair during delivery will be rejected and, if already installed, shall be repaired to the Engineer's acceptance level, if permitted, or removed and replaced, entirely at the Contractor's expense.
- B. All sections shall be inspected for general appearance, dimensions, soundness, etc. The surface shall be dense, close textured and free of blisters, cracks, roughness and exposure of reinforcement.
- C. Imperfections may be repaired, subject to the acceptance of the Engineer, after demonstration by the manufacturer that strong and permanent repairs result. Repairs shall be carefully inspected before final acceptance. Cement mortar used for repairs shall have a minimum compressive strength of 4,000 psi (28 MPa) at the end of 7 days and 5,000 psi (34 MPa) at the end of 28 days when tested in 3 inch (76 mm) diameter by 6 inch (152 mm) long cylinders stored in the standard manner. Epoxy mortar may be utilized for repairs.

#### 1.3 SUBMITTALS

#### A. Shop Drawings

The Contractor shall be provided with dimensional drawings and, when specified, utilize these drawings as the basis for preparation of shop drawings showing details for construction, reinforcing, joints and any cast-in-place appurtenances. Shop drawings shall be annotated to indicate all materials to be used and all applicable standards for materials, required tests of materials and design assumptions for structural analysis. Shop drawings shall be prepared at a scale of not less than 3/16-inches per foot (1:75). Six (6) hard copies of said shop drawings shall be submitted to the Engineer for review and approval.

#### PART 2.00 PRODUCTS

#### 2.1 MATERIALS AND DESIGN

- A. Concrete for precast stormwater treatment systems shall conform to ASTM C 857 and C 858 and meet the following additional requirements:
  - 1. The wall thickness shall not be less than 6 inches (152 mm) or as shown on the dimensional drawings. In all cases the wall thickness shall be no less than the minimum thickness necessary to sustain HS20-44 (MS18) loading requirements as determined by a Licensed Professional Engineer.
  - 2. Sections shall have tongue and groove or ship-lap joints with a butyl mastic sealant conforming to ASTM C 990.
  - 3. Cement shall be Type II Portland cement conforming to ASTM C 150.
  - 4. All sections shall be cured by an approved method. Sections shall not be shipped until the concrete has attained a compressive strength of 4,000 psi (28 MPa) or until 5 days after fabrication and/or repair, whichever is the longer.
  - Pipe openings shall be sized to accept pipes of the specified size(s) and material(s), and shall be sealed by the Contractor with a hydraulic cement conforming to ASTM C 595M
- B. Internal aluminum plate components shall be aluminum alloy 5052-H32 in accordance with ASTM B 209.
- C. Sealant to be utilized at the base of the swirl chamber shall be 60 durometer extruded nitrile butadiene rubber (Buna N) and shall be provided to the concrete precaster for installation.
- D. Brick or masonry used to build the manhole frame to grade shall conform to ASTM C 32 or ASTM C 139 and shall be installed in conformance with all local requirements.
- E. Casting for manhole frames and covers shall be in accordance with ASTM A48, CL.30B and AASHTO M105. The manhole frame and cover shall be equivalent to Campbell Foundry Pattern #1009A or #1012D custom cast with the CONTECH Stormwater Solutions logo and the words "Vortechs<sup>®</sup> Stormwater Treatment System".
- F. A bitumen sealant in conformance with ASTM C 990 shall be utilized in the sealing of the joint between the swirl chamber and the vault at the long wall tangent points. The butyl material shall be 3/4-inch thick by 3/4-inch wide.
#### 2.2 PERFORMANCE

Each stormwater treatment system shall adhere to the following performance specifications at the design treatment capacities, as listed below:

Table 2.2

Vortechs®	Design	Sediment
Model	Treatment	Storage
	Capacity	(yd <sup>3</sup> )/(m <sup>3</sup> )
	(cfs)/(l/s)	
1000	0 - 1.6 (0 - 45)	0.7 (0.54)
2000	1.6 - 2.8 (45-80)	1.2 (0.91)
3000	2.8 - 4.5 (80-125)	1.8 (1.38)
4000	4.5 - 6.0 (125-175)	2.4 (1.84)
5000	6.0 - 8.5 (175-240)	3.2 (2.45)
7000	8.5 - 11.0 (240-315)	4.0 (3.06)
9000	11.0 - 14.0 (315-400)	4.8 (3.67)
11000	14.0 - 17.5 (400-495)	5.6 (4.28)
16000	17.5 - 25.0 (495-710)	7.1 (5.43)

Each stormwater treatment system shall include a circular aluminum "swirl chamber" (or "grit chamber") with a tangential inlet to induce a swirling flow pattern that will accumulate and store settleable solids in a manner and a location that will prevent re-suspension of previously captured particulates.

Each stormwater treatment system shall be of a hydraulic design that includes flow controls designed and certified by a professional engineer using accepted principles of fluid mechanics that raise the water surface inside the tank to a pre-determined level in order to prevent the reentrainment of trapped floating contaminants.

Each stormwater treatment system shall be capable of removing **80% of the net annual Total Suspended Solids (TSS)** load based on a 50-micron particle size. Annual TSS removal efficiency models shall be based on documented removal efficiency performance from full scale laboratory tests. Annual TSS removal efficiency models shall only be considered valid if they are corroborated by independent third party field testing. Said field testing shall include influent and effluent composite samples from a minimum of ten storms at one location. Individual stormwater treatment systems shall have the Design Treatment Capacity listed in Table 2.2, and shall not resuspend trapped sediments or re-entrain floating contaminants at flow rates up to and including the specified Design Treatment Capacity.

Individual stormwater treatment systems shall have usable sediment storage capacity of not less than the corresponding volume listed in Table 2.2. The systems shall be designed such that the pump-out volume is less than  $\frac{1}{2}$  of the total system volume. The systems shall be designed to not allow surcharge of the upstream piping network during dry weather conditions.

A water-lock feature shall be incorporated into the design of the stormwater treatment system to prevent the introduction of trapped oil and floatable contaminants to the downstream piping during routine maintenance and to ensure that no oil escapes the system during the ensuing rain event. Direct access shall be provided to the sediment and floatable contaminant storage chambers to facilitate maintenance. There shall be no appurtenances or restrictions within these chambers.

Stormwater treatment systems shall be completely housed within one rectangular structure.

## 2.3 MANUFACTURER

Each stormwater treatment system shall be of a type that has been installed and used successfully for a minimum of 5 years. The manufacturer of said system shall have been regularly engaged in the engineering design and production of systems for the physical treatment of stormwater runoff during the aforementioned period.

Each stormwater treatment system shall be a Vortechs<sup>®</sup> System as manufactured by CONTECH Stormwater Solutions Inc., 200 Enterprise Drive, Scarborough, Maine 04074, phone: 207-885-9830, fax: 207-885-9825; and as protected under U.S. Patent #5,759,415.

## PART 3.00 EXECUTION

## 3.1 INSTALLATION

- A. Each Stormwater Treatment System shall be constructed according to the sizes shown on the Drawings and as specified herein. Install at elevations and locations shown on the Drawings or as otherwise directed by the Engineer.
- B. Place the precast base unit on a granular subbase of minimum thickness of six inches (152 mm) after compaction or of greater thickness and compaction if specified elsewhere. The granular subbase shall be checked for level prior to setting and the precast base section of the trap shall be checked for level at all four corners after it is set. If the slope from any corner to any other corner exceeds 0.5% the base section shall be removed and the granular subbase material re-leveled.
- C. Prior to setting subsequent sections place bitumen sealant in conformance with ASTM C 990 along the construction joint in the section that is already in place.
- D. After setting the base and wall or riser sections, prepare to install the swirl chamber. Place the 3/4-inch (19 mm) thick by 3/4-inch (19 mm) wide butyl mastic seal vertically on the outside of the swirl chamber starting one inch above the bottom of the swirl chamber and continuing to a height equal to the elevation of the bottom of the upper aperture of the swirl chamber. The butyl mastic seal should abut the downstream side of the predrilled mounting holes that attach the swirl chamber to the long walls of the concrete vault. Next, install the extruded Buna N seal on the bottom edge of the 180 degree downstream section of the swirl chamber by first applying a bead of Sikaflex-1a polyurethane elastomeric sealant into the extruded slot then slide the seal onto the swirl chamber. The extruded seal should extend 3-inches (76 mm) upstream of the mounting holes, toward the inlet end of the vault. Set the swirl chamber into position and keep the seal approximately 1/2-inch (13 mm) above the floor of the concrete vault. Apply a continuous bead of Sikaflex-1a sealant under the cupped bottom of the seal. Set the circular swirl chamber on the floor of the vault and anchor it by bolting the swirl chamber to the side walls of the concrete vault at the three (3) tangent points and at the inlet tab using HILTI brand stainless steel drop-in wedge anchors or equivalent 3/8-inch (10 mm) diameter by 2-3/4 inch (70 mm) minimum length at heights of approximately three inches (3") (76 mm) off the floor and at fifteen inch (15") (381 mm) intervals to approximately the same height of the butyl mastic sealant (at locations of pre-drilled holes in aluminum components). Apply a continuous bead of Sikaflex-1a sealant to the intersection of the inside bottom edge of the extruded seal and the vault floor.
- E. If the oil baffle wall (Baffle A) and flow control wall (Baffle B) are not integrally cast-in to riser/wall sections then the Baffle wall panels shall be placed in the formed keyways or between

bolted-in-place angle flanges as provided by the manufacturer. Apply non-shrink grout or Sikaflex-1a sealant to each end of Baffle A and Baffle B at the upstream intersection with the side walls of the concrete vault.

- F. Prior to setting the precast roof section, bitumen sealant equal to ASTM C 990 shall be placed along the top of the oil baffle wall (Baffle A), using more than one layer of mastic if necessary, to a thickness at least 1-inch (25 mm) greater than the nominal gap between the top of the baffle and the roof section. The nominal gap shall be determined either by field measurement or the shop drawings. Do not seal the top of Baffle B unless specified on the shop drawings to do so. After placement of the roof section has compressed the butyl mastic sealant in the gap over Baffle A, finish sealing the gap with an approved non-shrink grout on both sides of the gap using the butyl mastic as a backing material to which to apply the grout. If roof section is "clamshell" or "bathtub" halves, then finish sealing the ends of the Baffle walls by applying non-shrink grout or Sikaflex-1a sealant to each end of Baffle B at the downstream intersection with the side walls of the concrete vault.
- G. After setting the precast roof section of the stormwater treatment system, set precast concrete manhole riser sections, to the height required to bring the cast iron manhole covers to grade, so that the sections are vertical and in true alignment with a ¼-inch (6 mm) maximum tolerance allowed. Backfill in a careful manner, bringing the fill up in 6-inch (152 mm) lifts on all sides. If leaks appear, clean the inside joints and caulk with lead wool to the satisfaction of the Engineer. Precast sections shall be set in a manner that will result in a watertight joint. In all instances, installation of Stormwater Treatment Systems shall conform to ASTM specification C 891 "Standard Practice for Installation of Underground Precast Utility Structures".
- H. Holes made in the concrete sections for handling or other purposes shall be plugged with a nonshrink grout or by using grout in combination with concrete plugs.
- I. Where holes must be cut in the precast sections to accommodate pipes, do all cutting before setting the sections in place to prevent any subsequent jarring which may loosen the mortar joints. The Contractor shall make all pipe connections.

# Texas Commission on Environmental Quality

TSS Removal	Calculations	04-20-2009	
-------------	--------------	------------	--

Project Name: Christ Our King Anglican Church Date Prepared: 6/6/2010

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell.

Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348.

# Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for	or the total project:	Calculations f	om RG-348	Pages 3-27 to 3-30			
Page 3-29 Equation 3.3: L <sub>M</sub> = 27.2(A <sub>N</sub> x P)							
where:	$L_{M}$ total project = $A_{N} = P$	Required TSS Net increase i Average annu	removal resulting fro n impervious area for al precipitation, inche	m the proposed development = 80% of increased load the project s			
Site Data: Determine Required Predevelopment imp Total post-development im Total post	I Load Removal Based on the Entire Projec County = Total project area included in plan * = pervious area within the limits of the plan* = l-development impervious cover fraction * = P =	Comal 22.10 0.42 9.30 0.42 33	acres acres acres inches				
	LM TOTAL PROJECT =	7971	lbs.				
* The values entered in these field	is should be for the total project area.						
Number of drainage ba	asins / outfalls areas leaving the plan area =	5					
2. Drainage Basin Parameters (Th	is information should be provided for eac	ch basin):					
	Drainage Basin/Outfall Area No. =	: 1					
	Total drainage basin/outfall area =	2.42	acres				
Predevelopment impervio	ous area within drainage basin/outfall area =	0.00	acres				
Post-development impervio	ous area within drainage basin/outfall area =	1.75	acres				
Post-development impervious	fraction within drainage basin/outfall area =	0.72					
	LM THIS BASIN =	= 1571	lbs.				

3. Indicate the proposed BMP Code for this basin.



Off-site area Off-site Impervious cover Impervious fractio Off-site R	draining to BMP = draining to BMP = n of off-site area = unoff Coefficient =	0.00 0.00 0 0.00	acres acres		
Off-site Water	r Quality Volume =	#DIV/0!	cubic feet		
Stora	ige for Sediment =	#DIV/0!			
Total Capture Volume (required water quality vo	olume(s) x 1.20) =	#DIV/0!	cubic feet		
The values for BMP Types not selected in cell C45 will sho	water quality volur	ne(s) for the	selected BMP		
7. Retention/Irrigation System	(	Designed as F	Required in RG	-348	Pages 3-42 to 3-46
Required Water Quality Volume for	r retention basin =	NA	cubic feet		
Irrigation Area Calculations:					
Soil infiltration/p	ermeability rate = Irrigation area =	0.1 NA NA	in/hr square feet acres	Enter determined per	rmeability rate or assumed value of 0.1
8. Extended Detention Basin System	I	Designed as F	Required in RG	à-348	Pages 3-46 to 3-51
Required Water Quality Volume for extended	d detention basin =	NA	cubic feet		
9. Filter area for Sand Filters	1	Designed as F	Required in RG	à-348	Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration Syst	em				
Water Quality Volume for sed	limentation basin =	NA	cubic feet		
Minimum	n filter basin area =	NA	square feet		
Maximum sedimen Minimum sedimen	tation basin area = tation basin area =	NA NA	square feet square feet	For minimum water of For maximum water	depth of 2 feet depth of 8 feet
9B. Partial Sedimentation and Filtration S	ystem				
Water Quality Volume for	combined basins =	NA	cubic feet		
Minimun	n filter basin area =	NA	square feet		
Maximum sedimen Minimum sedimen	tation basin area = tation basin area =	NA NA	square feet square feet	For minimum water For maximum water	depth of 2 feet depth of 8 feet

10. Joretention System	Design	ed as Required in R	G-348 Pages 3-63 to 3-65
Required Water Quality Volume for Bioretention Basin	= N	A cubic feet	
11. Wet Basins	Design	ed as Required in R	G-348 Pages 3-66 to 3-71
	e coigin		
Required capacity of Permanent Pool Required capacity at WQV Elevation	= N = N	A cubic feet A cubic feet	Permanent Pool Capacity is 1.20 times the WQV Total Capacity should be the Permanent Pool Capacity plus a second WQV.
12. Constructed Wetlands	Design	ed as Required in R	G-348 Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands	i = N	A cubic feet	
<u>13. AquaLogic<sup>™</sup> Cartridge System</u>	Design	ed as Required in R	G-348 Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the require	ed 20% in	crease with mainte	nance contract with AquaLogic <sup>™</sup> .
Required Sedimentation chamber capacity	/= N	A cubic feet	
Filter canisters (FCs) to treat WQV	/= N	A cartridges	
Filter basin area (RIA <sub>F</sub>	) = N	A square feet	t
14. Stormwater Management StormFilter® by CONTECH			
Required Water Quality Volume for Contech StormFilter System	n = 1	A cubic feet	
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPs / LOAD REM	OVALS AF	E BASED UPON F	LOW RATES - NOT CALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Design	ed as Required in R	AG-348 Pages 3-51 to 3-54
Design parameters for the swale:			
Drainage Area to be Treated by the Swale = A	\ =	8.00 acres	
Impervious Cover in Drainage Area	a =	4.00 acres	
Rainfall intensity =	i =	1.1 in/hr	
Swale Slope	9 =	0.01 ft/ft	
Side Slope (z Design Water Denth - v	) =	3 033.ft	
Weighted Runoff Coefficient = 0	) =	0.54	
A <sub>CS</sub> = cross-sectional area of flow in Swale	9 =	13.17 sf	

The same of the

P <sub>w</sub> = Wetted Perimeter =	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = 1.49 A_{CS} R_{H}^{2/3} S^{0.5}$$
  
n  
 $b = \frac{0.134 \times Q}{y^{1.67} S^{0.5}} - zy = 38.51$  feet  
 $Q = CiA = 4.71$  cfs

To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) = Q/A<sub>CS</sub> = 0.36 ft/sec

To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

15B.	Alternative Method using Excel Solver				To solve for bottom v Excel can simultanec The required "Swale
	Design Q = CiA =	4.71 cfs			
					First, highlight Cell F
	Manning's Equation Q =	0.76 cfs	Error 1 =	3.95	Then click on "Tools"
	Swale Width=	6.00 ft			The value in the "Set
					The value in the "By (
					Click on solve.
	Instructions are provided to the right (green comments).				
					The resulting "Swale
					If the resulting "Swal
	Flow Velocity	0.36 ft/s			-
	Minimum Length =	107.24 ft			if there is not the opti
					Click on "Tools" and
	Instructions are provided to the right (blue comments).				Then proceed as inst
	Design Width =	6 ft			If you would like to in
	Desion Discharge =	0.76 cfs	Error 2 =	3.95	Excel can simultaneo
	Design Denth =	0.33 ft			The required "Design
	Doorgin Dopin -	II			

<b>-</b>					
Flow Velocity = Minimum Length =	ſ	0.3.2 cts 97.48 ft			First set the desired I Highlight Cell F232.
If any of the resulting values do not meet the design requirement set forth in	n RG-348,	, the design para	meters may be modi	fied and the solver rerun.	Click on "Tools" and
If any of the resulting values still do not meet the design requirement set for	rtn in HG-	-348, widening tr	ie swale bottom valu	e may not be possible.	The value in the "Set
16. Vegetated Filter Strips	Pages 3-55 to 3-57	The value in the "By Click on solve.			
There are no calculations required for determining the load or size of vegeta The 80% removal is provided when the contributing drainage area does not the sheet flow leaving the impervious cover is directed across 15 feet of en- across 50 feet of natural vegetation with a maximum slope of 10%. There can	ative filter exceed 7 gineered an be a b	r strips. '2 feet (direction filter strips with reak in grade as	of flow) and maximum slope of 2 long as no slope exc	0% or eeds 20%.	The resulting "Design If the resulting "Design First set the desired I Highlight Cell 5232
If vegetative filter strips are proposed for an interim permanent BMP, they n	nay be sia	zed as described	on Page 3-56 of RG	348.	Click on "Tools" and The value in the "Set
17. Wet Vaults	Designed	as Required in R	G-348	Pages 3-30 to 3-32 & 3-79	The value in the "By Click on solve.
Required Load Removal Based upon Equation 3.3 =	NA	lbs			The resulting "Design If the resulting "Design
First calculate the load removal at 1.1 in/hour					0
RG-348 Page 3-30 Equation 3.4: Q = CiA					
C = runoff coefficient for the drainage area = i = design rainfall intensity = A = drainage area in acres =		0.55 1.1 in/hour 1 acres	C = Runoff Coeffic	ent = 0.546 (IC) <sup>2</sup> + 0.328 (IC) + 0.03	
Q = flow rate in cubic feet per second =		0.61 cubic feet/s	ec		
RG-348 Page 3-31 Equation 3.5: V <sub>OR</sub> = Q/A					
Q = Runoff rate calculated above = A = Water surface area in the wet vault =		0.61 cubic feet/s 150 square feet	ec		
V <sub>OR</sub> = Overflow Rate =		0.00 feet/sec			
Percent TSS Removal from Figure 3-1 (RG-348 Page 3-31) =		53 percent			
Load removed by Wet Vault =	#VALL	JE! Ibs			
If a bypass occurs at a rainfall intensity of less than 1.1 in/hours Calculate the efficiency reduction for the actual rainfall intensity rate					
Actual Rainfall Intensity at which Wet Vault bypass Occurs =		0.5 in/hour			
Fraction of rainfall treated from Figure 3-2 RG-348 Page 3-32 $\approx$ Efficiency Reduction for Actual Rainfall Intensity $\approx$		0.75 percent 0.83 percent			

Service and service and service

NAMES OF TAXABLE PARTY OF TAXABLE PARTY.

Resultant TSS Load removed by Wet Vault	#VALUE!	lbs		
18. Permeable Concrete	Designed as F	lequired in RG	i-348	Pages 3-79 to 3-83
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING Z	ONE			
19. BMPs Installed in a Series	Designed as F	lequired in RG	à-348	Pages 3-32
Michael E. Barrett, Ph.D., P.E. recommended that the coeffi	icient for E <sub>2</sub> be	changed from	m 0.5 to 0.65 on May	3, 2006
$E_{TOT} = \{1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))\} \times 100 =$	= 86.38	l percent	NET EFFICIENCY O	F THE BMPs IN THE SERIES
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1$ =	= 75.00	) percent		
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	=	) percent		
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3 =$	≈ 0.00	) percent		
THEREFORE, THE NET LOAD REMOVAL WOULD BE: $(A_1 AND A_2 VALUES ARE FROM SECTION 3 ABOVE)$				
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>1</sub> X 34.6 X A <sub>P</sub> X0.54) =	= 1736.2	l ibs		
20. Stormceptor				
Required TSS Removal in BMP Drainage Area	= NA	lbs		
Impervious Cover Overtreatments	= 0.0000	ac		
BMP Sizing	= 0.00	IDS		
Effective Area :	= NA	EA		
Calculated Model Size(s) :	= #N/A			
Actual Model Size (if multiple values provided in Calculated	đ			
Model Size or if you are choosing a larger model size) =	= 0	Model Size		
Surface Area	= #N/A	ft <sup>2</sup>		
Overflow Rate :	= #VALUE!	Vor		
Rounded Overflow Rate :	= #VALUE!	Vor		
BMP Efficiency %	= #VALUE!	%		
L <sub>B</sub> Value :	= #VALUE!	lbs		
TSS Load Credit	= #VALUEI	lbs		
Is Sufficient Treatment Available? (TSS Credit $\geq$ TSS Uncapt.	) #VALUE!			
TSS Treatment by BMP (LM + TSS Uncapt.)	= #VALUEI			

## 21. Vortech

	Required TSS Removal in BMP Drainage Area=	1570.80	lbs
	Impervious Cover Overtreatment=	0.0000	ac
	TSS Removal for Uncaptured Area =	0.00	lbs
BMP Sizing			
	Effective Area =	1.60	EA
	Calculated Model Size(s) =	Vx16000	
Act	tual Model Size (if choosing larger model size) =	Vx16000	Pick Model Size
	Surface Area =	113.10	ft <sup>2</sup>
	Overflow Rate =	0.015514	V <sub>or</sub>
	Rounded Overflow Rate =	0.015600	V <sub>or</sub>
	BMP Efficiency % =	80.00	%
	L <sub>R</sub> Value =	1608.07	lbs
			120
	TSS Load Credit =	37.27	lbs
Is Sufficient Tr	eatment Available? (TSS Credit > TSS Uncapt.)	Yes	
	/ /		
	TSS Treatment by BMP (LM + TSS Uncapt.) =	1570.80	
	, , , , , , , , , , , , , , , , , , , ,		

# Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

Project Name: Christ Our King Anglican Church Date Prepared: 6/6/2010

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell.

Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348.

Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations	from RG-348	Pages 3-27 to 3-30					
Page 3-29 Equation 3.3: L <sub>M</sub> = 27.2(A <sub>N</sub> x P)								
where: L <sub>M TOTAL PRO</sub>	JECT = Required TS	S removal resulting fr	om the proposed development = 80% of increased load					
	A <sub>N</sub> = Net increase	in impervious area fo	r the project					
	P = Average ann	ual precipitation, inch	es					
Site Data: Determine Required Load Removal Based on the Entire F	Project							
Co	unty = Comal							
Total project area included in pla	an * = 22.11	acres						
Predevelopment impervious area within the limits of the pl	an * =0.42	acres						
Total post-development impervious area within the limits of the p	lan* = 9.30	acres						
Total post-development impervious cover fracti	on * = 0.42							
	P = <u>33</u>	linches						
	JECT = <b>7971</b>	lbs.						
* The values entered in these fields should be for the total project are	ea.							
Number of drainage basins / outfalls areas leaving the plan	area = 5							
2. Drainage Basin Parameters (This information should be provided for	or each basin):							
Drainage Basin/Outfall Area	No. = 2							
Total drainage basin/outfall	area = 4.14	acres						
Predevelopment impervious area within drainage basin/outfall	area = 0.00	acres						
Post-development impervious area within drainage basin/outfall a	area = 2.88	acres						
Post-development impervious fraction within drainage basin/outfall a	area = 0.70							
	BASIN = 2585	lbs.						
3. Indicate the proposed BMP Code for this basin.								

Proposed BMP	= Vortechs	a const		
Removal efficiency	= 0	BMP Type.	Aq Bid Co Co Ex Gr Re Sa Sta Ve Vo W	aualogic Cartridge Filter portention pontech StormFilter postructed Wetland trended Detention rassy Swale etention / Irrigation and Filter ormceptor egetated Filter Strips prtechs et Basin et Vault
RG-348 Page 3-33 Equation 3.7: L <sub>R</sub>	= (BMP efficier	ncy) x P x (A <sub>l</sub> x	34.6 + A <sub>P</sub> x 0.54)	
where: A <sub>C</sub>	= Total On-Site	e drainage area	a in the BMP catchment ar	ea
A <sub>1</sub>	= Impervious a	rea proposed	the BMP catchment area	a
	= TSS Load re	moved from th	is catchment area by the r	proposed BMP
-4	- 100 2000 10		is outerment area by the p	
Ac	= 4.14	acres		
A	= 2.88	acres		
Ap	= 1.26	acres		
L <sub>R</sub>	.= 0	lbs		
5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfal	ii area			
Desired L <sub>M THIS BASIN</sub>	i = 3482	lbs.		
F	= #DIV/0!			
6. Calculate Capture Volume required by the BMP Type for this drainage I	basin / outfall	area.	Calculations from RG-34	Pages 3-34 to 3-36
Rainfall Depth Post Development Runoff Coefficient On-site Water Quality Volume	a = #DIV/0! = 0.50 e = #DIV/0!	inches cubic feet		

Calculations from RG-348 Pages 3-36 to 3-37

Off-site area draining to BMP = Off-site Impervious cover draining to BMP = Impervious fraction of off-site area = Off-site Runoff Coefficient = Off-site Water Quality Volume =	= 0.00 = 0.00 = 0.00 = 0.00 = #DIV/0!	acres acres cubic feet	
Storage for Sediment = Total Capture Volume (required water quality volume(s) x 1.20) = The following sections are used to calculate the required water quality volu The values for BMP Types not selected in cell C45 will show NA. <u>7. Retention/Irrigation System</u>	#DIV/0! #DIV/0! ume(s) for the Designed as	cubic feet • selected BMP. Required in RG-348	Pages 3-42 to 3-46
Required Water Quality Volume for retention basin =	- NA	cubic feet	
Irrigation Area Calculations:			
Soil infiltration/permeability rate = Irrigation area =	= 0.1 = NA NA	in/hr Ente square feet acres	er determined permeability rate or assumed value of 0.1
8. Extended Detention Basin System	Designed as	Required in RG-348	Pages 3-46 to 3-51
Required Water Quality Volume for extended detention basin =	= NA	cubic feet	
9. Filter area for Sand Filters	Designed as	Required in RG-348	Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration System			
Water Quality Volume for sedimentation basin =	= NA	cubic feet	
Minimum filter basin area =	= NA	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	= NA = NA	square feet For i square feet For i	minimum water depth of 2 feet maximum water depth of 8 feet
9B. Partial Sedimentation and Filtration System			
Water Quality Volume for combined basins	= <b>NA</b>	cubic feet	
Minimum filter basin area	= <b>NA</b>	square feet	
Maximum sedimentation basin area = Minimum sedimentation basin area =	= NA = NA	square feet For square feet For	minimum water depth of 2 feet maximum water depth of 8 feet

10. Bioretention System	Designed	as Required in R	G-348	Pages 3-63 to 3-6ട
Required Water Quality Volume for Bioretention Basin =	= NA	cubic feet		
11. Wet Basins	Designed	as Required in R	G-348	Pages 3-66 to 3-71
Required capacity of Permanent Pool = Required capacity at WQV Elevation =	NA NA	cubic feet cubic feet	Permaner Total Cap plus a sec	It Pool Capacity is 1.20 times the WQV acity should be the Permanent Pool Capacity cond WQV.
12. Constructed Wetlands	Designed	as Required in R	G-348	Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands	= NA	cubic feet		
13. AquaLogic <sup>TM</sup> Cartridge System	Designed	as Required in R	IG-348	Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the required	d 20% incre	ease with mainte	enance cont	ract with AquaLogic <sup>™</sup> .
Required Sedimentation chamber capacity Filter canisters (FCs) to treat WQV Filter basin area (RIA <sub>F</sub> )	= NA = NA = NA	cubic feet cartridges square feel	t	
14. Stormwater Management StormFilter® by CONTECH				
Required Water Quality Volume for Contech StormFilter System	= NA	cubic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPs / LOAD REMO	VALS ARE	BASED UPON F	LOW RATE	S - NOT CALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designed	as Required in F	G-348	Pages 3-51 to 3-54
Design parameters for the swale:				
Drainage Area to be Treated by the Swale = A Impervious Cover in Drainage Area Rainfall intensity = i Swale Slope Side Slope (z) Design Water Depth = y Weighted Runoff Coefficient = C		8.00 acres 4.00 acres 1.1 in/hr 0.01 ft/ft 3 0.33 ft 0.54		
A <sub>CS</sub> = cross-sectional area of flow in Swale	=	13.17 sł		

P <sub>w</sub> = Wetted Perimeter =	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

#### 15A, Using the Method Described in the RG-348

Manning's Equation: 
$$Q = 1.49 A_{CS} R_{H}^{2/3} S^{0.5}$$
  
n  
 $b = 0.134 \times Q$  -  $zy = 38.51$  feet  
 $y^{1.67} S^{0.5}$   
 $Q = CiA = 4.71$  cfs

To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) =  $Q/A_{CS}$  = 0.36 ft/sec

To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

feet

15B. Alternative Method using Excel Solver				To solve for bottom v Excel can simultanec The required "Swale
Design Q = CiA =	4.71 cfs			
				First, highlight Cell F
Manning's Equation Q =	0.76 cfs	Error 1 =	3.95	Then click on "Tools"
Swale Width=	6.00 tt			The value in the "Set
				The value in the "By "
				Click on solve.
Instructions are provided to the right (green comments).				
				The resulting "Swale
				If the resulting "Swal
Flow Velocity	0.36 ft/s			
Minimum Length =	107.24 ft			if there is not the opti
				Click on "Tools" and
Instructions are provided to the right (blue comments).				Then proceed as inst
Dening Midth	C 14			If you would like to in
Design Width =		Error 2 -	2.05	Evcel can simultanec
Design Discharge =	0.76 CIS	Ellor 2 =	0.90	The required "Design
Design Depth =	0.33 n			me required pesign

Flow Velocity =	Ē	0.32 cfs			
Minimum Length =	9	97.48 ft			First set the desired I Highlight Cell F232.
If any of the resulting values do not meet the design requirement set forth in	1 RG-348,	the design para	ameters may be modifi-	ed and the solver rerun.	
If any of the resulting values still do not meet the design requirement set for	th in RG-	348, widening ti	he swale bottom value	may not be possible.	Click on "Tools" and The value in the "Set
16 Vegetated Filter Strips	Designed	as Required in F	G-348	Pages 3-55 to 3-57	The value in the "By
To. vegetated i nier otripo	Designed	as negatica in r			Click on solve.
There are no calculations required for determining the load or size of vegeta The 80% removal is provided when the contributing drainage area does not the sheet flow leaving the impervious cover is directed across 15 feet of eng across 50 feet of natural vegetation with a maximum slope of 10%. There can	% or <del>e</del> ds 20%.	The resulting "Design If the resulting "Desig First set the desired I Highlight Cell F232.			
If vegetative filter strips are proposed for an interim permanent BMP, they n	nay be siz	ed as described	d on Page 3-56 of RG-3	48.	Click on "Tools" and
					The value in the "By t
17. Wet Vaults	Designed	as Required in F	3G-348	Pages 3-30 to 3-32 & 3-79	Click on solve.
Required Load Removal Based upon Equation 3.3 =	NA	lbs			The resulting "Design If the resulting "Design
First calculate the load removal at 1.1 in/hour					
RG-348 Page 3-30 Equation 3.4: Q = CiA					
C = runoff coefficient for the drainage area = i = design rainfall intensity = A = drainage area in acres =		0.52 1.1 in/hour 1 acres	C = Runoff Coefficie	nt = 0.546 (IC) <sup>2</sup> + 0.328 (IC) + 0.03	
Q = flow rate in cubic feet per second =		0.57 cubic feet/	sec		
RG-348 Page 3-31 Equation 3.5: V <sub>OR</sub> = Q/A					
Q = Runoff rate calculated above = A = Water surface area in the wet vault =		0.57 cubic feet/ 150 square fee	sec it		
V <sub>OR</sub> = Overflow Rate =		0.00 feet/sec			
Percent TSS Removal from Figure 3-1 (RG-348 Page 3-31) =		53 percent			
Load removed by Wet Vault =	#VALU	JE! Ibs			
If a bypass occurs at a rainfall intensity of less than 1.1 in/hours Calculate the efficiency reduction for the actual rainfall intensity rate					
Actual Rainfall Intensity at which Wet Vault bypass Occurs =		0.5 in/hour			
Fraction of rainfall treated from Figure 3-2 RG-348 Page 3-32 = Efficiency Reduction for Actual Rainfall Intensity =		0.75 percent 0.83 percent			

Resultant TSS Load removed by Wet Vault = #VALUE! Ibs

and the second second

18. Permeable Concrete	Designed as Required in RG-348 Pages 3-79 to			
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING ZO	DNE			
19. BMPs Installed in a Series	Designed as F	Required in RG	à-348 Pages 3-32	
Michael E. Barrett, Ph.D P.E. recommended that the coeffic	cient for E <sub>2</sub> be	changed from	m 0.5 to 0.65 on May 3, 2006	
E <sub>TOT</sub> = [1 - ((1 - E <sub>1</sub> ) X (1 - 0.65E <sub>2</sub> ) x (1 - 0.25E <sub>3</sub> ))] X 100 =	86.3	3 percent	NET EFFICIENCY OF THE BMPs IN THE SERIES	
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1$ =	75.0	) percent		
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	70.0	) percent		
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3$ =	0.0	0 percent		
THEREFORE, THE NET LOAD REMOVAL WOULD BE: (A, AND A, VALUES ARE FROM SECTION 3 ABOVE)				
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>1</sub> X 34.6 X A <sub>P</sub> X0.54) =	2859.7	4 lbs		
20. Stormceptor				
Required TSS Removal in BMP Drainage Area=	NA	lbs		
Impervious Cover Overtreatment=	0.0000	ac		
TSS Removal for Uncaptured Area =	0.00	lbs		
BMP Sizing				
Effective Area =	NA	EA		
Calculated Model Size(s) =	#N/A			
Actual Model Size (if multiple values provided in Calculated Model Size or if you are choosing a larger model size) -	0	Model Size		
woder size of it you are choosing a larger moder size) -	U			
Surface Area =	#N/A	ft <sup>2</sup>		
Overflow Rate =	#VALUE!	Vor		
Rounded Overflow Rate =	#VALUE!	V <sub>or</sub>		
BMP Efficiency % =	#VALUE!	%		
L <sub>R</sub> Value =	#VALUE!	lbs		
TSS Load Credit =	#VALUE!	lbs		
Is Sufficient Treatment Available? (TSS Credit > TSS Uncapt.)	#VALUE!			
TSS Treatment by BMP (LM + TSS Uncapt.) =	#VALUE!			

## 21. Vortech

BMP Sizing	Required TSS Removal in BMP Drainage Area= Impervious Cover Overtreatment= TSS Removal for Uncaptured Area =	2585.09 0.00 0.00	lbs ac Ibs
U U	Effective Area =	2.63	EA
	Calculated Woder Size(s) = A	irea 100 Larg	je
Ac	ctual Model Size (if choosing larger model size) =	Vx1421	Pick Model Size
	Surface Area =	153.90	ft <sup>2</sup>
	Overflow Rate =	0.018796	Vor
	Rounded Overflow Rate =	0.018900	Vor
	BMP Efficiency % =	75.00	%
	L <sub>R</sub> Value =	2483.13	lbs
	TSS Load Credit =	-101.96	lbs
Is Sufficient T	reatment Available? (TSS Credit $\geq$ TSS Uncapt.)	No	
	TSS Treatment by BMP (LM + TSS Uncapt.) =	NA	

# Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

		Date Prepared:	6/6/2010
Additional information is provided for cells with a red triangle in Text shown in blue indicate location of instructions in the Technical G Characters shown in red are data entry fields. Characters shown in black (Bold) are calculated fields. Changes	the upper right corner. auidance Manual - RG-34 s to these fields will ren	Place the curso 8. nove the equation	r over the cell. ns used in the spreadsheet.
1. The Required Load Reduction for the total project:	alculations from RG-348	P	ages 3-27 to 3-30
Page 3-29 Equation 3.3: $L_M = 2$	7.2(A <sub>N</sub> x P)		
where: $L_{M \text{ TOTAL PROJECT}} = F$ $A_N = N$ P = A	Required TSS removal resultin let increase in impervious are verage annual precipitation, i	g from the proposed o a for the project nches	development = 80% of increased load
Site Data: Determine Required Load Removal Based on the Entire Project County = Total project area included in plan * = Predevelopment impervious area within the limits of the plan * = Total post-development impervious area within the limits of the plan * = Total post-development impervious cover fraction * = P =	Cornal           22.11         acres           0.42         acres           9.30         acres           0.42         acres           33         inches		
* The values entered in these fields should be for the total project area.	<b>7971</b> lbs.		
Number of drainage basins / outfalls areas leaving the plan area =	5		
2. Drainage Basin Parameters (This information should be provided for each	basin):		
Drainage Basin/Outfall Area No. =	3		
Total drainage basin/outfall area = Predevelopment impervious area within drainage basin/outfall area = Post-development impervious area within drainage basin/outfall area = Post-development impervious fraction within drainage basin/outfall area = L <sub>M THIS BASIN</sub> =	2.78 acres 0.00 acres 1.42 acres 0.51 1275 lbs.		

Project Name: Christ Our King Anglican Church

3. Indicate the proposed BMP Code for this basin.

Proposed BMP =	Vortechs	
Removal efficiency =	0	percent

Aqualogic Cartridge Filter Bioretention Contech StormEdier Constructed Wetland Extended Detention Grassy Swale Retention / Irrigation Sand Filter Stormceptor Vegetated Filter Strips Vortechs Wet Basin Wet Vault

#### 4. Calculate Maximum TSS Load Removed (L<sub>B</sub>) for this Drainage Basin by the selected BMP Type.

RG-348 Page 3-33 Equation 3.7:  $L_R = (BMP \text{ efficiency}) \times P \times (A_1 \times 34.6 + A_P \times 0.54)$ 

where:

$A_{C} = To$	A <sub>c</sub> = Total On-Site drainage area in the BMP catchment area						
$A_1 = 1m$	A <sub>1</sub> = Impervious area proposed in the BMP catchment area						
$A_P \simeq P \in$	ervious are	a remaining in the BMP catchment area					
$L_R = TS$	L <sub>R</sub> = TSS Load removed from this catchment area by the proposed BMP						
$A_{C} =$	4.14	acres					
$A_i =$	2.88	acres					
$A_P =$	1.26	acres					

 $L_R = 0$  lbs

#### 5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall area

Desired L <sub>M THIS BASIN</sub> =	3482	lbs.		
F =	#DIV/0			
6. Calculate Capture Volume required by the BMP Type for this drainage basin / outfall area.			Calculations from RG-348	Pages 3-34 to 3-36
Rainfall Depth =	#DIV/0	inches		
On-site Water Quality Volume =	#DIV/0	cubic feet		

Calculations from RG-348 Pages 3-36 to 3-37

Off-site area draining to BMP Off-site Impervious cover draining to BMP	= 0.00 = 0.00	acres acres	
Impervious fraction of off-site area Off-site Runoff Coefficient	= 0 = 0.00		
Off-site Water Quality Volume	= #DIV/0!	cubic feet	
Storage for Sediment	= #DIV/0!		
Total Capture Volume (required water quality volume(s) x 1.20)	= #DIV/0!	cubic feet	_
The following sections are used to calculate the required water quality vo	lume(s) for the	selected BMF	2.
7. Retention/Irrigation System	Designed as	Required in RC	G-348 Pages 3-42 to 3-46
an ann			
Required Water Quality Volume for retention basin	= NA	cubic feet	
Irrigation Area Calculations:			
Soil infiltration/permeability rate	= 0.1	in/hr	Enter determined permeability rate or assumed value of 0.1
Irrigation area	= NA	square feet	
	NA	acres	
8. Extended Detention Basin System	Designed as	Required in RC	G-348 Pages 3-46 to 3-51
Required Water Quality Volume for extended detention basin	= NA	cubic feet	
······································			
9. Filter area for Sand Filters	Designed as	Required in RC	3-348 Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration System			
Water Quality Volume for sedimentation basin	= NA	cubic feet	
Minimum filter basin area	= NA	square feet	
Maximum sedimentation basin area	= NA	square feet	For minimum water depth of 2 feet
Minimum sedimentation basin area	= NA	square feet	For maximum water depth of 8 feet
OB Rocticl Codimentation and Elitentics Custom			
95. Partial Sequinentation and Fintration System			
Water Quality Volume for combined basins	= NA	cubic feet	
Minimum filter basin area	= NA	square feet	
Maximum sedimentation basin area Minimum sedimentation basin area	= NA = NA	square feet	For minimum water depth of 2 feet For maximum water depth of 8 feet

10. Elevetention System	Designed	Designed as Required in RG-348		Pages 3-63 to 3-65
Required Water Quality Volume for Bioretention Basin =	NA	cubic feet		
11. Wet Basins	Designed	as Required in R	G-348	Pages 3-66 to 3-71
Required capacity of Permanent Pool = Required capacity at WQV Elevation =	NA NA	cubic feet cubic feet	Permanent Total Capa plus a seco	Pool Capacity is 1.20 times the WQV city should be the Permanent Pool Capacity and WQV.
12. Constructed Wetlands	Designed	as Required in R	G-348	Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands =	= NA	cubic feet		
13. AquaLogic <sup>TM</sup> Cartridge System	Designed	as Required in R	G-348	Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the required	1 20% incre	ase with mainte	nance contra	act with AquaLogic <sup>™</sup> .
Required Sedimentation chamber capacity = Filter canisters (FCs) to treat WQV = Filter basin area (RIA=) =	= NA = NA = NA	cubic feet cartridges square feet		
14. Stormwater Management StormFilter® by CONTECH				
Required Water Quality Volume for Contech StormFilter System =	= NA	cubic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPs / LOAD REMO	VALS ARE	BASED UPON F	LOW RATES	- NOT CALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designed	as Required in R	G-348	Pages 3-51 to 3-54
Design parameters for the swale:				
Drainage Area to be Treated by the Swale = A = Impervious Cover in Drainage Area = Rainfall intensity = i = Swale Slope = Side Slope (z) =	E E E E	8.00 acres 4.00 acres 1.1 in/hr 0.01 ft/ft		
Design Water Depth = y = Weighted Runoff Coefficient = C =		0.33 ft 0.54		
$A_{CS}$ = cross-sectional area of flow in Swale =	= '	13.17 sf		

$P_w =$ Wetted Perimeter =	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

#### 15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = 1.49 A_{CS} R_{H}^{2/3} S^{0.5}$$
  
n

$$b = \frac{0.134 \times Q}{y^{1.67}} - zy = 38.51$$
 feet  
 $y = CiA = 4.71$  cfs

To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) =  $Q/A_{CS}$  = 0.36 ft/sec

#### To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

15B. Alternative Method using Excel Solver			To solve for bottom v Excel can simultaneo The required "Swale
Design Q = CiA =	4.71 cfs		
Manning's Equation Q = Swale Width=	0.76 cfs 6.00 ft	Error 1 = 3.9	First, highlight Cell F Then click on "Tools' The value in the "Set The value in the "By C Click on solve.
instructions are provided to the right (green comments).			The resulting "Swale
	0.00.4/-		If the resulting "Swal
Minimum Length =	0.36 ft/s 107.24 ft		If there is not the opti Click on "Tools" and Then proc <del>eed</del> as inst
Design Width = Design Discharge = Design Depth =	6 ft 0.76 cfs 0.33 ft	Error 2 = 3.9	If you would like to in Excel can simultaneo The required "Design

Flow Veloc: = Minimum Leng: /=	0 cfs 973 tt	First set the desired I Highlight Cell F232.
If any of the resulting values do not meet the design requirement set forth in If any of the resulting values still do not meet the design requirement set for	RG-348, the design parameters may be modified and the solver rerun. th in RG-348, widening the swale bottom value may not be possible.	Click on "Tools" and
16. Vegetated Filter Strips	Designed as Required in RG-348 Pages 3-55 to 3-57	The value in the "By" Click on solve.
There are no calculations required for determining the load or size of vegeta The 80% removal is provided when the contributing drainage area does not the sheet flow leaving the impervious cover is directed across 15 feet of eng across 50 feet of natural vegetation with a maximum slope of 10%. There can	tive filter strips. exceed 72 feet (direction of flow) and jineered filter strips with maximum slope of 20% or in be a break in grade as long as no slope exceeds 20%.	The resulting "Desig If the resulting "Desig First set the desired I Highlight Cell F232.
If vegetative filter strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, they make the strips are proposed for an interim permanent BMP, the strips are proposed for an interim permanent BMP, the strips are proposed for an interim permanent BMP, the strips are proposed for an interim permanent BMP, the strips are proposed for an interim permanent BMP, the strips are proposed for an interim permanent BMP, the strips are permanent by the strips are proposed for an interim permanent BMP, the strips are proposed for an interim permanent by the strips are proposed for an interim permanent by the strips are proposed for an interim permanent by the strips are permanent by the strips are proposed for an interim permanent by the strips are perm	ay be sized as described on Page 3-56 of RG-348.	Click on "Tools" and The value in the "Set
17. Wet Vaults	Designed as Required in RG-348 Pages 3-30 to 3-32 & 3-79	The value in the "By ( Click on solve.
Required Load Removal Based upon Equation 3.3 =	NA Ibs	The resulting "Desigi
First calculate the load removal at 1.1 in/hour		
RG-348 Page 3-30 Equation 3.4: Q = CiA		
C = runoff coefficient for the drainage area = i = design rainfall intensity = A = drainage area in acres =	0.34 C = Runoff Coefficient = 0.546 (IC) <sup>2</sup> + 0.328 (IC) + 0.03 1.1 in/hour 1 acres	
Q = flow rate in cubic feet per second =	0.37 cubic feet/sec	
RG-348 Page 3-31 Equation 3.5: V <sub>OR</sub> = Q/A		
Q = Runoff rate calculated above = A = Water surface area in the wet vault =	0.37 cubic feet/sec 150 square feet	
V <sub>OR</sub> = Overflow Rate =	0.00 feet/sec	
Percent TSS Removal from Figure 3-1 (RG-348 Page 3-31) =	53 percent	
Load removed by Wet Vault =	#VALUE! Ibs	
If a bypass occurs at a rainfall intensity of less than 1.1 in/hours Calculate the efficiency reduction for the actual rainfall intensity rate		
Actual Rainfall Intensity at which Wet Vault bypass Occurs =	0.5 in/hour	
Fraction of rainfall treated from Figure 3-2 RG-348 Page 3-32 = Efficiency Reduction for Actual Rainfall Intensity =	0.75 percent 0.83 percent	

18. Permeable Concrete	Designed as	Required in R	G-348	Pages 3-79 to 3-83
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING Z	ONE			
19. BMPs Installed in a Series	Designed as	Required in R	<u>3-348</u>	Pages 3-32
Michael E. Barrett, Ph.D., P.E. recommended that the coeff	icient for E <sub>2</sub> b	e changed fro	m 0.5 to 0.65 on May	3, 2006
$E_{TOT} = [1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))] \times 100 =$	- 86.	38 percent	NET EFFICIENCY O	F THE BMPs IN THE SERIES
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_{1}$ =	- 75.	00 percent		
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	70.	00 percent		
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3$ =	= 0.	00 percent		
THEREFORE, THE NET LOAD REMOVAL WOULD BE: (A, AND A, VALUES ARE FROM SECTION 3 ABOVE)				
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>1</sub> X 34.6 X A <sub>P</sub> X0.54) =	2859.	74 lbs		
20. Stormceptor				
Required TSS Removal in BMP Drainage Area=	NA	lbs		
Impervious Cover Overtreatment=	0.0000	ac		
TSS Removal for Uncaptured Area = BMP Sizing	0.00	ibs		
Effective Area =	NA	EA		
Calculated Model Size(s) = Actual Model Size (if multiple values provided in Calculated	#N/A			
Model Size or if you are choosing a larger model size) =	0	Model Size		
Surface Area =	#N/A	ťt <sup>2</sup>		
Overflow Rate =	#VALUE!	V <sub>or</sub>		
Rounded Overflow Rate =	#VALUE!	Vor		
BMP Efficiency % =	#VALUE!	%		
L <sub>B</sub> Value =	#VALUEI	lbs		
TSS Load Credit =	#VALUE!	lbs		
Is Sufficient Treatment Available? (TSS Credit $\geq$ TSS Uncapt.)	#VALUEI			
TSS Treatment by BMP (LM + TSS Uncapt.) =	#VALUE!			

Resultant TSS Load removed by Wet Vault = #VALUE! Ibs

CONTRACTOR OF THE OWNER

in the second second second

## 21. Vortech

BMP Sizing	Required TSS Removal in BMP Drainage Area= Impervious Cover Overtreatment= TSS Removal for Uncaptured Area =	<b>1274.59</b> 0.0000 0.00	lbs ac lbs
	Effective Area = Calculated Model Size(s) =	1.32 Vx16000	EA
	Actual Model Size (if choosing larger model size) =	Vx16000	Pick Model Size
	Surface Area =	113.10	ft <sup>2</sup>
	Overflow Rate =	0.012827	Vor
	Rounded Overflow Rate =	0.013300	V <sub>or</sub>
	BMP Efficiency % =	83.00	%
	L <sub>P</sub> Value =	1365.84	lbs
	TSS Load Credit =	91.25	lbs
Is Sufficient	Treatment Available? (TSS Credit $\geq$ TSS Uncapt.)	Yes	
	TSS Treatment by BMP (LM + TSS Uncapt.) =	1274.59	

## Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

Project Name: Christ Our King Anglican Church Date Prepared: 6/6/2010

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell.

Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348.

Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations	rom RG-348	Pages 3-27 to 3-30
Page 3-29 Equation 3.3: L <sub>M</sub> =	27.2(A <sub>N</sub> x P)		
where: L <sub>M TOTAL PROJECT</sub>	Required TSS Net increase	S removal resulting fi in impervious area fo	om the proposed development = 80% of increased load or the project
P =	Average ann	ual precipitation, inch	ies
Site Data: Determine Required Load Removal Based on the Entire Project County = Total project area included in plan * = Predevelopment impervious area within the limits of the plan * = Total post-development impervious area within the limits of the plan * = Total post-development impervious cover fraction * = P =	Comal 22.10 0.42 9.30 0.42 33	acres acres acres inches	
L <sub>M TOTAL PROJECT</sub> = * The values entered in these fields should be for the total project area.	7971	lbs.	
Number of drainage basins / outfalls areas leaving the plan area =	: 5		
2. Drainage Basin Parameters (This information should be provided for each	ch basin):		
Drainage Basin/Outfall Area No. =	- 4		
Total drainage basin/outfall area = Predevelopment impervious area within drainage basin/outfall area = Post-development impervious area within drainage basin/outfall area = Post-development impervious fraction within drainage basin/outfall area = السر This BASIN	= 1.98 = 0.00 = 1.40 = 0.71 = 1257	acres acres acres Ibs.	
3. Indicate the proposed BMP Code for this basin.			

Proposed BMP =	Vortechs	
Removal efficiency =	0	percent

Aqualogic Cartridge Filter Bioretention Contech StormFilter Constructed Wetland Extended Detention Grassy Swale Retention / Irrigation Sand Filter Stormceptor Vegetated Filter Strips Vortechs Wet Basin Wet Vault

#### 4. Calculate Maximum TSS Load Removed (L<sub>B</sub>) for this Drainage Basin by the selected BMP Type.

RG-348 Page 3-33 Equation 3.7:	L <sub>R</sub> = (B	MP efficien	ncy) x P x (A <sub>1</sub> x 34.6 + A <sub>P</sub> x 0.54)
	$A_{C} = T_{C}$	otal On-Site	drainage area in the BMP catchment area
	$A_i = Im$	npervious a	rea proposed in the BMP catchment area
	$A_P = P_0$	ervious area	a remaining in the BMP catchment area
	L <sub>R</sub> = TS	SS Load rer	moved from this catchment area by the proposed BMP
	A <sub>C</sub> =	1.98	acres
	A <sub>t</sub> =	1.40	acres
	A <sub>P</sub> =	0.58	acres
	L <sub>A</sub> =	0	lbs

#### 5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall area

where:

Desi	ired $L_{M}$ this basin =	3482	lbs.		
	F =	#DIV/0!			
6. Calculate Capture Volume required by the BMP Type for this drainage basin / outfall area.				Calculations from RG-348	Pages 3-34 to 3-36
Post Development Rut On-site Water	Rainfall Depth = noff Coefficient = Quality Volume =	#DIV/01 0.51 #DIV/01	inches cubic feet		

Calculations from RG-348 Pages 3-36 to 3-37

Off-site area draining to Off-site Impervious cover draining to Impervious fraction of off-site	BMP = BMP = e area =	0.00 0.00 0	acres acres	
Off-site Runoff Coef Off-site Water Quality Vo	ficient = olume =	0.00 #DIV/0!	cubic feet	
Storage for Sed	liment = $(1.20)$ =	#DIV/0!	aubia fa st	
The following sections are used to calculate the required water qual The values for BMP Types not selected in cell C45 will show NA.	lity volu	me(s) for the	selected BM	Р.
7. Retention/Irrigation System		Designed as F	Required in R	G-348 Pages 3-42 to 3-46
Required Water Quality Volume for retention	basin =	NA	cubic feet	
Irrigation Area Calculations:				
Soil infiltration/permeability Irrigation	y rate = area =	0.1 NA NA	in/hr square feet acres	Enter determined permeability rate or assumed value of 0.1
8. Extended Detention Basin System	1	Designed as F	lequired in R	G-348 Pages 3-46 to 3-51
Required Water Quality Volume for extended detention	basin =	NA	cubic feet	
9. Filter area for Sand Filters	ļ	Designed as F	lequired in R	G-348 Pages 3-58 to 3-63
9A. Full Sedimentation and Filtration System				
Water Quality Volume for sedimentation I	basin =	NA	cubic feet	
Minimum filter basin	area =	NA	square feet	
Maximum sedimentation basin Minimum sedimentation basin	area = area =	NA NA	square feet square feet	For minimum water depth of 2 feet For maximum water depth of 8 feet
9B. Partial Sedimentation and Filtration System				
Water Quality Volume for combined ba	asins =	NA	cubic feet	
Minimum filter basin	area =	NA	square feet	
Maximum sedimentation basin Minimum sedimentation basin	area = area =	NA NA	square feet square feet	For minimum water depth of 2 feet For maximum water depth of 8 feet

10. Bioretention System	Designe	ed as Required in R	G-348 P	ages 3-63 to 3-65
Required Water Quality Volume for Bioretention Bas	sin = N	A cubic feet		
11. Wet Basins	Designe	ed as Required in R	G-348 P	ages 3-66 to 3-71
Required capacity of Permanent Poor Required capacity at WQV Elevatio	ol= N/ on= N/	<ul><li>A cubic feet</li><li>A cubic feet</li></ul>	Permanent Pool Capac Total Capacity should plus a second WQV.	city is 1.20 times the WQV be the Permanent Pool Capacity
12. Constructed Wetlands	Designe	ed as Required in R	G-348 P	ages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetland	ds = N.	A cubic feet		
13. AquaLogic <sup>TM</sup> Cartridge System	Designe	ed as Required in F	G-348 P	rages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the requi	ired 20% inc	crease with mainte	nance contract with Aqu	uaLogic <sup>™</sup> .
Required Sedimentation chamber capac	ity = N	A cubic feet		
Filter canisters (FCs) to treat WC Filter basin area (RIA	2V = N \∈) = N	A cartridges A square fee		
		equale for		
14. Stormwater Management StormFilter® by CONTECH				
Required Water Quality Volume for Contech StormFilter Syste	em = N	A cubic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPs / LOAD REP	MOVALS AR	E BASED UPON F	LOW RATES - NOT CAL	CULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designe	ed as Required in F	G-348 F	Pages 3-51 to 3-54
Design parameters for the swale:				
Drainage Area to be Treated by the Swale =	A =	8.00 acres		
Impervious Cover in Drainage Ar	ea =	4.00 acres		
Swale Slo	pe =	0.01 ft/ft		
Side Slope	(z) =	3		
Design Water Depth = Weighted Bunoff Coefficient ⇒	=y= ⊧C≃	0.33 ft 0.54		
	~ -	0.01		
$A_{CS}$ = cross-sectional area of flow in Swa	ale =	13.17 sf		

.

$P_{W} = Wetted Perimeter =$	40.62 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

#### 15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = 1.49 A_{CS} R_{H}^{2/3} S^{0.5}$$
  
n

$$b = 0.134 \times Q$$
 - zy = 38.51 feet  
 $y^{1.67} S^{0.5}$   
 $Q = CiA = 4.71 cfs$ 

To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) = Q/A<sub>CS</sub> = 0.36 ft/sec

#### To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

15B.	Alternative Method using Excel Solver				To solve for bottom v Excel can simultaneo The required "Swale
	Design Q = CiA =	4.71 cfs			
	Manning's Equation Q = Swale Width=	0.76 cfs 6.00 ft	Error 1 =	3.95	First, highlight Cell F Then click on "Tools' The value in the "Set The value in the "By Click on solve.
	instructions are provided to the right (green comments).				The resulting "Swale If the resulting "Swal
	Flow Velocity	0.36 ft/s			
	Minimum Length = Instructions are provided to the right (blue comments).	107.24 ft			If there is not the opti Click on "Tools" and Then proc <del>ee</del> d as inst
	Design Width <del>=</del> Design Discharge = Design Depth =	6 ft 0.76 cfs 0.33 ft	Error 2 =	3.95	If you would like to in Excel can simultaned The required "Design

Flow Velocity =	0	.32 cfs			
Minimum Length =	97	.48 ft			First set the desired I Highlight Cell F232.
If any of the resulting values do not meet the design requirement set forth in	ı RG-348, tl	he design paran	neters may be modified	ed and the solver rerun.	
If any of the resulting values still do not meet the design requirement set for	th in RG-34	48, widening the	swale bottom value	may not be possible.	Click on "Tools" and
16. Vegetated Filter Strips	Designed as	s Required in RG	-348	Pages 3-55 to 3-57	The value in the "Set
These we establishes required for determining the load or size of used	Aliza filkan a				Click on solve.
There are no calculations required for determining the load or size of vegetative filter strips. The 80% removal is provided when the contributing drainage area does not exceed 72 feet (direction of flow) and the sheet flow leaving the impervious cover is directed across 15 feet of engineered filter strips with maximum slope of 20% or across 50 feet of natural vegetation with a maximum slope of 10%. There can be a break in grade as long as no slope exceeds 20%.					
If vegetative filter strips are proposed for an interim permanent BMP, they m	nay be size	d as described	on Page 3-56 of RG-3	48.	Click on "Tools" and The value in the "Set
					The value in the "By
17. Wet Vaults	Designed a:	s Required in RG	-348	Pages 3-30 to 3-32 & 3-79	Click on solve.
Required Load Removal Based upon Equation 3.3 =	NA	lbs			The resulting "Design If the resulting "Design
First calculate the load removal at 1.1 in/hour					
RG-348 Page 3-30 Equation 3.4: Q = CiA					
C = runoff coefficient for the drainage area = i = design rainfall intensity = A = drainage area in acres =	0	0.53 1.1 in/hour 1 acres	C = Runoff Coefficie	nt = 0.546 (IC) <sup>2</sup> + 0.328 (IC) + 0.03	
Q = flow rate in cubic feet per second =	C	).59 cubic feet/se	с		
RG-348 Page 3-31 Equation 3.5: V <sub>OR</sub> = Q/A					
Q = Runoff rate calculated above =	C	).59 cubic feet/se	с		
A = Water surface area in the wet vault =	1	150 square feet			
V <sub>OR</sub> = Overflow Rate =	C	).00 feet/sec			
Percent TSS Removal from Figure 3-1 (RG-348 Page 3-31) =		53 percent			
Load removed by Wet Vault =	#VALUE	l lbs			
If a bypass occurs at a rainfall intensity of less than 1.1 in/hours Calculate the efficiency reduction for the actual rainfall intensity rate					
Actual Rainfall Intensity at which Wet Vault bypass Occurs =		0.5 in/hour	a		
Fraction of rainfall treated from Figure 3-2 RG-348 Page 3-32 = Efficiency Reduction for Actual Rainfall Intensity =	C	).75 percent ).83 percent			

Resultant TSS Load removed by Wet Vault = #VALUE! Ibs

18. Permeable Concrete	Designed as F	Required in RC	à-348 Pages 3-79 to 3-83	
PERMEABLE CONCRETE MAY CNLY BE USED ON THE CONTRIBUTING ZONE				
19. BMPs Installed in a Series	Designed as F	Required in RC	à-348 Pages 3-32	
Michael E. Barrett, Ph.D., P.E. recommended that the coeffic	cient for E <sub>2</sub> be	changed fro	m 0.5 to 0.65 on May 3, 2006	
$E_{TOT} = [1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))] \times 100 =$	86.38	B percent	NET EFFICIENCY OF THE BMPs IN THE SERIES	
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1 =$	75.00	) percent		
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	70.00	) percent		
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3 =$	0.0	) percent		
THEREFORE, THE NET LOAD REMOVAL WOULD BE: (A, AND A <sub>P</sub> VALUES ARE FROM SECTION 3 ABOVE)				
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>I</sub> X 34.6 X A <sub>P</sub> X0.54) =	1389.6	5 lbs		
20. Stormceptor				
Required TSS Removal in BMP Drainage Area= Impervious Cover Overtreatment= TSS Removal for Uncaptured Area =	NA 0.0000 0.00	lbs ac lbs		
BMP Sizing				
Effective Area = Calculated Model Size(s) =	NA #N/A	EA		
Actual Model Size (if multiple values provided in Calculated Model Size or if you are choosing a larger model size) =	0	Model Size		
Surface Area =	#N/A	ft <sup>2</sup>		
Overflow Rate =	#VALUE!	V <sub>or</sub>		
Rounded Overflow Rate =	#VALUE!	Vor		
BMP Efficiency % =	#VALUE!	%		
L <sub>R</sub> Value =	#VALUE!	lbs		
TSS Load Credit =	#VALUE!	lbs		
Is Sufficient Treatment Available? (TSS Credit $\geq$ TSS Uncapt.)	#VALUE!			
TSS Treatment by BMP (LM + TSS Uncapt.) =	#VALUE!			

## 21. Vortech

Required TSS Removal in BMP Drainage Area=	1256.64	lbs
Impervious Cover Overtreatment=	0.0000	ac
TSS Removal for Uncaptured Area =	0.00	lbs
BMP Sizing		
Effective Area =	1.28	EA
Calculated Model Size(s) =	Vx16000	
	1410000	
Actual Model Size (if choosing larger model size) =	Vx16000	Pick Model Size
Notadi Model eize (il eneoding larger model bize) -	•***•••••	
Surface Area =	113.10	ft <sup>2</sup>
	0.040404	N N
Overflow Rate =	0.012424	Vor
Rounded Overflow Rate =	0.012500	Vor
BMP Efficiency % =	84.00	%
L <sub>B</sub> Value =	1351.44	lbs
TSS Load Credit =	94.80	lbs
	01.00	
Is Sufficient Treatment Available? (TSS Credit > TSS Uncant)	Ves	
	, 100	
TSS Treatment by BMP (I M + TSS Lincapt ) -	1256.64	
100 Heathent by DMF (EM + 100 Ofcapt.) -	1200.04	

# Texas Commission on Environmental Quality

TSS Removal Calculations 04-20-2009

Project Name: Christ Our King Anglican Church Date Prepared: 6/6/2010

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell.

Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348.

Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations fr	om RG-348	Pages 3-27 to 3-30		
Page 3-29 Equation 3.3: L <sub>M</sub> = 2	27.2(A <sub>N</sub> x P)				
where: L <sub>M TOTAL PROJECT</sub> =   A <sub>N</sub> =   P = ,	Requir <b>e</b> d TSS Net increase i Average annu	removal resulting from n impervious area for the al precipitation, inches	the proposed development = 80% of increased load e project		
Site Data: Determine Required Load Removal Based on the Entire Project County = Total project area included in plan * = Predevelopment impervious area within the limits of the plan * = Total post-development impervious cover fraction * = P =	Comai 22.10 0.42 9.30 0.42 33	acres acres acres inches			
LM TOTAL PROJECT =	7971	lbs.			
* The values entered in these fields should be for the total project area.					
Number of drainage basins / outfalls areas leaving the plan area =	5				
2. Drainage Basin Parameters (This information should be provided for each basin):					
Drainage Basin/Outfall Area No. =	5				
Total drainage basin/outfall area =	2.59	acres			
Predevelopment impervious area within drainage basin/outfall area =	0.00	acres			
Post-development impervious fraction within drainage basin/outfall area =	0.73	acres			
L <sub>M THIS BASIN</sub> =	1687	lbs.			
3. Indicate the proposed BMP Code for this basin.					
Proposed BMP = Vo	ortechs				
----------------------	---------	---------			
Removal efficiency =	0	percent			

Aqualogic Cartridge Filter Bioretention Contech StormFilter Constructed Wetland Extended Detention Grassy Swale Retention / Irrigation Sand Filter Stormceptor Vegetated Filter Strips Vortechs Wet Basin Wet Vault

#### 4. Calculate Maximum TSS Load Removed (L<sub>B</sub>) for this Drainage Basin by the selected BMP Type.

RG-348 Page 3-33 Equation 3.7: L<sub>R</sub> = (BMP efficiency) x P x (A<sub>1</sub> x 34.6 + A<sub>P</sub> x 0.54)

where:

A <sub>c</sub> = Total On-Site drainage area in the BMP catchment area						
A <sub>1</sub> = Impervious area proposed in the BMP catchment area						
A <sub>P</sub> = Pen	vious area	remaining in the BMP catchment area				
L <sub>R</sub> = TSS	Load rem	oved from this catchment area by the proposed BMP				
$A_{\rm C} =$	1.98	acres				
A <sub>i</sub> =	1.40	acres				
A <sub>P</sub> =	0.58	acres				
L <sub>R</sub> =	0	lbs				

#### 5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall area

Desired LM THIS BASIN =	3482	lbs.	
-------------------------	------	------	--

F = #DIV/0!

6. Calculate Capture Volume required by the BMP Type for this drainage basin / outfall area.

Calculations from RG-348

Pages 3-34 to 3-36

Rainfall Depth = #DIV/0! inchesPost Development Runoff Coefficient = 0.51On-site Water Quality Volume = #DIV/0!cubic feet

Calculations from RG-348 Pages 3-36 to 3-37

Off-site area draining to BMP =	• 0.00	acres	
Olf-site Impervious cover draining to BMP =	0.00	acres	
Impervious fraction of off-site area =	. 0		
Off-site Bunoff Coefficient =	0.00		
Off alto Mater Quality Volume -	- #DIV/01	cubic foot	
On-site water quality volume =	- #01v/0:	cubic reet	
Storage for Sediment =	#DIV/0!		
Total Capture Volume (required water quality volume(s) x 1.20) =	= #DIV/0!	cubic feet	
The following sections are used to calculate the required water quality vol-	ume(s) for the	e selected BMP.	
The values for BMP Types not selected in cell C45 will show NA.			
7 Retention/Irrigation System	Designed as	Required in BG-3	Pages 3-42 to 3-46
r. netendowingation oyatem	Designed as	nequies in no-o	
Required Water Quality Volume for retention basin =	- NA	cubic feet	
Irrigation Area Calculations:			
Coil infiltration/normanhility rate.	. 01	in/hr E	nter determined permeability rate or assumed value of 0.1
Son annualloupenneabhry rate -	= U.1	111/111 1	inci determined permeasanty rate of assumed value of or
irrigation area =	= NA	square reet	
	NA	acres	
8. Extended Detention Basin System	Designed as	Required in RG-3	348 Pages 3-46 to 3-51
·			
Required Water Quality Volume for extended detention basin =	= NA	cubic feet	
9 Filter area for Sand Filters	Designed as	Required in BG-3	848 Pages 3-58 to 3-63
S. THE DESTERATION OWNER AND S	Designed as	inequied in the e	1 4903 0 00 10 0 00
9A. Full Sedimentation and Filtration System			
an a			
Water Quality Volume for sedimentation basin :	= NA	cubic feet	
Minimum filter basin area :	= NA	square feet	
Maximum sedimentation basin area :	= NA	square feet E	for minimum water depth of 2 feet
Minimum codimentation basin area	_ NA	courre feet E	for maximum water denth of 8 feet
Winninghi Sedimentation basin area -	- 114	square reer 1	or maximum water depth of o feet
9B. Partial Sedimentation and Filtration System			
Water Quality Volume for combined basins :	= NA	cubic feet	
Minimum filter basin area	= NA	square feet	
Maximum sedimentation basin area	= NA	square feet F	or minimum water depth of 2 feet

10. Bioretention System	Designed a	as Required in R	G-348	Pages 3-63 to 3-65
Required Water Quality Volume for Bioretention Basin	= <b>NA</b>	cubic feet		
11. Wet Basins	Designed a	as Required in R	G-348	Pages 3-66 to 3-71
Required capacity of Permanent Pool Required capacity at WQV Elevation	= NA = NA	cubic feet cubic feet	Permanent Pool Cap Total Capacity shou plus a second WQV	pacity is 1.20 times the WQV Id be the Permanent Pool Capacity
12. Constructed Wetlands	Designed	as Required in R	G-348	Pages 3-71 to 3-73
Required Water Quality Volume for Constructed Wetlands	= NA	cubic feet		
13. AquaLogic <sup>™</sup> Cartridge System	Designed	as Required in R	G-348	Pages 3-74 to 3-78
** 2005 Technical Guidance Manual (RG-348) does not exempt the require	ed 20% incre	ase with mainte	nance contract with A	lquaLogic <sup>™</sup> .
Required Sedimentation chamber capacity Filter canisters (FCs) to treat WQV Filter basin area (RIA <sub>F</sub> )	= NA = NA = NA	cubic feet cartridges square feet		
14. Stormwater Management StormFilter® by CONTECH				
Required Water Quality Volume for Contech StormFilter System	= NA	cubic feet		
THE SIZING REQUIREMENTS FOR THE FOLLOWING BMPs / LOAD REMO	OVALS ARE	BASED UPON F	LOW RATES - NOT C	ALCULATED WATER QUALITY VOLUMES
15. Grassy Swales	Designed	as Required in R	G-348	Pages 3-51 to 3-54
Design parameters for the swale:				
Drainage Area to be Treated by the Swale = A Impervious Cover in Drainage Area Rainfall intensity = i Swale Slope Side Slope (z) Design Water Depth = y Weighted Runoff Coefficient = C		8.00 acres 4.00 acres 1.1 in/hr 0.01 ft/ft 3 0.33 ft 0.54		
A <sub>CS</sub> = cross-sectional area of flow in Swale	) = 1	3.17 sf		

P <sub>w</sub> = Wetted Perimeter =	40.82 feet
$R_{H}$ = hydraulic radius of flow cross-section = $A_{CS}/P_{W}$ =	0.32 feet
n = Manning's roughness coefficient =	0.2

#### 15A. Using the Method Described in the RG-348

Manning's Equation: 
$$Q = 1.49 A_{CS} B_{H}^{2/3} S^{0.5}$$
  
n  
 $b = \frac{0.134 \times Q}{y^{1.67} S^{0.5}} - zy = 38.51$  feet  
 $Q = CiA = 4.71$  cfs

To calculate the flow velocity in the swale:

V (Velocity of Flow in the swale) = Q/A<sub>CS</sub> = 0.36 ft/sec

#### To calculate the resulting swale length:

L = Minimum Swale Length = V (ft/sec) \* 300 (sec) = 107.24 feet

If any of the resulting values do not meet the design requirement set forth in RG-348, the design parameters must be modified and the solver rerun.

15B. /	Iternative Method using Excel Solver				To solve for bottom v Excel can simultaneo The required "Swale
	Design Q = CiA =	4.71 cfs			
	Manning's Equation Q = Swale Width=	0.76 cfs 6.00 ft	Error 1 =	3.95	First, highlight Cell F Then click on "Tools' The value in the "Set The value in the "By Click on solve.
	Instructions are provided to the right (green comments).				The resulting "Swale
					If the resulting "Swal
	Flow Velocity	0.36 ft/s			
	Minimum Length =	107.24 ft			If there is not the opti Click on "Tools" and Then proceed as inst
	Design Width = Design Discharge = Design Depth =	6 ft 0.76 cfs 0.33 ft	Error 2 =	3.95	lf you would like to in Excel can simultaneo The required "Design

Flow Velocity =	0.37 cfs	
Minimum Length =	97.48 ft	First set the desired I Highlight Cell F232.
If any of the resulting values do not meet the design requirement set forth in	G-348, the design parameters may be modified and the solver rerun.	
If any of the resulting values still do not meet the design requirement set for	in RG-348, widening the swale bottom value may not be possible.	Click on "Tools" and
		The value in the "Set
16. Vegetated Filter Strips	signed as Required in RG-348 Pages 3-55 to 3-57	Click on solve.
There are no calculations required for determining the load or size of vegeta	ve filter strips.	
The 80% removal is provided when the contributing drainage area does not of	ceed 72 feet (direction of flow) and	The resulting "Design
the sheet flow leaving the impervious cover is directed across 15 feet of eng	eered filter strips with maximum slope of 20% or	If the resulting "Designation of the second se
across 50 feet of natural vegetation with a maximum slope of 10%. There ca	be a break in grade as long as no slope exceeds 20%.	First set the desired i
If vegetative filter string are prepared for an interim permanent DHD they may	the sized as described as Data 2.55 of DC 249	Click on "Tools" and
in vegetative inter strips are proposed for an interim permanent BMP, they m	be sized as described on Page 3-56 of RG-346.	The value in the "Set
		The value in the "By
17. Wet Vaults	signed as Required in RG-348 Pages 3-30 to 3-32 & 3-79	Click on solve.
Required Load Removal Based upon Equation 3.3 =	NA Ibs	The resulting "Design
First calculate the load removal at 1.1 in/hour		if the resulting "Desig
RG-348 Page 3-30 Equation 3.4: Q = CiA		
C = rupoff coefficient for the drainage area =	0.56 0 - Runoff Coofficient - 0.545 (IC) <sup>2</sup> + 0.328 (IC) + 0.03	
i – design rainfall intensity –	1.1 in/hour	
A = drainage area in acres =	1 acres	
Q = flow rate in cubic feet per second =	0.61 cubic feet/sec	
RG-348 Page 3-31 Equation 3.5: $V_{OB} = Q/A$		
Q = Runoff rate calculated above =	0.61 cubic feet/sec	
A = Water surface area in the wet vault =	150 square feet	
V <sub>OR</sub> = Overflow Rate =	0.00 feet/sec	
Percent TCC Demousl from Figure 2.1 (PC 244 Page 2.21)		
Fercenic 133 Removaritoni Figure 3-1 (RG-346 Fage 3-31) =	55 percent	
Load removed by Wet Vault =	#VALUE! Ibs	
If a bypass occurs at a rainfall intensity of less than 1.1 in/hours		
Calculate the efficiency reduction for the actual rainfall intensity rate		
Actual Rainfall Intensity at which Wet Vault bypass Occurs =	0.5 in/hour	
Fraction of rainfall treated from Figure 3.0 DC 348 Days 0.00	0.75 percent	
Fificiency Reduction for Actual Rainfall Intensity -	0.75 percent	
Enciency neduction for Actual Maintair Intensity =	oldo percent	

18. Permeable Concrete	Designed as F	Required in RC	à-348	Pages 3-79 to 3-83		
PERMEABLE CONCRETE MAY ONLY BE USED ON THE CONTRIBUTING ZONE						
19. BMPs Installed in a Series	Designed as f	Required in RC	à-348	Pages 3-32		
Michael E. Barrett, Ph.D P.E. recommended that the coeffic	ient for $E_2$ be	changed fro	m 0.5 to 0.65 on May	3, 2006		
$E_{TOT} = [1 - ((1 - E_1) \times (1 - 0.65E_2) \times (1 - 0.25E_3))] \times 100 =$	86.3	8 percent	NET EFFICIENCY O	F THE BMPS IN THE SERIES		
EFFICIENCY OF FIRST BMP IN THE SERIES = $E_1 =$	75.0	0 percent				
EFFICIENCY OF THE SECOND BMP IN THE SERIES = $E_2$ =	70.0	0 percent				
EFFICIENCY OF THE THIRD BMP IN THE SERIES = $E_3$ =	0.0	0 percent				
THEREFORE, THE NET LOAD REMOVAL WOULD BE: $(A_1 \text{ AND } A_P \text{ VALUES ARE FROM SECTION 3 ABOVE})$						
L <sub>R</sub> = E <sub>TOT</sub> X P X (A <sub>i</sub> X 34.6 X A <sub>P</sub> X0.54) =	1389.6	5 lbs				
20. Stormceptor						
Required TSS Removal in BMP Drainage Area=	NA	lbs				
TSS Removal for Uncaptured Area =	0.0000	ac Ibs				
BMP Sizing						
Effective Area =	NA	EA				
Calculated Model Size (if multiple volved provided in Calculated	#N/A					
Model Size or if you are choosing a larger model size) =	0	Model Size				
Surface Area =	#N/A	ft <sup>2</sup>				
Overflow Rate =	#VALUE!	Vor				
Rounded Overflow Rate =	#VALUE!	V <sub>or</sub>				
BMP Efficiency % =	#VALUE!	%				
L <sub>R</sub> Value =	#VALUE!	lbs				
TSS Load Credit =	#VALUE!	lbs				
Is Sufficient Treatment Available? (TSS Credit > TSS Uncapt.)	#VALUE!					
TSS Treatment by BMP (LM + TSS Uncapt.) =	#VALUE!					

Resultant TSS Load removed by Wet Vault = #VALUE! Ibs

#### 21. Vortech

Required TSS Removal in BMP Drainage Area=	1687.49	lbs
Impervious Cover Overtreatment=	0.0000	ac
TSS Removal for Uncaptured Area =	0.00	lbs
BMP Sizing		
Effective Area =	1.71	EA
Calculated Model Size(s) =	Vx1319	
Actual Model Size (if choosing larger model size) =	Vx1421	Pick Model Size
Surface Area =	153.90	ft <sup>2</sup>
Overflow Rate =	0.012246	V <sub>or</sub>
Rounded Overflow Rate =	0.012500	Vor
BMP Efficiency % =	84.00	%
L <sub>R</sub> Value =	1813.76	lbs
TSS Load Credit =	126.27	lbs
Is Sufficient Treatment Available? (TSS Credit $\geq$ TSS Uncapt.)	Yes	
TSS Treatment by BMP (LM + TSS Uncapt.) =	1687.49	

RECEIVED Agent Authorization Form JUN 1 1 2010 For Required Signature Edwards Aquifer Protection Program HOUNTY ENGINEER Relating to 30 TAC Chapter 213 Effective June 1, 1999 L Charles Salsman Print Name **Project Manager** Title - Owner/President/Other Christ Our King Anglican Church of Corporation/Partnership/Entity Name have authorized \_\_\_\_\_ Jeffrev D. Moeller, P.E. Print Name of Agent/Engineer Hollmia Moeller Thornhill. Inc. of Print Name of Firm to represent and act on the behalf of the above named Corporation, Partnership, or Entity for

to represent and act on the behalf of the above named Corporation, Partnership, or Entity for the purpose of preparing and submitting this plan application to the Texas Commission on Environmental Quality (TCEQ) for the review and approval consideration of regulated activities.

I also understand that:

- 1. The applicant is responsible for compliance with 30 Texas Administrative Code Chapter 213 and any condition of the TCEQ's approval letter. The TCEQ is authorized to assess administrative penalties of up to \$10,000 per day per violation.
- 2. For applicants who are not the property owner, but who have the right to control and possess the property, additional authorization is required from the owner.
- 3. Application fees are due and payable at the time the application is submitted. The application fee must be sent to the TCEQ cashier or to the appropriate regional office. The application will not be considered until the correct fee is received by the commission.

4. A notarized copy of the Agent Authorization Form must be provided for the person preparing the application, and this form must accompany the completed application.

<u>6/3/1/0</u> Date plicant's Signature AMANDA M. GOLD Notary Public, State of Texas My Commission Expires THE STATE OF TO X45 § September 15, 2013 County of <u>Comal</u>

BEFORE ME, the undersigned authority, on this day personally appeared  $\underline{Chartes Salsman}$  known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that (s)he executed same for the purpose and consideration therein expressed.

GIVEN under my hand and seal of office on this <u>3</u> day of  $\frac{1}{2}$ ,  $\frac{2010}{2}$ .

Amanda H. Aale

Amanda m. Gold Typed or Printed Name of Notary

MY COMMISSION EXPIRES: <u>September 15, 2013</u>

#### Texas Commission on Environmental Quality Edwards Aquifer Protection Program Application Fee Form

NAME OF PROPOSED REGULATED I	ENTITY: <u>Chri</u>	<u>st Our King A</u>	<u>Inglican Chu</u>	<u>urch</u>	
REGULATED ENTITY LOCATION: 46	<u>3 FM 1863, No</u>	<u>ew Braunfels,</u>	TX 78132		
NAME OF CUSTOMER:Christ	<b>Our King An</b>	glican Church	1		
CONTACT PERSON: Charles Salsm	nan	P	HONE:	(830) 632-774	4
(Please Print)					
Customer Reference Number (if	issued): CN			_ (nine digits)	
Regulated Entity Reference Number (if	issued): RN _			(nine digits)	
Austin Regional Office (3373)	🗌 Hays	Travis	🗌 William	son	
San Antonio Regional Office (3362)	🗌 Bexar	🛛 Comal	🗌 Medina	🗌 Kinney	Uvalde
Application fees must be paid by check Environmental Quality. Your cancele your fee payment. This payment is be	, certified cheo d check will s ing submitted	ck, or money c erve as your r to (Check One	order, payable eceipt. <b>This</b> e):	e to the <b>Texas (</b> form must be	Commission on submitted with

 □ Austin Regional Office
 □ San Antonio Regional Office

 □ Mailed to TCEQ:
 □ Overnight Delivery to TCEQ:

 TCEQ – Cashier
 TCEQ - Cashier

 Revenues Section
 12100 Park 35 Circle

 Mail Code 214
 Building A, 3rd Floor

 P.O. Box 13088
 Austin, TX 78711-3088

 Austin, TX 78711-3088
 512/239-0347

Site Location (Check All That Apply):

Type of Plan	Size	Fee Due
Water Pollution Abatement Plan, Contributing Zone Plan: One Single Family Residential Dwelling	Acres	\$
Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks	Acres	\$
Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential	22.11 Acres	\$ 6,500
Sewage Collection System	L.F.	\$
Lift Stations without sewer lines	Acres	\$
Underground or Aboveground Storage Tank Facility	Tanks	\$
Piping System(s)(only)	Each	\$
Exception	Each	\$
Extension of Time	Each	\$

Celonar

6/3/10 Date

If you have questions on how to fill out this form or about the Edwards Aquifer protection program, please contact us at 210/490-3096 for projects located in the San Antonio Region or 512/339-2929 for projects located in the Austin Region.

Individuals are entitled to request and review their personal information that the agency gathers on its forms. They may also have any errors in their information corrected. To review such information, contact us at 512/239-3282.

TCEQ-0574 (Rev. 4/25/08)

### Texas Commission on Environmental Quality Edwards Aquifer Protection Program Application Fee Schedule 30 TAC Chapter 213 (effective 05/01/2008)

#### Water Pollution Abatement Plans and Modifications Contributing Zone Plans and Modifications

PROJECT	PROJECT AREA IN ACRES	FEE
One Single Family Residential Dwelling	< 5	\$650
Multiple Single Family Residential and Parks	< 5 5 < 10 10 < 40 40 < 100 100 < 500 ≥ 500	\$1,500 \$3,000 \$4,000 \$6,500 \$8,000 \$10,000
Non-residential (Commercial, industrial, institutional, multi-family residential, schools, and other sites where regulated activities will occur)	< 1 1 < 5 5 < 10 10 < 40 40 < 100 ≥ 100	\$3,000 \$4,000 \$5,000 \$6,500 \$8,000 \$10,000

#### **Organized Sewage Collection Systems and Modifications**

PROJECT	COST PER LINEAR FOOT	MINIMUM FEE MAXIMUM FEE
Sewage Collection Systems	\$0.50	\$650 - \$6,500

#### Underground and Aboveground Storage Tank System Facility Plans and Modifications

PROJECT	COST PER TANK OR PIPING SYSTEM	MINIMUM FEE MAXIMUM FEE
Underground and Aboveground Storage Tank Facility	\$650	\$650 <mark>- \$6,500</mark>

#### **Exception Requests**

PROJECT	FEE
Exception Request	\$500

#### Extension of Time Requests

PROJECT	FEE
Extension of Time Request	\$150



TCEQ Use Only

# **TCEQ Core Data Form**

For detailed instructions regarding completion of this form, please read the Core Data Form Instructions or call 512-239-5175.

SECTION	N I: <u>G</u> e	neral Information							
1. Reason fo	or Submis	sion (If other is checked please	describe i	in space pro	vided)				
New Pe	rmit, Regis	tration or Authorization (Core Da	ata Form si	hould be su	bmitted v	with the program a	pplicatio	on)	
Renewa	I (Core D	ata Form should be submitted wi	th the rene	ewal form)		Other			
2. Attachme	nts	Describe Any Attachments:	(ex. Title V /	Application, V	Vaste Trai	nsporter Application,	etc.)		
Yes	No	WPAP Application							//// A
3. Customer	Heterenc	e Number ( <i>it issued</i> )	for CN or	s link to sear	<u>ch</u> <b>4.</b> I in	Regulated Entity	Hetere	nce Numbe	er (if issued)
CN	_		Centra	I Registry**	F	RN			
<b>SECTION</b>	NII: C	ustomer Information							
5. Effective	Date for C	ustomer Information Updates (	mm/dd/yy	<b>yy)</b> 5/2	4/2010	)			
6. Customer	Role (Pro	posed or Actual) - as it relates to the	Regulated	Entity listed o	on this for	n. Please check onl	y <u>one</u> of	the following.	
Owner		Operator	$\boxtimes$ (	Owner & Op	erator				
	nal Licens	ee 🔲 Responsible Party		oluntary Cl	eanup Ap	oplicant C	Other:		
7. General C	ustomer l	nformation							
🛛 New Cus	tomer	🗌 Up	date to Cu	istomer Info	rmation	🔲 Ch	ange in	Regulated I	Entity Ownership
Change ir	Legal Na	ne (Verifiable with the Texas Sec	retary of S	itate)		<u>No</u>	Change	<u>)**</u>	
**lf "No Cha	nge" and	Section I is complete, skip to S	ection III -	- Regulated	l Entity I	nformation.			
8. Type of C	ustomer:	Corporation		ndividual		Sole Prop	rietorsh	ip- D.B.A	
City Gove	ernment	County Government	[]	ederal Gov	rnment	State Gov	ernmen	it	
Other Go	vernment	General Partnership	🗆 l	imited Part	nership	Other:			
9. Customer	Legal Na	ne (If an individual, print last name f	irst: ex: Doe	, John)	If new C below	ustomer, enter prev	/ious Cu	stomer	End Date:
Christ Ou	r King A	nglican Church							
	111 W	. San Antonio, St. Suite 2	250						
10. Mailing									
Address:	City	New Braunfels	State	ТХ	7IP	78130		7IP + 4	5158
11 Country	Uniling In		otato	10	E Mail A				5150
TI. Country	maning in			12.	<u>E-Mail A</u> alsman	asignalequit	ies co	m	
13. Telephor	e Number	1	4. Extensi	on or Code		15. Fax I	Vumber	(if applicat	ole)
(830)63	32-7744					( 830	) 632	7779	,
16. Federal 1	ax ID (9 dig	its) 17. TX State Franchise Ta	x ID (11 dig	its) 18. [	OUNS Nu	imber (if applicable)	19. TX	SOS Filing	Number (il applicable)
		32037185405					8009	85577	
20. Number	of Employ	ees				21. Inc	depende	ently Owne	ed and Operated?
0-20	21-100	101-250 251-500	🗌 501 a	nd higher			×Υ	es	No
SECTION	III: R	egulated Entity Infor	mation						
22. General F	Regulated	Entity Information (If 'New Reg	ulated Enti	tv" is select	ed below	this form should b	e accor	mpanied by	a permit application)
New Requ	ulated Entit	Update to Regulated En	tity Name		ate to Red	gulated Entity Info	rmation	□ No	Change** (See below)
		**If "NO CHANGE" is checked	and Section	l is complete	, skip to Se	ection IV, Preparer In	formation	ı.	
23. Regulate	d Entity N	ame (name of the site where the reg	ulated actio	n is taking pla	ace)				
Christ Our	King A	nglican Church							

24. Street Address	463 F	M 1863								
of the Regulated			_							
(No.P.O. Boxes)	City	New Braun	fels	State	TX	ZIP 7	8132		ZIP + 4	3629
	111 V	V. San Anto	onio St,	Suite 250						
25. Mailing										
AUG1635.	City	<b>City</b> New Braunfels		State	TX	ZIP 7	8130	_	ZIP + 4	5158
26. E-Mail Address:	csal	sman@sigr	alequiti	es.com						
27. Telephone Number	er			28. Extension	n or Code	29. Fa	x Number (if a	pplicable)		
<b>(</b> 830 <b>)</b> 632-7744						( 830	) 632-777	9		
30. Primary SIC Code	(4 digits)	31. Seconda	ry SIC Co	de (4 digits)	32. Primary I	NAICS Co	de 33.	Second	ary NAIC	S Code
8661		NA			813110		N/	A		
34. What is the Prima	ry Busine	ess of this enti	ity? (Ple	ase do not repe	eat the SIC or N	AICS descri	ption.)			
Church Campus	and Sch	1001								
C	uestions	34 - 37 addres	ss geogra	phic location	n. Please refe	r to the in	structions for	applica	bility.	
35. Description to Physical Location:	It is lo Highv	ocated on Fl way 46	M 1863	approx. 0	.75 miles so	outhwes	t of the inte	ersectio	on with	State
36. Nearest City			(	County		Sta	te		Nearest	ZIP Code
New Braunfels			(	Comal	-	ТУ	ζ		78132	
37. Latitude (N) In D	ecimal:	29.7150			38. Longit	ude (W)	In Decimal:	98.18	375	
Degrees	Minutes		Seconds		Degrees		Minutes		Sec	onds
029	42		54		98		11		15	
39. TCEQ Programs an	d ID Nur	<b>bers</b> Check all Pr	rograms and	write in the perm	nits/registration nur	mbers that wi	I be affected by th	e updates	submitted or	n this form or the
Dam Safety		Districts		Edwards /	Aquifer		atrial Hazardous	Macto		cinal Solid Waste
						Indu	Silial mazaluous	VVasie		
					Indu		Waste			
New Source Review	- Air	OSSF		Petroleum	Storage Tank			Waste		je
New Source Review	- Air	OSSF		Petroleum	n Storage Tank	D Indu		VVdSle		je
New Source Review	- Air	OSSF Title V – Air		Petroleum	n Storage Tank		d Oil			je
New Source Review	- Air	OSSF Title V – Air		Petroleum Tires	n Storage Tank		d Oil			je
New Source Review  Stormwater  Voluntary Cleanup	- Air	OSSF Title V – Air Waste Water		Petroleum Tires Wastew	a Storage Tank	Indu  PWS  Use  Wat	d Oil er Rights	Waste	Sludç	je
New Source Review Stormwater SECTION IV: I	- Air	OSSF   Title V – Air   Waste Water   er Inform:	ation	Petroleum Tires Wastew	a Storage Tank	Indu	d Oil er Rights	VVASIE	Sludg     Utili     Othe	je
New Source Review  Stormwater  Voluntary Cleanup  SECTION IV: I  40. Name: Jeffre	- Air	OSSF   Title V – Air   Waste Water   <b>er Inform</b> : peller, P.F.	ation	Petroleum Tires Wastew	a Storage Tank	Indu Indu Indu Indu Indu Indu Indu Indu	d Oil er Rights	d Age	Othe	je lies
New Source Review Stormwater Voluntary Cleanup SECTION IV: I 40. Name: Jeffre 42. Telephone Numbe	Prepar	OSSF Title V – Air Waste Water er Informa Deller, P.E. 43. Ext/Code	ation 44.	Petroleum Tires Wastew Fax Number	ater Agriculture	Indu     Indu	d Oil er Rights Authorize	ed Age	Slude     Other	
New Source Review  Stormwater  Voluntary Cleanup  SECTION IV: I  40. Name: Jeffre  42. Telephone Numbe (830) 625-8555	- Air	OSSF Title V – Air Waste Water er Inform: Deller, P.E. 43. Ext/Code	ation 44.	Petroleum Tires Wastew Fax Number 30) 625-8:	ater Agriculture	Indu     Indu	d Oil er Rights Authorize Address	ed Age	D Sludo	je
<ul> <li>New Source Review</li> <li>Stormwater</li> <li>Voluntary Cleanup</li> <li>SECTION IV: I</li> <li>40. Name: Jeffre</li> <li>42. Telephone Numbe</li> <li>(830) 625-8555</li> <li>SECTION V: A</li> </ul>	- Air	OSSF Title V – Air Waste Water er Informa Deller, P.E. 43. Ext/Code	<u>ation</u> 44. (8 ture	Petroleum Tires Wastew Fax Number 30) 625-8:	ater Agriculture	Indu     Indu	d Oil er Rights Authorize	ed Age	Initial Study     Initial Study     Initial Study     Initial Study     Initial Study     Initial Study	je

and that I have signature authority to submit this form on behalf of the entity specified in Section II, Field 9 and/or as required for the updates to the ID numbers identified in field 39.

(See the Core Data Form instructions for more information on who should sign this form.)

Company:	Christ Our King Anglican Church	Job Title:	Project	Manager	
Name(In Print):	Charles Salsman			Phone:	(830)632-7744
Signature:	Stoclomon			Date:	6/3/2010



# LEGEND LEGAL BOUNDARY LIMITS OF DRAINAGE AREA **ROCK BERM** SILT FENCE 900 -----STABILIZED CONSTRUCTION ENTRANCE

		-	8 8		/		UT BAS	
		-	- Kat w					
		-			Kdr _ 1	SILT FENCE		EXISTING
		-		STA				HOUSE
		_	- 11	946	1			It
				948		1340 Lr	X KAX	
				350				A
			111	952 Khu	VEG			
		-	11	956 000	FILTE	R STRIP		AX NB .
				10 950 -				TRUA
		,	111	962	1			
		/	11/1/	N	CONTROL	EASEMENT		
			11/1			-6	5%	
		-	411			B	STE EN PE	ZA HI
						VEGETATIVE	SPAX	S
M.			* • …		FI		NIKT	
					FVIET			
should be	secured w	ith a woven wire	sheathing baving maxin		- EXISTI	NG HOUSE	1 H H	KINT
um wire	diameter of	20 gauge galvan	ized and should be see	cured with	RETA	EXISTING <u> </u>		
					~			TTR-
3 - 5 in es of flor	w are expec	r rock should be cted, where $5 - 8$	used, except in areas 3 inch diameters rocks	where high may be used.		KOT		
					'			7
wire sheat	thing perper	ndicular to the flow	w line. the sheath	ing should be	S S			
top widt	h of 2 feet	with side slopes	being 2:1 (h:v) o	or flatter.	AL I			
g the she	athing as s	hown in the diagr	am, to a height of not	less than 18			1050	The g d
hing grou	nd the rock	and secure with	tie wire on that the e	ade of the	ACF		De C	
ast 2 incl	hes, and th	e berm retains its	shape when walked u	pon.	RES			and the second s
t along t	he contour	at zero percent g	rade or as near as po	ssible.				
m should	be tied int	to existing upslope	grade and the berm	should be		STABILIZED	X Z/m	
ice Guidel	lines:				01.	ENTRANCE	KI SH	
made w	eekly and a	fter each rainfall.	repair or replacement	should be	ŗ			HERIN
e of the	accumulate	d silt in an appro	oved manner that will n	n buildup ot cause anv	¢G.		1948948	11111941111
					122		4 844	PAR I
e sheathi	ng.					9	-946 2 -94	
resnaped e replace	d when stru	i during inspection icture ceases to t	function as intended dι	e to silt			Pro I	
rocks, w	ashout, con	struction traffic d	amage, etc.					
ld be left	in place u	ntil all upstream o	areas are stabilized and		OT 3		ENI	MAR
			WOMEN WIRE		- /			Coff
			SHEATHING			m	and the	-938
			FLOW		-			
					-	F	125×5	93
	-	3" 10 5" OPEN -	8-0209-00000000					
WOVEN	WIRE HING	GRADED RUCK	SINGS LABORED		-		- Ler-	
WOVEN	WINE HING				· v	ORTECHS		
WOVEN SHEAT	WIRE HING TO 4"				- V S MODI	ORTECHS YSTEM #1	A Start	
- 3°	TO 4"				V S MODI	YSTEM #1	Sent All	
	WIRE HING TO 4"	ISO	METRIC PLAN	VIEW	V S MODI	YSTEM #1	Serve and a serve	
	WIRE HING TO 4"	ISO	METRIC PLAN	VIEW	V S MODI	YSTEM #1		
- 3" - 3" ON Phase	To 4"	Impervious Area	METRIC PLAN	VIEW	WODI	VORTECHS YSTEM #1		
Phase 1 2	To 4" To 4" Total Area 0.12 0.11	Impervious Area 0.12 0.11	Treatment System Vegetative Filter Strip	VIEW s	WODI	VORTECHS YSTEM #1 EL 16000		Kgt
Phase 1 2 2	Total Area 0.12 0.11 0.23	Impervious Area 0.12 0.11 0.23	Treatment System Vegetative Filter Strip Vegetative Filter Strip	VIEW s s s	WODI	VORTECHS YSTEM #1 EL 16000		Kgt
Phase 1 2 2 2 2 2	Total Area 0.12 0.11 0.23 0.16 0.04	Impervious Area 0.12 0.11 0.23 0.16 0.04	Treatment System Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vortechs System #3 Vegetative Filter Strip	VIEW s s s	WODI	VORTECHS YSTEM #1 EL 16000	State	Kgt
Phase 1 2 2 2 1	Total Area 0.12 0.11 0.23 0.16 0.04 0.14	Impervious Area 0.12 0.11 0.23 0.16 0.04 0.13	Treatment System Vegetative Filter Strip Vegetative Filter Strip Vortechs System #3 Vegetative Filter Strip Vegetative Filter Strip	VIEW s s s s	WODI	PORTECHS YSTEM #1 EL 16000		
Phase 1 2 2 2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2	Total Area 0.12 0.11 0.23 0.16 0.04 0.14 0.17	Impervious Area 0.12 0.11 0.23 0.16 0.04 0.13 0.14	Treatment System Vegetative Filter Strip Vegetative Filter Strip Vortechs System #3 Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip	VIEW s s s s s s	V SS MODI	TECHS		
WOVEN           - 3"           - 3"           ION           Phase           1           2	Total Area 0.12 0.11 0.23 0.16 0.04 0.14 0.17 0.19 0.97	Impervious Area 0.12 0.11 0.23 0.16 0.04 0.13 0.14 0.11 0.00	Treatment System Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vortechs System #3 Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vortechs System #3 Vortechs System #3	VIEW s s s s s	V S MODI	TECHS		
WOVEN           - 3"           - 3"           ION           Phase           1           2           2           2           2           2           2           2           2           2           2           2           2           3	Total Area 0.12 0.11 0.23 0.16 0.04 0.14 0.17 0.19 0.97 0.12	Impervious Area 0.12 0.11 0.23 0.16 0.04 0.13 0.14 0.11 0.11 0.00 0.12	Treatment System Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vortechs System #3 Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vegetative Filter Strip Vortechs System #3 Vortechs System #3 Vortechs System #3	S S S S S S S S S S S S S S S S S S S	V S MODI	TECHS TECHS TECHS TECHS TECHS TECHS TECHS TECHS TECHS TECHS		Kgt Roc
WOVEN           - 3"           - 3"           ION           Phase           1           2           2           2           2           2           2           2           2           2           3           1           2	Total Area 0.12 0.11 0.23 0.16 0.04 0.14 0.17 0.19 0.97 0.12 0.06 0.47	Impervious Area 0.12 0.11 0.23 0.16 0.04 0.13 0.14 0.11 0.00 0.12 0.00 0.12 0.06	Treatment System Vegetative Filter Strip Vegetative Filter Strip Vortechs System #3 Vortechs System #3 Vortechs System #3 Vortechs System #3	VIEW s s s s s s s	V S MODI	TECHS TECHS EM #4 16000 Texas	Commission on Envire Water Pollution Abates	Roce

- Written construction notification must be given to the appropriate TCEQ regional office no later than 48 hours prior to commencement of the regulated activity. Information must include the date on which the regulated activity will commence, the name of the approved plan for the regulated activity, and the name of the prime contractor and the name and telephone number of the contact person.
- 2. All contractors conducting regulated activities associated with this project must be provided with complete copies of the approved Water Pollution Abatement Plan and the TCEQ letter indicating the specific conditions of its approval. During the course of these regulated activities, the contractors are required to keep on-site copies of the approved plan and approval
- be immediately notified of any sensitive features encountered during construction. The regulated activities near the sensitive feature may not proceed until the TCEQ has reviewed and approved the methods proposed to protect the sensitive feature and the Edwards Aquifer from any potentially adverse impacts to water quality.
- 5. Prior to commencement of construction, all temporary erosion and sedimentation (E&S) control measures must be properly selected, installed, and maintained in accordance with the
- manufacturers specifications and good engineering practices. Controls specified in the temporary storm water section of the approved Edwards Aquifer Protection Plan are required during construction. If inspections indicate a control has been used inappropriately, or incorrectly, the applicant must replace or modify the control for site situations. The controls must remain in place until disturbed areas are revegetated and the areas have become permanently stabilized.

# **ROCK BER**

### Materials:

(1) The berm structure of 11 inch and a minin shoat rings.

(2) Clean, open graded velocities or large volum Installation:

(1) Lay out the woven 20 gauge woven wire m

(2) Berm should have a (3) Place the rock alon

inches. (4) Wrap the wire sheat

sheathing overlaps at lea (5) Berm should be built (6) The ends of the be buried in a trench appro Inspection and Maintenan

(1) Inspection should be made promptly as neede reaches 6" and dispo additional siltation.

(3) Repair any loose wire

(4) The berm should be

(5) The berm should b accumulation among the (6) The rock berm should

accumulated silt removed

	24" MIN.	Г	
WOVEN WIRE SHEATHING	20000	R	
- 3" TO 4"			

CROSS SECT

Drainage Area ID	Phase	Total Area	Impervious Area	Treatment System
1	1	0.12	0.12	Vegetative Filter Strips
2	2	0.11	0.11	Vegetative Filter Strips
3	2	0.23	0.23	Vegetative Filter Strips
4	2	0.16	0.16	Vortechs System #3
5	2	0.04	0.04	Vegetative Filter Strips
6	1	0.14	0.13	Vegetative Filter Strip
7	2	0.17	0.14	Vegetative Filter Strips
8	2	0.19	0.11	Vortechs System #3
9	2	0.97	0.00	Vortechs System #3
10	3	0.12	0.12	Vortechs System #3
11	1	0.06	0.06	Vegetative Filter Strip
12	2	0.47	0.20	Vortechs System #3
13	2	0.05	0.05	Vortechs System #1
14	2	0.45	0.26	Vortechs System #1
15	3	0.53	0.33	Vortechs System #2
16	4	0.24	0.12	Vortechs System #1
17	4	0.73	0.41	Vortechs System #1
18	4	0.04	0.04	Vortechs System #1
19	4	0.87	0.53	Vortechs System #2
20	5	0.88	0.59	Vortechs System #2
21	1	1.15	0.96	Vortechs System #1
22	1	1.62	1.31	Vortechs System #2
23	6	1.98	1.40	Vortechs System #4
24	6	2.59	1.88	Vortechs System #5

### **VEGETATIVE FILTER STRIP**

**EXISTING CONTOURS** 

**PROPOSED CONTOURS** 

FM 1863

# SOIL STABILIZATION NOTE

DISTURBED AREA NOTE

**ORTECHS** SYSTEM #3 **MODEL 16000** 

ALL DISTURBED SOILS SHOULD BE SEEDED OR OTHERWISE STABILIZED WITH 14 CALENDAR DAYS AFTER FINAL GRADING OR WHERE CONSTRUCTION ACTIVITY HAS TEMPORARILY CEASED FOR MORE THAN 21 DAYS.

ALL AREAS SHOWN WITH PAVEMENT, BUILDINGS, SIDEWALKS, SITE GRADING, VEGETATIVE FILTER STRIPS, AND VORTECHS SYSTEMS WILL BE DISTURBED. THE TOTAL DISTURBED AREA FOR THE PROJECT IS 12.38 ACRES. DUE TO THE PHASING OF THE PROJECT, NO MORE THAN 10 ACRES WILL BE DISTURBED AT ONE TIME.



PROFILE

# -POLYPROPYLENE, POLYETHYLENE OR POLYAMIDE



## SILT FENCE Materials:

(1) Silt fence material should be polypropylene, polyethylene or polyamide woven or nonwoven fabric. The fabric width should be 36 inches, with a minimum unit weight 4.5 oz/yd, mullen burst strength exceeding 190 lb/in2, ultraviolet stability exceeding 70%, and minimum apparent opening size of U.S. Sieve No. 30.

(2) Fence posts should be made of hot rolled steel, at least 4 feet long with Tee or Ybar cross section, surface painted or galvanized, minimum nominal weight 1.25 Ib/ft2, and Brindell hardness exceeding 140.

(3) Woven wire backing to support the fabric should be galvanized 2" x 4" welded w 12 gauge minimum.

Installation:

SILT FENCE

- VORTECHS

/SYSTEM #2

MODEL 1421

F

(1) Steel posts, which support the silt fence, should be installed on a slight angle toward the anticipated runoff source. Post must be embedded a minimum of 1deep and spaced not more than 8 feet on center. Where water concentrates, the maximum spacing should be 6 feet.

(2) Lay out fencing down-slope of disturbed area, following the contour as closely as possible. The fence should be sited so that the maximum drainage area is 1/4 acre/100 feet of fence.

(3) The toe of the silt fence should be trenched in with a spade or mechanical trenche so that the down-slope face of the trench is flat and perpendicular to the line of flow. Where fence cannot be trenched in (e.g., pavement or rock outcrop), weight fabrie flap with 3 inches of pea gravel on uphill side to prevent flow from seeping under fend (4) The trench must be a minimum of 6 inches deep and 6 inches wide to allow for the silt fence fabric to be laid in the ground and backfilled with compacted material. (5) Silt fence should be securely fastened to each steel support post or to woven win which is in turn attached to the steel fence post. There should be a 3-foot overlap securely fastened where ends of fabric meet.

(6) Silt fence should be removed when the site is completely stabilized so as not to block or impede storm flow or drainage.

Inspection and Maintenance Guidelines:

(1) Inspect all fencing weekly, and after any rainfall.

(2) Remove sediment when buildup reaches 6 inches.

(3) Replace any torn fabric or install a second line of fencing parallel to the torn section.

(4) Replace or repair any sections crushed or collapsed in the course of construction activity. If a section of fence is obstructing vehicular access, consider relocating it to spot where it will provide equal protection, but will not obstruct vehicles. A triangular filter dike may be preferable to a silt fence at common vehicle access points.

(5) When construction is complete, the sediment should be disposed of in a manner th will not cause additional siltation and the prior location of the silt fence should be revegetated. The fence itself should be disposed of in an approved landfill.

- 6. If sediment escapes the construction site, off-site accumulations of sediment must be removed at a frequency sufficient to minimize offsite impacts sediment in street being washed into surface streams or sensitive features by the next rain).
- 7. Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50%. A permanent statindicate when the sediment occupies 50% of the basin volume.
- 8. Litter, construction debris, and construction chemicals exposed to stormwater shall be prevented from becoming a pollutant source for stormwater disch picked up daily).
- 9. All spoils (excavated material) generated from the project site must be stored on—site with proper E&S controls. For storage or disposal of spoils at Aquifer Recharge Zone, the owner of the site must receive approval of a water pollution abatement plan for the placement of fill material or mass grad spoils at the other site.
- 10. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently cease 14 days after the construction activity in that portion of the site has temporarily or permanently ceased. Where the initiation of stabilization meas construction activity temporary or permanently cease is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable. a portion of the site is temporarily ceased, and earth disturbing activities will be resumed within 21 days, temporary stabilization measures do not have to of site. In areas experiencing droughts where the initiation of stabilization measures by the 14th day after construction activity has temporarily or permanent seasoned arid conditions, stabilization measures shall be initiated as soon as practicable.

11. The following records shall be maintained and made available to the TCEQ upon request: the dates when major grading activities occur; the date temporarily or permanently cease on a portion of the site; and the dates when stabilization measures are initiated.

The holder of any approved Edward Aquifer protection plan must notify the appropriate regional office in writing and obtain approval from the executive director

MERRI J PARMLEY DOC. NO. 9606012461 CK BERM VORTECHS SYSTEM #5 -**MODEL 1421** 

ROCK BERM -

3. If any sensitive feature is discovered during construction, all regulated activities near the sensitive feature must be suspended immediately. The appropriate TCEQ regional office must

4. No temporary aboveground hydrocarbon and hazardous substance storage tank system is installed within 150 feet of a domestic, industrial, irrigation, or public water supply well, or other sensitive feature.

STABILIZ	ED CONSTRUCTION ENTRANCE / EXIT				RNHILL
Materials: (1) The aggrega	ate should consist of 4 to 8 inch washed stone over a stable foundation				R = THO
as specified in (2) The aggreg	the plan.			65	
(3) The geotex	tile fabric should be designed specifically for use as a soil filtration media				MOE
with an approxi	mate weight of 6 oz/yd2, a mullen burst rating of 140 lb/in2, and an				
equivalent open	ing size greater than a number 50 sieve.				
(4) If a washin washed stone	g facility is required, a level area with a minimum of 4 inch diameter or commercial rack should be included in the plans. Divert wastewater to		IL		
a sediment tra	o or basin.	410	N S		
Installation:		NEV	N. SI	AUNFE	LS
(1) Avoid curve	s on public roads and steep slopes. Remove vegetation and other material from the foundation area. Grade crown foundation for positive			7010	0001
drainage.	indicende norm the roundation dred. Grade crown roundation for positive	IBPE ww	Firm w.hm	tnb.cc	0961 om
(2) The minimu	m width of the entrance/exit should be 12 feet or the full width of exit	Ph: 8 Fax:	330- 830-	625-8	8555 8556
roadway, whiche	ever is greater.			1	1.1.
(3) The constru (4) If the slope	toward the road exceeds 2% construct a ridge 6 to 8 inches high with		and l		Jour
3:1 (H:V) side	slopes, across the foundation approximately 15 feet from the entrance to	(it	717		***
divert runoff aw	ay from the public road.	JE	FREY	). MOELI	ER
(5) Place geote	xtile fabric and grade foundation to improve stability, especially where wet	FROM	88	NSED	ALL ALL
(6) Place store	to dimensions and grade shown on plane. Leave surface smooth and		SION	ALENS	10
slope for draina	ge.			~1	
(7) Divert all su	urface runoff and drainage from the stone pad to a sediment trap or				
basin.					
(8) Install pipe	unaer paa as neeaea to maintain proper public road drainage. Maintenance Guidelines:				
(1) The entranc	e should be maintained in a condition, which will prevent tracking or				
lowing of sedim	ent onto public rights—of—way. This may require periodic top dressing with	_			
additional stone	as conditions demand and repair and/or cleanout of any measures used	A			
(2) All sedimen	t spilled, dropped, washed or tracked onto public rights—of—way should be	Ч			
removed imme	diately by contractor.	E			
(3) When neces	sary, wheels should be cleaned to remove sediment prior to entrance onto	S			
, public right-of- (4) When washi	way. ng is required, it should be done on an area stabilized with crushed stone	AP			
that drains into	an approved sediment trap or sediment basin.	A N			
(5) All sediment	t should be prevented from entering any storm drain, ditch or water	-			
course by using	approved methods.				
HYDRAU	LIC MULCH				
Materials:					
Hydraulic Mulch matrices. Wood	es: Wood fiber mulch can be applied alone or as a component of hydraulic fiber applied alone is typically applied at the rate of 2.000 to 4.000				
Ib/acre. Wood	fiber mulch is manufactured from wood or wood waste from lumber mills sources.				
Hydraulic Matric	es: Hydraulic matrices include a mixture of wood fiber and acrylic polymer				
or other tackifi (i.e., hydro see	er as binder. Apply as a liquid slurry using a hydraulic application machine der) at the following minimum rates, or as specified by the manufacturer				
to achieve com	plete coverage of the target area: 2,000 to 4,000 lb/acre wood				20
Bonded Elber M	atrix: Bonded fiber matrix (BFM) is a hydraulically applied system of fibers	g	5		TE 2.
and adhesives a	that upon drying forms an erosion resistant blanket that promotes prevents soil erosion. BFMs are typically applied at rates from 3,000		F		SUI SUI
Ib/acre to	4,000 lb/acre based on the manufacturer's recommendation. A	<b>a</b>	Ę		EX,
the BFM should	also be biodegradable and should not dissolve or disperse upon ically, biodegradable BFMs should not be applied immediately before during				S, T
or immediately	after rainfall if the soil is saturated. Depending on the product, BFMs 12 to 24 hours to dry and become effective		N		NTO NTO
Installation:		S.			AN A
(1) Prior t	o application, roughen embankment and fill areas by rolling with a crimping the roller or by track walking. Track walking shall only be used where other	¥ 3	5		V. SV
methods are im (2) To be	offective, hydraulic matrices require 24 hours to dry before rainfall occurs	0	Z		NIN NIN
(3) Avoid vegetation, etc.	mulch over spray onto roads, sidewalks, drainage channels, existing				
Inspection and	Maintenance Guidelines:				
(1) Mulche and repair any	d areas should be inspected weekly and after each rain event to locate damage.				
(2) Areas and hydraulic m	damaged by storms or normal construction activities should be regraded nulch reapplied as soon as practical.				
water quality (e.g., fusitive	the following:				101
must be provided that any	A. any physical or operational modification of any water pollution abatement structure(s), including but	/2010			)K001.
hiust be provided that can	B. any change in the nature or character of the regulated activity from that which was originally	5/8/	=	Sol	ER: CO
es (e.g., screening outfalls,	approved or a change which would significantly impact the ability of the plan to prevent pollution of the Edwards Aquifer;		BY: ,	BY:	NUMBE
nother site on the Edwards prior to the placement of	C. any development of land previously identified as undeveloped in the original water pollution abatement plan.	NN B	GNED	CKED	EVED
but in no case more than	Austin Regional Office     San Antonio Regional Office       2800 S. IH 35, Suite 100     14250 Judson Road       Austin Taxas     78704 5719	DATE	DESIG	CHEC	PROJ
es by the 14th day after ere construction activity on be initiated on that portion	Ausuri, 1exas         76704-5712         San Antonio, 1exas         78233-4480           Phone (512)         339-2929         Phone (210)         490-3096           Fax         (512)         339-3795         Fax         (210)         545-4329	5	HE	ET	
ntly ceased is precluded by			-		
when construction activities					
ior to initiating any of			OF	1	



v:\!Projects\Christ Our King Anglican Church\Project Admin\Documents\WPAP\WPAP Grading Plan-Phase 1.dwg User: IngallsJI Jun 08, 2010 -



and a comparison of a A CANADA AND A CANADA A the west of the second second 



N:\!Projects\Christ Our King Anglican Church\Project Admin\Documents\WPAP\WPAP Grading Plan-Phase 4.dwg User: IngallsJI Jun 08, 2010 - 11:14am





A -IMB R WIL D





